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THE MEAN OBSERVED METEOROLOGICAL STRUCTURE AND CIRCULATION OF THE STRATOSPHERE AND MESOSPHERE

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CONTENTS

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Abstract														•									•				٠,	•	i
INTRODUCTION	1										•	•	•										•	•					1
SOUNDINGS .																•	•	•			•		•	•					2
PRESENTATION	1 O	F	Τŀ	ŧΕ	D	ΑT	Ά		•	•		•										•					•		4
ANALYSIS OF F	RES	sU	LI	S				•	•													•				•			5
CONCLUSION																			•			•		•				•	31
References				•									•	•										•	•			•	32
Appendix A				•																•				•	•			•	35
Appendix B																												′ .	57

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Globe Universal Sciences

INTRODUCTION

The Meteorological Sounding Rocket Program at Goddard Space Flight Center has conducted in situ measurements of the meteorological parameters of the atmosphere since 1960 in a systematic effort intended to define and better understand the physics and meteorology of the atmosphere in the altitude region between approximately 35 and 100 km. The atmosphere above 50 km is relatively inaccessible except to high performance sounding rockets, and their rapid passage through the region of interest requires such sophisticated sensing methods as the acoustic grenade and pitot probe techniques, rather than immersion thermometry to measure ambient temperature, for example. Since these techniques involve more complex experimental hardware and data processing to obtain results, the number of soundings that can be conducted is limited by economic considerations. Thus, the mean profiles and analyses included in this report are based upon 227 soundings, a relatively small sample compared to the data available at lower levels. Nevertheless, the soundings compiled here represent the largest body of data for which the techniques, quality control, and data processing have been consistent over a 10 year period of time.

The standard atmosphere models, such as the "COSPAR International Reference Atmosphere"; (Reference 1), the "U.S. Standard Atmosphere, 1962" (Reference 2), and the "U.S. Standard Atmosphere Supplements, 1966" (Reference 3), are based on the observations which were available prior to 1966. Additional data are now available, and the existing techniques for observing the meteorological structure of the mesosphere have been improved upon, revealing some differences with and filling some voids in these model atmospheres. All model atmospheres have minute detail removed from their structure, but oversimplification by smoothing can also compromise the usefulness of the model. Hopefully, the compilation of statistical means produces realistic values of the atmospheric parameters,

provided the sample is a representative one. The purpose of this report is to compile a climatology of observed values of temperature, pressure, density, and wind at various sites during all seasons which will update and supplement the standard models to provide realistic inputs for computations involving neutral and ion composition, energy deposition and propagation, transport processes, and design considerations for spacecraft reentry.

SOUNDINGS

As mentioned in the foregoing section, two methods were employed to obtain the data: the acoustic grenade technique (Reference 4) was used to measure profiles of temperature and horizontal wind, which permitted the derivation of pressure and density profiles, and the pitot probe technique (Reference 5) was used to measure profiles of density, which permitted the derivation of temperature and pressure profiles. Of the 227 soundings included in this report, 207 were grenade soundings, and the remainder were pitot soundings. Complete tabulations of the individual soundings are published in References 6, 7, 8, 9, 10, 11, and 12.

The acoustic grenade technique averages inherently the temperature and wind over layers between adjacent grenade explosions which are typically 2 to 4 km in thickness. The pitot probe technique, however, produces density profiles which have a vertical resolution of 0.5 km. The technical details of these techniques and the errors associated with them are published in the references already cited and will not be repeated here.

The mean profiles given here include soundings carried out from five sites which covered a wide range of geographical latitudes during all seasons. The launch sites included Natal, Brazil (6° S), and Ascension Island (8° S), which were combined to represent a tropical regime; Wallops Island, Virginia, United States (38° N), representing a temperate regime; Churchill, Manitoba, Canada (59° N), representing a subarctic regime; and Point Barrow, Alaska, United States (71° N), representing an arctic regime. The soundings were fairly well distributed throughout the year, as well as the diurnal cycle, as shown by the distributions given in Figures 1(a) and 1(b). Ideally, these distributions would be uniform, but the soundings were conducted over the years to satisfy various objectives, with climatological ones low in priority.

No attempt has been made to remove the tidal components from the data because of the uncertainties involved in the theory. Variations produced by relatively short term phenomena ranging from gravity waves to synoptic scale eddies tend to be removed by the averaging process when monthly and seasonal means are computed. Gravity wave and tidal phenomena are believed to be responsible for very large amplitude fluctuations observed in the structure of the upper atmosphere in certain cases; however, the averaging procedure appears to remove these short term changes from the mean profiles effectively. This is indicated by the coherent geostrophic analyses which result from the mean wind and pressure values at all but the highest altitudes. Were the short term fluctuations not removed, their ageostrophic contributions would make such analyses impossible.

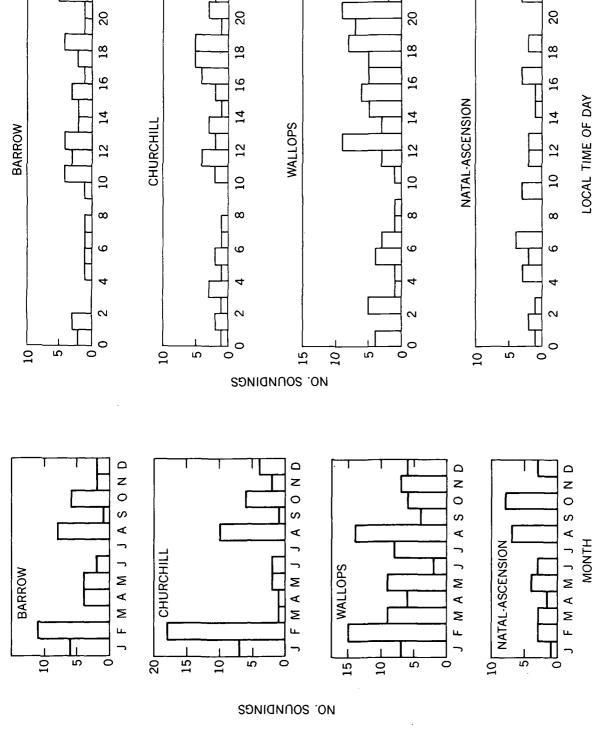


Figure 1(b)—The hourly distribution of the soundings for each site.

Figure 1(a)—The monthly distribution of the

soundings for each site.

PRESENTATION OF THE DATA

The relatively small number of soundings available has made it necessary to combine the monthly data into seasonal means. Therefore, those soundings conducted in December, January, and February were averaged to produce a mean winter model; those soundings conducted in June, July, and August were averaged to produce a mean summer model; and those conducted in March, April, May, September, October, and November were averaged to produce a mean spring/fall, or transition, model for the sites Wallops Island, Churchill, and Barrow. Since only a very small seasonal dependence was detected in the Natal-Ascension soundings, the data for all months were averaged together to produce a mean annual model. The numbers of soundings and the months included in each model are listed in Table 1. The annual and seasonal mean profiles are tabulated in Appendixes A and B. Tables A.1 through A.4 present the temperature, pressure, and density data as compared with values from "U.S. Standard Atmosphere, 1962", and Tables B.1 through B.4 present the same results compared with values from the "U.S. Standard Atmosphere Supplements, 1966".

The models consist of tabulations of mean temperature, mean pressure, and mean density at 1 km intervals along with the standard deviations of these mean values and their percent difference from values in "U.S. Standard Atmosphere, 1962". The number of observations included at each level is tabulated at the right. This number refers to the number of times that the parameters were observed (or derived from an observation) at that altitude.

Rather than interpolating values at 1 km altitude intervals as was done for the thermodynamic structure, the winds were taken from the grenade soundings at their observed altitudes and grouped into layers 5 km thick. All the wind observations within each layer were averaged with equal weight to produce the mean and the standard deviation for that layer. The mean for each layer is listed by the altitude of the lower boundary of the layer for convenience. For example, the mean listed at 40 km is actually the mean for the 40 to 45 km layer. In the curves of the mean wind profiles, the averages for the layers are plotted at the center of the layer (i.e., the mean value for the 40 to 45 km layer is plotted at 42.5 km).

Table 1—Number of soundings included in each mean atmosphere me	Table 1 Normbon of	'aassadiaaa	سنام ما مراه سنا		-4
	Table 1—Number of	soundings	included in	each mean	armosphere model.

Site	Winter (Dec., Jan., Feb.)	Summer (June, July, Aug.)	Spring/Fall (Mar., Apr., May, Sep., Oct., Nov.)	Annual (JanDec.)
Natal-Ascension (6 to 8° S)	-	_	_	34
Wallops (38° N)	28	24	41	_
Churchill (59° N)	29	12	13	_
Barrow (71° N)	19	10	17	-

The most recent grenade soundings include error analyses for temperature or both temperature and wind (soundings conducted between 1964 and 1967 were analyzed for temperature error only, and the 1968 through 1969 soundings were analyzed for both temperature and wind errors). In order to give the reader an estimate of the total uncertainty in the data, these errors were averaged and standard deviations from those average values computed. For simplicity, the errors were tabulated in the same fashion as the winds. No errors were computed for pressure and density as these are not only a function of the errors in the temperature profiles (for the grenade technique) but also depend upon the errors contained in the initial pressure reference points which are obtained from balloonsondes.

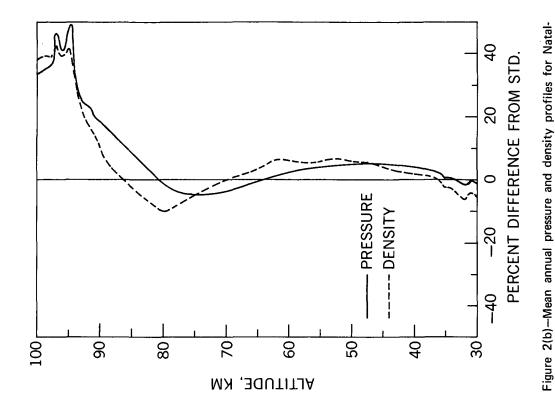
In Reference 13, some of the same data (1960 to 1968) have been compared with values from "U.S. Standard Atmosphere Supplements, 1966", demonstrating that some substantial differences exist between the statistical mean of the observations and the values from their corresponding latitude and season standard models. Of course, the argument can be made that the observations are valid for only one station, while the standard model is an attempt to give a representative value for a given latitude (i.e., all longitudes). However, the standard models relied heavily upon earlier observations even though they were more sparse than the data reported here, and as will be shown later, conditions at one latitude vary greatly with longitude.

The resulting statistical models, presented both graphically and in tabular form, are given in Figures 2 through 5 and the corresponding Tables A.1 through A.4 and B.1 through B.4. These values are the results of arithmetically averaging all of the included data, and no interpretation of the individual mean profiles is given, other than to note that the atmosphere varies greatly with both season and geographical location.

ANALYSIS OF RESULTS

The remainder of this report is concerned with the analysis of the mean profiles. Time and meridional cross sections of mean temperature, pressure, density, and wind, as well as mean seasonal synoptic maps at 60, 70, and 80 km, have been presented (see Reference 14). As might be expected, these analyses lack detail due to the sparse data available and the smoothing which is inherent in compiling mean values. Nevertheless, the cross sections and maps are useful in describing the gross characteristics of the thermodynamic structure and general circulation of the atmosphere between about 40 and 100 km altitude, primarily over the North American continent.

In Figures 6(a) through 6(d), the mean monthly temperature profiles for each site were analyzed as a function of time. Figure 6(a), which shows the mean temperature cross section for Natal, is characterized by its uniformity below 75 km. There is an insignificant annual variation in the stratopause temperature; the total change is less than 10 K throughout the year. The warmest temperatures at the stratopause occur in the February through April period. The lapse rates in the mesosphere do not vary significantly with time below 70 km. The upper mesosphere and lower thermosphere monthly means are subject to 10 to 20 K changes during the course of the year, probably more as a result of incomplete removal of the tidal components rather than a genuine seasonal effect.



(6° S to 8° S) based on 34 soundings.

Figure 2(a) - Mean annual temperature profile for Natal-Ascension

ALTITUDE, KM

TEMPERATURE, K

Ascension (6° S to 8° S) based on 34 soundings. (Standard is Reference 2.)

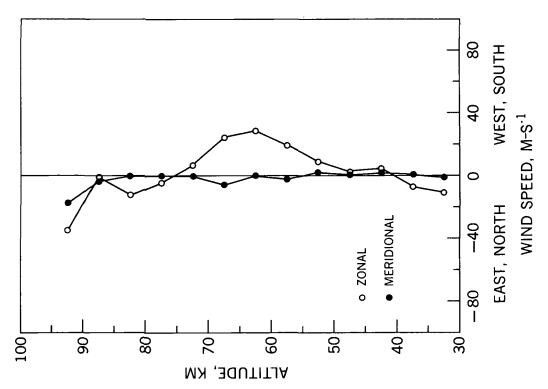
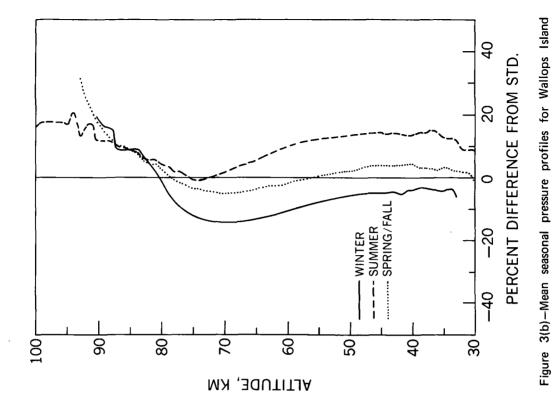


Figure 2(c)—Mean annual wind components for Natal-Ascension (6° S to 8° S) based on 28 soundings.



soundings.

(38° N) based on 28 winter, 24 summer, and 41 transition soundings.

(Standard is Reference 2.)

Figure 3(a)-Mean seasonal temperature profiles for Wallops Island (38° N) based on 28 winter, 24 summer, and 41 transition

TEMPERATURE, K

320

280

240

200

160

9

..... SPRING/FALL ---- SUMMER

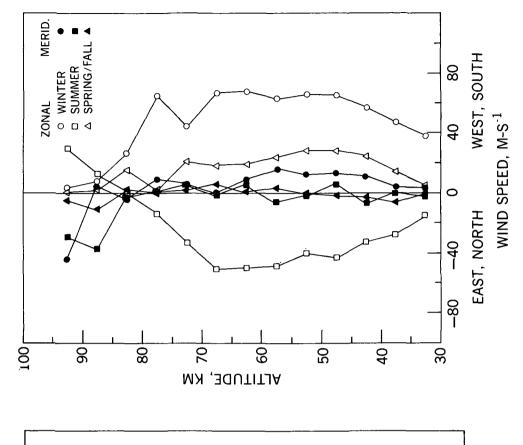
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ALTITUDE, KM

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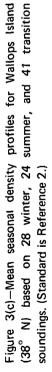
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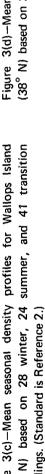


---- SUMMER
---- SPRING/FALL

ALTITUDE, KM

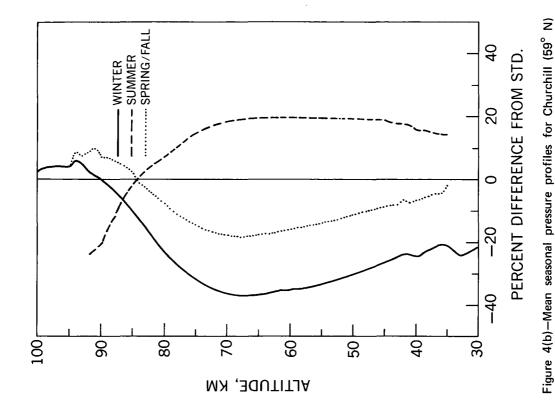


PERCENT DIFFERENCE FROM STD.



-20

Figure 3(d)-Mean seasonal wind components for Wallops Island (38° N) based on 28 winter, 19 summer, and 39 transition soundings.



ALTITUDE, KM

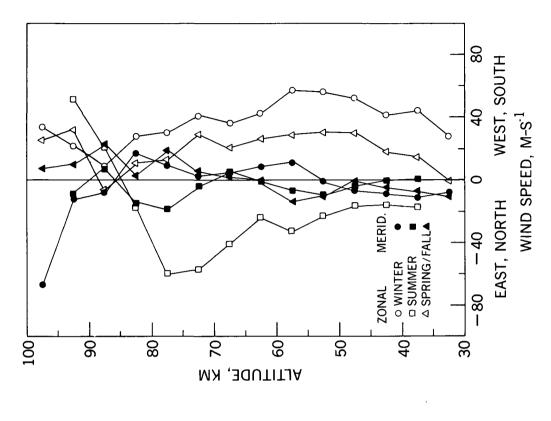
soundings.

based on 29 winter, 12 summer, and 13 transition soundings. (Stand-

ard is Reference 2.)

(59° N) based on 29 winter, 12 summer, and 13 transition Figure 4(a)-Mean seasonal temperature profiles for Churchill

TEMPERATURE, K



— WINTER -- SUMMER SPRING/FALL

8

2

АСТІТИРЕ, КМ

8

100

ard is Reference 2.)

based on 29 winter, 12 summer, and 13 transition soundings. (Stand-Figure 4(c)-Mean seasonal density profiles for Churchill (59° N)

PERCENT DIFFERENCE FROM STD.

40

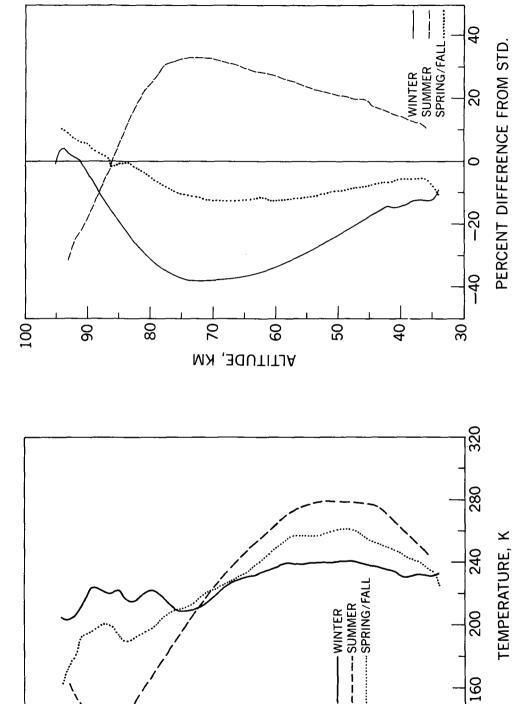
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Figure 4(d)–Mean seasonal wind components for Churchill (59 $^{\circ}$ N) based on 25 winter, 11 summer, and 13 transition soundings.

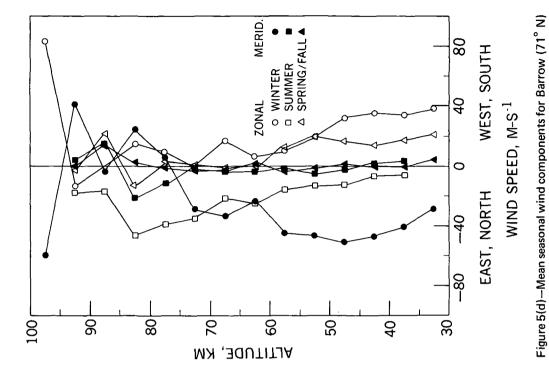


ALTITUDE, KM

Figure 5(a)—Mean seasonal temperature profiles for Barrow (71° N) based on 19 winter, 10 summer, and 17 transition soundings.

based on 19 winter, 10 summer, and 17 transition soundings. Figure 5(b)-Mean seasonal pressure profiles for Barrow (71° N)

(Standard is Reference 2.)



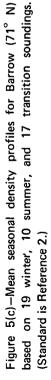
АСТІТОВЕ, КМ

based on 19 winter, 10 summer, and 17 transition soundings. (Standard is Reference 2.)

PERCENT DIFFERENCE FROM STD.

———SUMMERSPRING/FALI - WINTER

based on 19 winter, 10 summer, and 15 transition soundings.



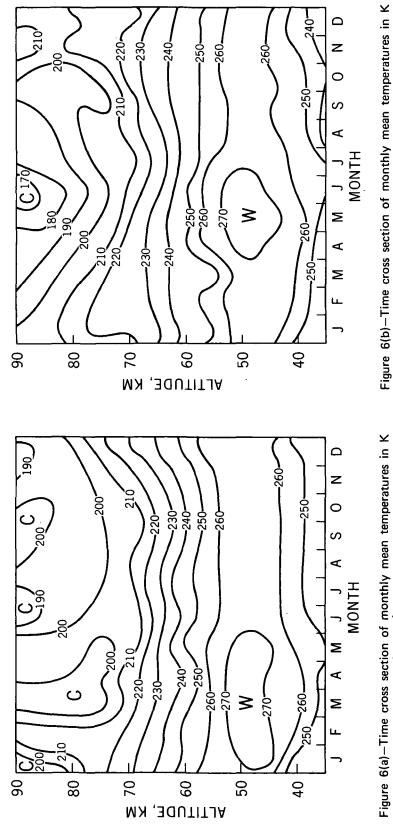
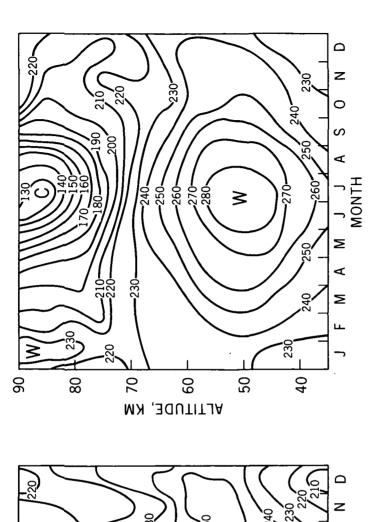


Figure 6(a)-Time cross section of monthly mean temperatures in K for Natal-Ascension (6° S to 8° S) based on 34 soundings.

for Wallops Island (38° N) based on 93 soundings.

14



160,1

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АСТІТИВЕ, КМ

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Figure 6(c)—Time cross section of monthly mean temperatures in K for Churchill (59° N) based on 54 soundings.

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MONTH

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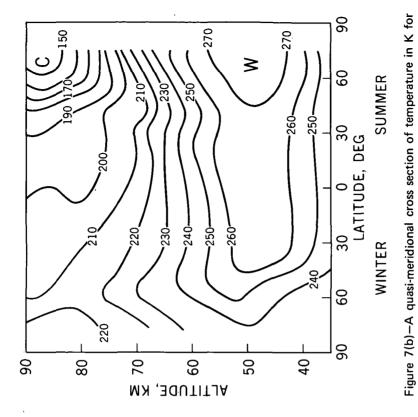
Figure 6(d)—Time cross section of monthly mean temperatures in K for Barrow (71° N) based on 46 soundings.

Figure 6(b), which shows the mean temperature cross section for Wallops Island, indicates a definite annual effect in the temperature structure. The maximum stratopause temperature occurs in the April through June period (late spring to early summer), and the lapse rates in the mesosphere vary considerably from January (1.4 K-km⁻¹) to July (2.5 K-km⁻¹). Also, there is a pronounced annual effect in the upper mesosphere, where the mesopause in summer is some 40 K colder than it is in winter. The strong temporal temperature changes, especially in the 70 to 80 km region in winter, are indicative of the seasonal effect that is observed over Wallops Island, which is absent from the low latitude results.

The mean temperature cross section for Churchill, shown in Figure 6(c), contains the same patterns that were present in the Wallops structure, but here, they are more pronounced. The mean monthly stratopause temperature varies by more than 30 K with season and reaches its warmest value in early summer. The mesopause temperature has a mean value of approximately 140 K in June through July, considerably colder than any temperatures found at lower latitudes. The annual temperature variation at the 90 km level is more than twice that observed at the stratopause, ranging from a minimum of 140 K in summer to 220 K in winter. Note that the average mesopause occurs at an altitude of almost 90 km in summer but is poorly defined in winter. The very strong changes in monthly mean temperatures at 80 km from spring to late summer occur at a time when the individual profiles are least variable, resulting from a rapid but orderly transition from the disturbed thermal structure of winter.

In the mean cross section for Barrow, given in Figure 6(d), the latitudinal trend mentioned earlier continues. The Barrow mean summer stratopause temperature is the warmest of all the sites, with a value of 280 K, whereas the mean winter stratopause is some 40 K colder. Note in Figures 6(a) through 6(d) that the time when the stratopause is warmest occurs later in the year with increasing latitude. The coldest temperatures observed in the earth's atmosphere are found at the summer mesopause, where a mean value of 130 K occurs in June. In contrast, the mean winter mesosphere above Barrow approaches an isothermal value near 235 K in January. The annual temperature variation at 85 km ranges from 130 K in summer to 230 K in winter, which makes it the largest seasonally induced change in the mixed region of the atmosphere (surface to 105 km). These mean profiles should be used only with due consideration of their standard deviations. For example, the summer mean profile is quite representative of its individual constituent profiles, while the winter mean is not representative of the atmosphere at any one given time due to the highly variable nature of the mesosphere in winter.

With the compilation of the seasonal mean profiles listed in Table 1, it is possible to produce quasi-meridional cross sections along a diagonal path traced across the North American continent from Barrow southeastward through Churchill and Wallops Island and across the western Atlantic Ocean to Natal, as shown in Figure 7(a). The resulting temperature cross section, given in Figure 7(b), forms an organized pattern dominated by the warm stratopause and cold mesopause of the high latitudes in summer and the almost isothermal structure of the high latitudes in winter. These features are, in general terms, similar to the earlier models of Murgatroyd (Reference 15) except that the high latitude summer stratopause and mesopause are colder than in Murgatroyd's model. Figure 7(b) is also similar to the cross section given in the "U.S. Standard Atmosphere Supplements, 1966" (Reference 3), except that the winter mesosphere shown here is colder than in Reference 3.



CHURCHILL

BARROW



mean winter, summer, and annual temperature values.

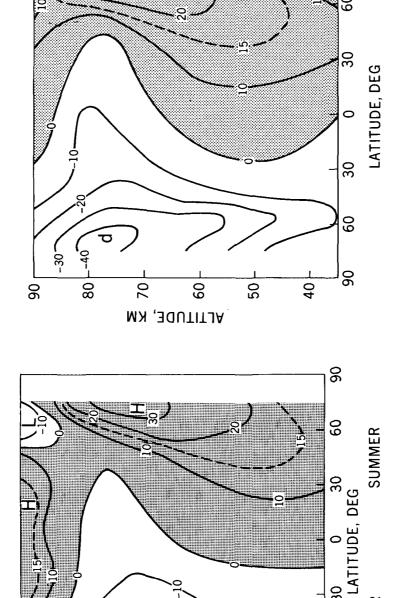


Figure 7(c)-A quasi-meridional cross section of pressure (as percent and annual pressure values.

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90

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WINTER

difference from Reference 2 atmosphere) for mean winter, summer,

Figure 7(d)-A quasi-meridional cross section of density (as percent difference from Reference 2 atmosphere) for mean winter, summer,

and annual density values.

8

90

80

70

9

АСТІТИРЕ, КМ

The combination of the mean seasonal pressure profiles into the same quasi-meridional cross section described above results in Figure 7(c). Here, the values are analyzed in percent difference from the "U.S. Standard Atmosphere, 1962" (Reference 2) reference profile for convenience. Note that the zero percent difference line (i.e., exact agreement with the standard model) is most nearly approximated by a low latitude pressure profile in winter, while a well developed low pressure region dominates the winter mesosphere and a high pressure region dominates the summer mesosphere. These differences, of course, drive the mean circulation in the mesosphere and are consistent with the observed winds, as will be shown later. The low pressure (cyclonic) region in the winter mesosphere underlies a high pressure (anticyclonic) region, and the high pressure region in the summer mesosphere underlies a low pressure region. This vertical alternation of pressure systems closely resembles the patterns observed in the troposphere, but the vertical scale sizes are much larger in the upper atmosphere. The relative sizes of the cyclonic and anticyclonic regions in the mesosphere probably result from the locations of the sampling sites with regard to the pressure systems rather than to the actual size of the systems. In other words, longitudinal variability is very important but cannot be evaluated from these data. The areas with the tightest horizontal pressure gradients, near 60 km at 45° N latitude in winter, for example, are the regions where the most intense zonal winds occur. This is again internally consistent with the observed winds.

Figure 7(d) is a quasi-meridional cross section of the mean density. Isopleths are drawn in percent difference from the standard density profile of Reference 2. The variation of density with season and latitude resembles the pressure pattern in Figure 7(c), with low densities over the winter pole and high densities over the summer pole at 80 km. The total annual change in density is approximately 70 percent at 75 km over Barrow (71° N), and obviously should be taken into account in any calculations involving the density in the mesosphere.

The large scale circulation of the mesosphere has not been well documented since relatively few observations of both wind and pressure (derived from temperature in most cases) have been made above 60 km. The circulation analyses presented here are based on the monthly and seasonal mean values from only four sites, and while they are useful to give only a gross picture of the upper stratosphere-mesosphere circulation over North America, they provide a considerable improvement in the circulation estimates based only on one or perhaps two stations.

Figures 8(a) through 8(h) present the time cross sections of zonal and meridional components deduced from the monthly mean winds at each of the four sites considered. The time cross section of mean zonal winds above Natal is given in Figure 8(a). The winds in the 35 to 70 km region are primarily westerly during the months of March through October, with a strong easterly jet of over 60 m-s⁻¹ at 45 km during December through February. A strong westerly core exceeding 60 m-s⁻¹ near 60 km occurs in February. While the westerly circulation dominates the upper stratosphere and lower mesosphere, the intensity of the flow is relatively weak, i.e., less than 40 m-s⁻¹. A distinct annual pattern is evident at all levels, but the pattern is not precisely defined due to sparse data coverage. Evidence of the quasi-biennial oscillation, if present, is probably masked because of the manner in which the data were averaged. The significance of this representation of the circulation is therefore reduced at altitudes where the quasi-biennial oscillation is important. The mean meridional components of the wind over Natal, given in Figure 8(b), contain only a couple of well-defined features: a northerly

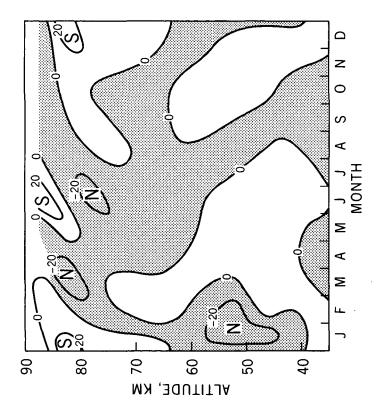
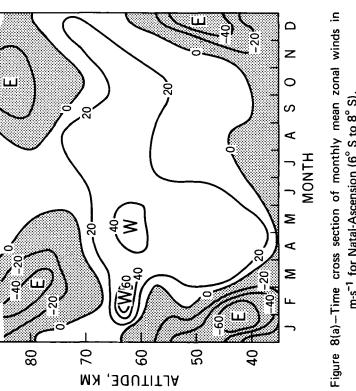
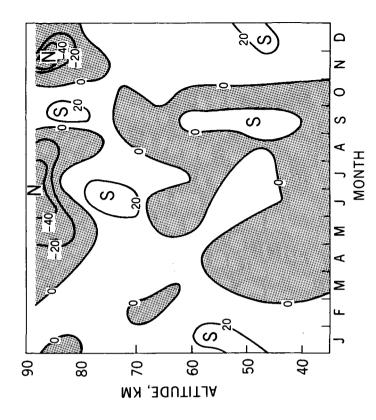


Figure 8(b)—Time cross section of monthly mean meridional winds in m-s⁻¹ for Natal-Ascension (6° S to 8° S).

m-s⁻¹ for Natal-Ascension (6° S to 8° S).





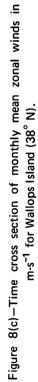


Figure 8(d)—Time cross section of monthly mean meridional winds in m-s^1 for Wallops Island (38 $^\circ$ N).

Щ_©) MONTH Σ 80 50 40 70 АСТІТИВЕ, КМ

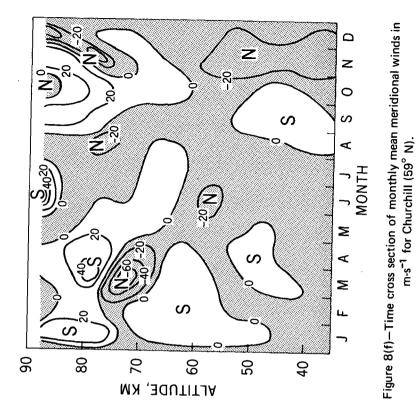


Figure 8(e)—Time cross section of monthly mean zonal winds in m·s⁻¹ for Churchill (59 $^\circ$ N).

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АГТІТОDE, КМ

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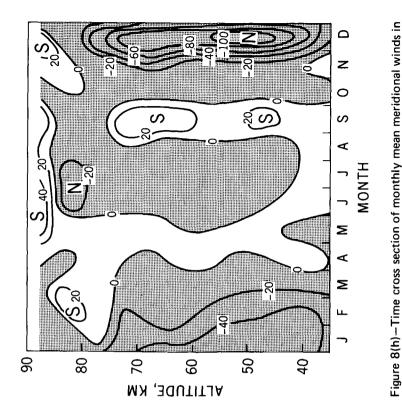
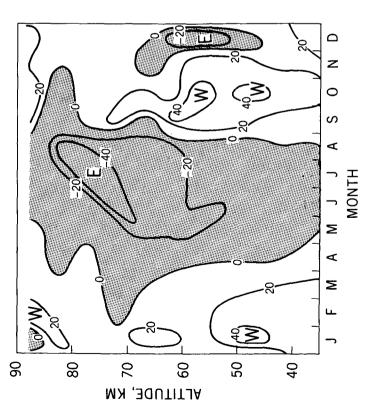


Figure 8(g)—Time cross section of monthly mean zonal winds in m-s⁻¹ for Barrow (71 $^{\circ}$ N).

m-s⁻¹ for Barrow (71° N).



component of over 20 m-s⁻¹ in February at the stratopause and a reversal in the winds approximately every 3 months above 80 km. The remainder of the meridional circulation is weak, and its significance is not clear.

Figure 8(c), which gives the mean zonal winds above Wallops Island, shows the distinct annual variation in the circulation. Strong westerly winds with peak speeds exceeding 90 m-s⁻¹ dominate the entire mesosphere during January when the flow is most intense. The westerlies gradually diminish during late winter so that by early spring, the flow direction reverses at upper levels first. The change to easterly flow is complete by late May. The easterly circulation develops to a maximum of over 60 m-s⁻¹ in June and July, then weakens until by September, westerly flow is reestablished.

The mean meridional winds over Wallops Island, shown in Figure 8(d), do not exhibit a strong seasonal pattern. In broad terms, they are predominately southerly during the winter months and generally northerly from March to October. Two intense northerly cores of over 40 m-s⁻¹ exist at the 85 to 90 km level in July and December, but elsewhere, the meridional wind speeds are light.

The zonal winds above Churchill, given in Figure 8(e), are characterized by two strong westerly jets in winter near 55 km, a maximum easterly flow in August at 75 km, and a strong annual cycle in the direction of the circulation. The westerly jet in March, which exceeds 100 m-s⁻¹ indicates that perhaps this flow might be in some way associated with the retreating mean position of the polar fronts in the troposphere and the jet stream at the tropopause. The short duration of the easterly regime is consistent with the abbreviated summer at these latitudes, and the more chaotic flow pattern in winter results from the generally disturbed structure of the mesosphere in winter.

Figure 8(f), which shows the mean meridional components of the Churchill circulation, is without a consistent pattern. The dominance of northerly components below 65 km, the strong northerly core of over 60 m-s⁻¹ which occurs in March at 70 km, and the sharply changing nature of the 85 to 90 km layer in November and December are noteworthy, however.

Figure 8(g) shows the mean zonal winds over Barrow. A seasonal dependence is obvious, although it is not as strong as in the Wallops and Churchill cases. The most prominent features include a moderate westerly flow in January and October, a moderate easterly circulation centered near 75 km in July, an abrupt reversal of flow direction in August, and the reappearance of easterly flow at 45 to 65 km in December. The position of Barrow with respect to the pressure systems makes it atypical of its latitude. The lack of an intense westerly flow in winter can be attributed to the fact that there are easterly components generated by the Aleutian Anticyclone even in January. These easterlies dominate the circulation in December in the lower mesosphere and probably contribute to the extended duration of easterly flow in summer.

The mean meridional winds above Barrow, given in figure 8(h), exhibit a reasonably consistent pattern with other nontropical sites except that the meridional circulation is very intense. Strong northerly components of up to 100 m-s⁻¹ dominate the December mesosphere. These northerly components also occur in January and February, when their vertical extent includes the entire mesosphere. A strong southerly flow above 85 km is observed from May until late September. The April to September period is marked by generally light meridional components, with northerly flow

prevailing in June, July, and August. Once again, the position of Barrow on the western edge of the North American continent, where it lies between the anticyclonic regime over the Gulf of Alaska and the cyclonic flow over the Arctic, probably accounts for this atypical behavior.

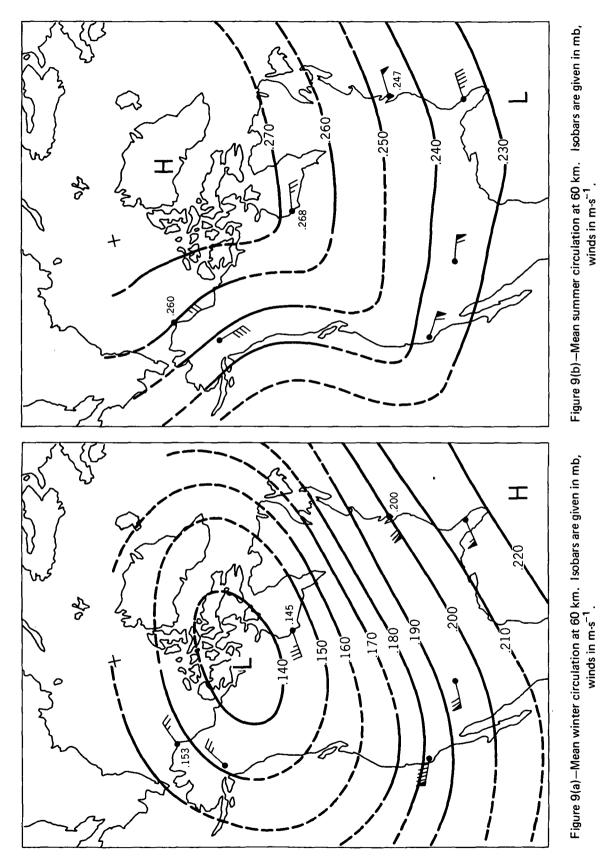
Figures 9(a) through 9(i) present the mean seasonal maps over the North American continent for the 60, 70, and 80 km levels. These maps are polar stereographic projections with the North Pole indicated by the X at the top center of each figure. Longitudes radiate from that point, and latitudes are concentric circles, the center of which is the pole. The maps were analyzed by plotting the mean wind and mean pressure for the appropriate level for each of the three sites previously mentioned. In addition, the mean data from the Meteorological Rocket Network (MRN) for January, July, and October were plotted in the winter, summer, and transition maps to aid in the analyses. Isobars were drawn at convenient intervals, but these intervals are consistent for a given level. (For example, the pressure gradients on the 70 km winter map can be compared with the pressure gradients on the 70 km summer map directly.) As the altitude increases, horizontal pressure gradients become weaker, necessitating the choice of smaller intervals of pressure to describe the flow at higher levels. These analyses are geostrophic, which means that the curvature of the isobars, friction, and all short term effects have been neglected. Most of these analyses have been published in Reference 14 but are included here because they constitute an integral part of the climatology of the mesosphere. The mean wind and pressure values given in Figures 2 through 5 were supplemented with data from Reference 16.

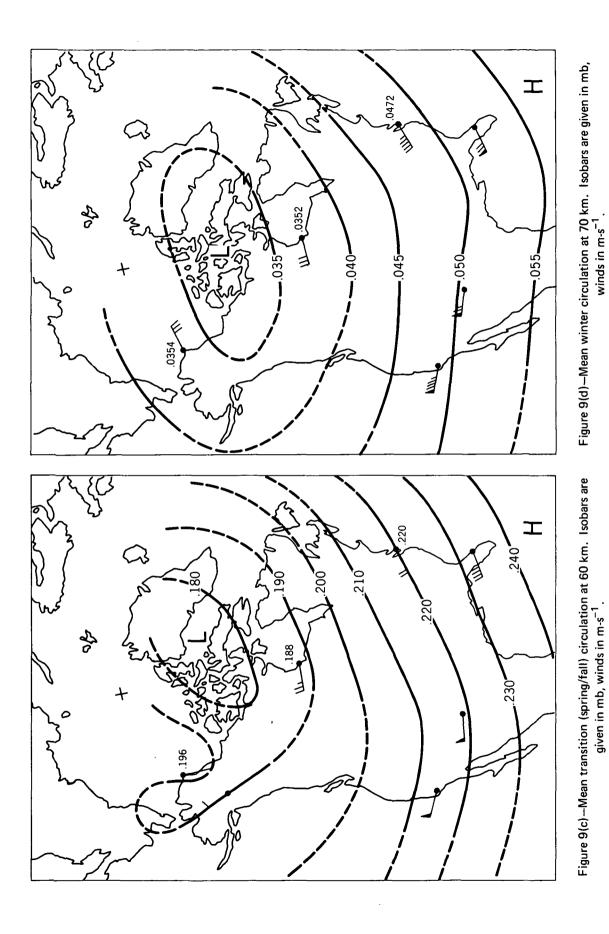
Figure 9(a), which gives the mean winter circulation at 60 km, indicates that the flow is dominated by a vortex centered over north central Canada, far from the geographic pole. This circulation produces strong westerly winds over most of the continent and a predominately northerly component over Alaska. If the analysis is accurate where broken lines are shown, strong southerly winds occur over Greenland. The polar asymmetry of the flow, then, provides a ready means for the transport of atmospheric properties across latitude circles. Note that in north central Canada, where the vortex center occurs, the pressure increases by a factor of almost two in summer, as shown in Figure 9(b).

The mean summer circulation at 60 km [Figure 9(b)] is dominated by an anticyclone to the north whose center cannot be determined from the available data. This pattern produces easterly winds over most of the continent, with the strongest zonal components occurring along the southern portion of the United States. The pressure gradients are smaller in magnitude in summer than in winter, producing generally lighter winds.

Figure 9(c), which gives the mean transition circulation at 60 km, indicates that a vortex drives the flow, but it is less intense than in winter. Wind speeds are everywhere lower, and an anticyclonic flow is indicated at Barrow. The mean pressures at all three stations during the transition months lie between the extremes of winter and summer.

The mean winter circulation at 70 km, which shows the presence of the vortex seen at lower levels, is given in Figure 9(d). Most of the discussion which applied at 60 km also applies at this level, so a detailed description is unnecessary. A significant difference is that the maximum winds observed at 70 km are not as intense as those observed at 60 km. There appears to be no symmetry over the pole at either level.





27

given in mb, winds in m-s⁻¹.

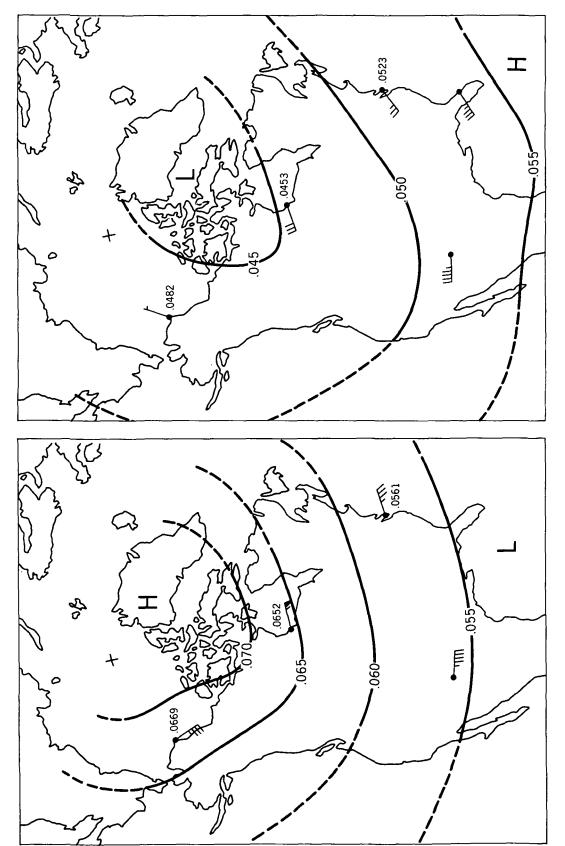
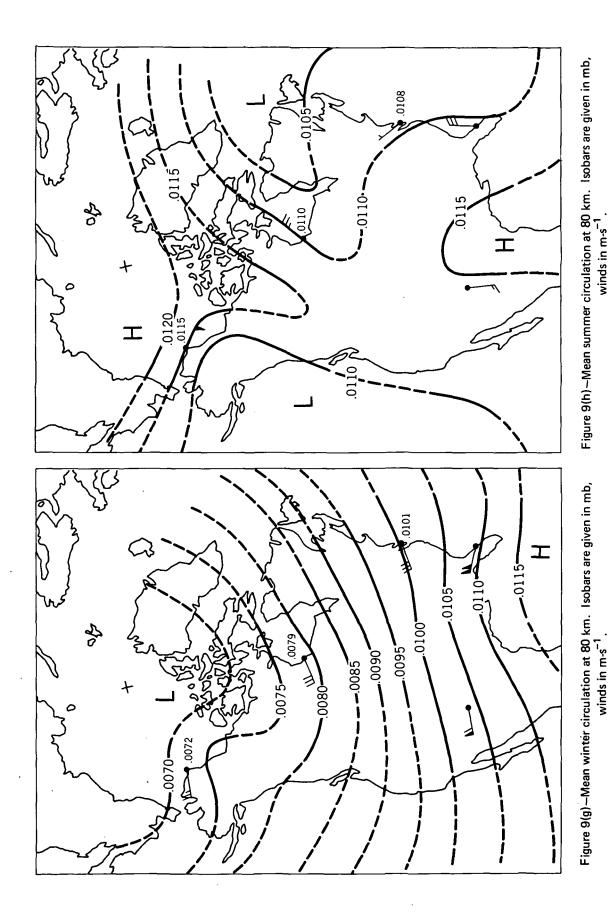


Figure 9(e) –Mean summer circulation at 70 km. Isobars are given in mb, Figur winds in $m \cdot s^{-1}$.

Figure 9(f)–Mean transition (spring/fall) circulation at 70 km. Isobars are given in mb, winds in m-s $^{-1}$.



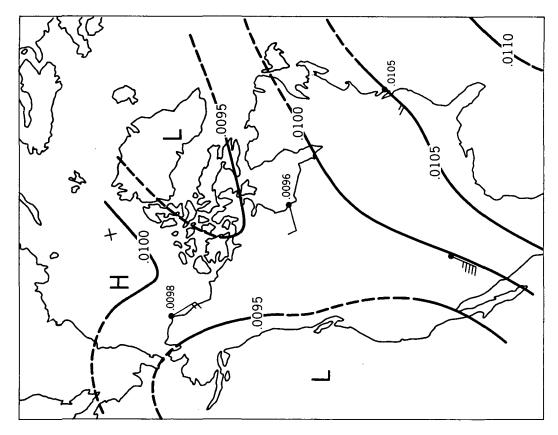


Figure 9(i)—Mean transition (spring/fall) circulation at 80 km. Isobars are given in mb, winds in $m \cdot s^{-1}$.

Figure 9(e) shows that the mean summer circulation at 70 km is dominated by the same anticyclone observed at 60 km in summer, and, as a result, easterly winds prevail over the entire North American continent. Again, the center of this high pressure system appears to be located south of the geographic pole.

A weak vortex governs the mean flow at 70 km during the months of transition, as shown in Figure 9(f). The circulation is predominately westerly, with light wind speeds north of Wallops and moderate speeds along the southern United States. Pressure values are higher than those observed in winter but below the summer values, as was the case at 60 km.

Figure 9(g) shows the mean winter circulation at 80 km. This coherent circulation is somewhat unexpected since the data from individual soundings fluctuate widely. The averaging process appears to filter out most of the amplitudes which are normally comparable to geostrophic considerations. The prevailing drift, in this case, the vortex generated westerlies, remains essentially intact. Even in this so-called mean flow, there is some indication that the effect of large fluctuations are not removed entirely. The ridging over eastern Alaska, which produces a southerly wind over Barrow, and the divergent flow between Wallops Island and Cape Kennedy are two good examples of such fluctuations.

The mean summer and transition circulations at 80 km, shown in Figures 9(h) and 9(i), represent vastly different circulations than were seen at lower levels. The high pressure region to the north of the continent still exists in summer, but ridging appears across the center of the continent in a north-south direction, producing a seemingly chaotic circulation. Low pressure regions extend onshore from both the Atlantic and Pacific Oceans, and the flow is generally light (except at Barrow in the summer). The transition circulation exhibits a mixture of features from the winter and summer regimes. It is presented only to demonstrate that the simple flow patterns no longer exist. The appearance of these maps may result from the breakdown of the geostrophic assumption at these altitudes. If tides and/or gravity waves dominate the flow, then large accelerations occur, and the geostrophic balance no longer applies. Averaging a sample of this small size may not adequately remove short term influences since the variability of the individual soundings about the mean is quite large. In any case, Figures 9(h) and 9(i) may not represent true mean circulations. Nevertheless, these analyses are included because they point out the problems that exist in determining the mean circulation at 80 km and above.

CONCLUSION

The data observed during the years 1960 through 1969 have been compiled into mean profiles of temperature, pressure, density, and wind for each of several sites representing various latitudes and climatic regimes. Cross sections and maps have been prepared from the mean data in the hope that these will be of some value to those interested in the mesosphere. While it is recognized that these analyses contain certain shortcomings, primarily the scarcity of data, they are presented as a first approximation to the real atmosphere to point out certain unrealistic features of the standard models.

ACKNOWLEDGMENT

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National Aeronautics and Space Administration
Greenbelt, Maryland, May 5, 1971
607-12-01-01-51

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Appendix A

The annual mean temperature, pressure, and density profiles for Natal-Ascension and seasonal mean profiles for Wallops Island, Churchill, and Barrow, along with the corresponding wind parameters and error analyses for temperature and wind, are tabulated in the following tables [comparisons are made with values from "U.S. Standard Atmosphere, 1962" (Reference 2)]:

Table	Station	Data	Page
A.1	Natal-Ascension	Annual	36
A.2(a)		Winter	38
A.2(b)	Wallops Island	Summer	40
A.2(c)	•	Spring/Fall	42
A.3(a)		Winter	44
A.3(b)	Churchill	Summer	46
A.3(c)		Spring/Fall	48
A.4(a)		Winter	50
A.4(b)	Barrow	Summer	52
A.4(c)		Spring/Fall	54

Table A.1.

ANNUAL MEAN PROFILE NATAL

ALTITUDE	**TE	EMPERATURE*	URE**	* * *	**PRE	****PRESSURE****	***	****	**DENS11Y*****	* * * * *	O _N
M MSL		DEG K			Z	W 05/			KG/CU M		OBS
	MEAN	ST DEV	PCT DIF	MEAN	S	T DEV	PCT DIF	MEAN	ST DEV	PCT DIF	
25000	218.1	5.3	-1.5	0.247E 0	ာ		-2.	0.3956-01		-1.3	m
26 000	223.6	3.9	4.0		9			0.331E-01			9
2 7000	230.8	6.0	3•2		0 (.368E 02		0.276E-01	0.534E-03		m
28000	235.3	1.3	4 • 0		· د			U-233E-01			m .
29000	36	7.0	, • •)			0.202E-01			M (
0000	23/00) ·	•)			0.1516101			9.0
32000	7.000	•	, ,		9 0		•	0.1275-01			n 4
33000	261.1		- e		· C		1 5	0.105-01			٠.
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37000	247.2	1 4	2.1		, =		. "	0.628F=02	0.236F-03		30
38000	250.1	-	2.2))	1 40	m	0.543E-02			31
39000	252.9	, 14	2.1			315	6	0.470E-02	0.181E-03		32
00000	255.6		2.1		0	16E	'n	0.406E-02	0.162E-03		33
41000	258.5	4.6	2•1		0			0.352E-02	0.142E-03		33
42000	261.1		2.0		0		4	0.306E-02	0.132E-03		9
43000	263.1		1.7		0		4	0.267E-02	0.113E-03		96
00044	265.0		1.3		0		4	0.233E-02	0.103E-03		34
45000	266.9		1.0		0		ē.	0.204E-02	0.925E-04		34
00097	268.2		0.5		0			0.179E-02	0.781E-04		34
4 7000	269.2		-0.1		_	483E 01	5.	0.157E=02	0.672E-04		34
00087	569.4		+0-		•	424E 01	5.	0.139E-02			34
49000	269.2		-0.5		_	396E 01	Š	0.122E-02			34
20000	268.4		-0. 8		_	348E 01		0.108E-02			33
51000	267.5		-1•1		_	16E	ŝ	0.9635-03		6.2	e .
52000	266.1		-1.6		_	97	.	0.853E-03	0.353E-04	9•9	e :
53000	264.6		8.1.			τς τ Τ	.	0.756E-03		. o	M
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7000	756.7		8		0	. H		0.465F-03	0.214E-04		9 60
58000	253.9		-2.2		9			0.412E-03	0.183E-04		9 (7)
59000	250.6	9	-2.7		0		2.	0.366E-03	0.161E-04		33
00009	247.0		13.4		02 0	.106E 01	2.	0.324E-03	0.155E-04	6.2	33
91000	243.3		-4.1		9		2.	0.287E-03	0.1436-04		33
95000	239.7		7.7-		0		-	0.254E-03	U-129E-04		33
93000	235.9	9•9	-4.5		o .		ċ	0.224E-03	0.112E-04		60
64000	232.7		6.4-		9 (•	0.197E-03	0.941E-05		m c
65000	229.5		0.4		o (.591E 00		0.1/2E=03		9 0	
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71000	209.4	۰۰	-2.9		0	ш		56E	<u> </u>	6.0	32
72000	207.0	4.6	-2.3		0		-4.3	0.652E-04	0.490E-05	-1.9	31
73000	204.5	œ	-1.6		0	3E		51E	띭	-2.9	31
74000	202 • 4	٥	8.0-		0	960	•	82E	띭	-3.8	31
75000	201.1	σ.	7.0		0	78E		4 10E-	Ä	-5.2	31
16000	199.8	0	8.1		0 (52E	*	350	W !	-6.2	31
77000	198.6	0:	3.2		o :		•	29 /E-	35	-7.2	16
78000	197.9	Ξ:	0 .	0.143E U	•	•120E 00		0.252E-04	0.185E-05	-8.3	90
79000	198•2	10.5	7.4	_	. 0	107E 00	•	12E-	3E-0	-9.5	30

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0.9638 0.9649 0.05649 0.05649 0.05648 0.05658 0.0349 0.	
0.865E 00 0.865E 00 0.525E 00 0.525E 00 0.317E 00 0.227E 00 0.165E 00 0.1160E	
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SPEED M/SEC MEAN	10.7 4.04 2.04 19.5 19.5	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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Table A.2(a).

SEASONAL MEAN PROFILE WALLOPS WINTER

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M MSL	ı	DEG K				M 05/18	٠	2 4 5	¥67.53 ₹07.53		200
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33000	233.4	•	1.0			0.939E 01	-5	0.107E-01	0.326E-03	-	ď
34000	236.7	•	1.2			0.274E 02	ņ	2E-02	0.420E-03	9.4-	10
35000	239.8	6.1	1.4			0.255E 02)E-02	0.361E-03	-	13
36000	243.7	•	. T			0.210E 02	e e	2E=02	0.312E-03		1
3 7000	248.0	•	7.0			0.180E 02		100	0.277E-03		9 5
0000	250.1	9 9	7.0	0.469E		0.163E 02	13.1	35-02	0.2075=03 =2	20.4	0 0
00004	253.0	4 6				0.135F 02	ì	F=02	0.180F-03		22
41000	255.1	0				0.122E 02		E-02	0.155E-03	. =	23
4 2000	256.4	4.6	0.5			0.115E 02	4-	55-02	0.141E-03	_	25
43000	260.0	9.1	0.0			0.110E 02	4	3E-02	0.128E-03	6.4	27
44000	262.6	9.1	4.0			0.103E 02	4	\$E-02	0.112E-03	1.4-7	28
4 5 0 0 0	265.0	9.6	0.3			0.948E 01	4-	Z0-31	0.107E-03	14.5	28
46000	267.3	11.0	0.1			0.863E 01	•	3E-02	0.102E-03	-4.3	28
4 7000	268.2	10.7	-0.5			0.783E 01	1	3E-02	0.955E-04	-3 •8	28
4 8 0 0 0	267.7	7.6	1.0			0.710E 01	14	7E-02	0.8485-04	-3.4	28
4 9000	266.0	7.5	-1.7			0.637E 01	•	E-02	0.764E-04	9.0	28
50000	264.0	7.6	-2.4			0.572E 01	4	E-02	0.721E-04	12.5	28
51000	262.2	0.6	-3.1			0.512E 01	5	7E-03	0.681E-04	15.	29
5.2000	260.7	4.6	-3.6			0.457E 01		E=03	0.5955.04	0.0	92
53000	259.0	4.6	3.8			0.409E 01	ė.	103	0.726E-04	200	B 6
54000	257.0	5.6	-3.9			U.366E UI	ė	103	0.4 rat = 04	0.7	D (
55000	254.9	10.4	0.7			0.326E 01		2E-03	0.44441	7 6	9 0
26000	251.9	10.6	5 · 5 ·			0.290E 01			10111111111111111111111111111111111111	n u	9 6
2 7000	249.0	9 6	1 I			0.234E 01	Ď		0111000		0 00
0000	244.46	0 6	0 0			0.1955 01	Ŷ		308E-0	9.4-	2 6
2000	27.2					1405 01			274F-0		28
0000	240.3	0 0	7 6 6			0.145E 01			0.246E-04	9.61	2 69
00024	7 4 6	4	10.			0.125F 01	-		217E-	8.9	2 8
63000	236.5	6.6	-4.2			0.106E 01	-12		190E-0	-8.2	28
94000	234.4	8.9	-3.5			0.913E 00	-12.		53E-0	4.6-	28
65000	232.5	9.1	-2.8			0.179E 00	-13.		40E-0	-10.5	28
00099	230.3	10.1	-2.1			0.667E 00	-13.6		25E-0	-11.5	28
67000	227.7	11.2	-1.5			0.573E 00	-13.		.106E-0	-12.2	28
68000	224.1	10.9	-1.4			0.495E 00	7		908E-0	-12.6	28
00069	221.2	10.4	-1.0			0.428E 00	-14.		- 794E-0	-13.1	58
10000	219.5	6.	0.0			0.367E 00	<u>.</u>		700F=0	1.4.1	80 6
71000	218.5	11.4	1.2			0.311E 00	7 7		0.6566.00	7.61	91
0002	2000	73.0	0.0			0.465E 00	•		00200	2 6	17
2000	220.1	1 u	10			1946	1		286F		- 10
75000	2000	7.6				0.1755 00	1		310F-0	-20.0	7.5
26000	210.0		11.3			0.142F 00	֡֝֟֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֓֓֓֓֡֓֓֡֓		260F=0	-20-2	7,0
77000	216.6	16.6	12.6			0.129F 00	101		208E-0	-19.8	54
78000	215.4	14.7	14.3			0.107E 00	-		172E-0	-18.9	21
79000	216.0	14.1	17.1			0.101E 00	•		0.1695-05	-18.8	19
80000	212.9	13.1	17.8			0.874E-01	-2		.154E-0	-16.6	18
R 1000	211.5	13.4	17.0			0.814E-01	-		.155E-0	-13.3	16
8 2000	210.7	14.0	16.6			0.701E-01	æ		34E-0	-10.6	16
83000	209.1	13.8	15.7		8	×	9		109E-0	-7.8	16
84000	205.8	15.5	13.9		8	0.530E-01	a o		.962E-0	14.1	16
85000	204.4	13.8	13.1		8	.514	ο :		. 705E-0	•	- .
86000	200.4	12.6	10.9	377E	8	0.464E-01	10.1		Ŏ.	80 ·	01
_	197.0	13.2	0.6	•316E	8	0.420E-01	10.7		0.649E=06	1.6	5

198.0	8.3		0.275E 00		15.8	0.484E-05	0.677E-06	S. 88	_
199.3	14.8		0.227E 00		15.3	0.401E-05	0.666E-06	5.2	•
204.1	22.0		0.193E 00		17.5	0.333E-05	0.600E-06	5.3	•
194.4	7.6	5.9	0.152E 00		11.1	0.273E-05	0.917E-07	5.1	~
194.4	7.8		0.128E 00		12.3	0.230E-05	0.750E-07	7.9	2
188.0	3.2		0.107E 00		12.4	0.199E-05	0.112E-07	13.3	2
182.4	0		0.890E-01		10.4	0.170E-05	00 30000	16.5	~
177.3	0		0.738E-01		9.6	0.145E-05	0.000E 00	19.8	_
172.1	0	•	0.612E-01	0.000E 00	9•9	0.124E-05	0.000E 00	23.0	_

88000 99000 91000 92000 94000 95000

SEASONAL MEAN PROFILE WALLOPS WINTER

NO OBS	11	22	27	56	27	52	27	54	35	58	91	7	-
ERROR SREES ST DEV	0.0	3.1	3.5	3.2	3.1	4.7	5.7	0.4	7.5	7.8	10.8	4.9	0,0
TEMP DEGE	1.4	2.8	5.6	5.9	2.7	3,3	3.6	2.9	4.6	5.1	6.5	4 • 8	10.0
NO OBS	iv s	, c o	01	11	10	01	80	10	14	12	٥	•	-
SOUTH ERROR M/SEC MEAN ST DEV	0.1	9.0	0.3	0.5	0.5	9.0	0.3	0.5	0.8	31.9	48.7	2.7	0.0
SOUTH MEAN	1.1	1.9	2.2	2.3	2.5	2.5	2.2	3.1	4.2	15.3	25.4	10.4	6.000
WEST ERROR M/SEC MEAN ST DEV	0.5	0	0.3	0.3	4.0	4.0	0.3	4.0	9•0	17.2	48.2	1.9	•
WEST M.	0.0	1.1	1.6	1.5	1.7	1.6	1.5	2.1	2 • B	9. 6	23.2	9.1	3 30 1
NO OBS	13	59	34	33	33	32	34	31	37	32	17	œ	•
DIRECTION DEGREES MEAN	263.9	258.9	258.9	259.1	255.4	262.7	269.9	261.7	262.3	279.3	242.8	355.3	71.6
SPEED M/SEC MEAN	38.6	57.8	66.7	6.99	65.4	68.3	9.99	44.3	65.2	27.3	8.2	0.44	0
SOUTH COMPONENT M/SEC MEAN ST DEV	11.8	14.8	18.1	19.6	20.6	25.2	26.4	24.2	46.3	50.3	62.2	130.2	
SOUTH MEAN	4 6	11.1	12.7	12.5	16.4	9.8	0.0	6.3	9.6	4.4	4.2	-43.8	,
COMPONENT M/SEC ST DEV	19.2	34.5	34.6	38.3	34.5	33.5	42.7	45.5	38.6	34.3	28.6	41.6	•
WEST C	38.4	56.7	65.5	65.7	63.3	67.7	9.99	43.8	9.49	26.9	8 • 2	3.5	000
17UDE MSL	0000	0000	5000	0000	2000	0000	2000	0000	5000	0000	5000	0000	000

Table A.2(b).

SEASONAL MEAN PROFILE WALLOPS SUMMER

1										•		
ALTITUDE M MS!	# *	**TEMPERATURE**	JRE**	*	*	**************************************	* * *	*	****	**************************************	***	2 6
	MEAN	ST DEV	PCT DIF	MEAN		ST DEV		PCT DIF	MEAN	ST DEV	PCT DIF	2
25000	223.0	2.0	9•0	0.273E	50		25	7.1	0.426E-01	0.694E-03		2
26000	223.9	1.4	9.0	0.234E	70		25	6•9	0.354E-01	0.546E-03		7
27000	223.9	0 0	0.0	0.204E	3 6	0.374E	2 5		0.317E-01	0.698E=03		en e
20002	226.8	3 6	0	0.151E	70		2.5	9 00	0.231E-01	0.390E-03		n m
30000	228.6	2.8	•	0.130E	70		25	8.6	0.198E-01	0.255E-03		m
31000	228.1	4.4	0.2	0.112E	70		22	8.9	0.171E-01	0.339E-03		m
32000	230.2	ي د د	•	0.968E	60		25	o	0.146E-01	0.385E-03		4
33000	234.3	2 6	4 0	0.856E	0 0		2 0	11.6	0.127E-01	0.439E-03	•	•
34000	730.0	9 6	•	0.444	9 6		7 6	12.0	0.0305.03	0.40/E=03	٠.	0 r
00066	2000	7.7	2 4	0.5675	9 6		4 0	13.0	0.8136-02	0.3445-03	٠,	~ a
0000	744.5	7.0	\ @ • •	0.496F	3 6		, .	14.6	0.7015-02	0.248E-03	٦-	0
38000	248.2	8 2	1.4	0.429E	0 0		2 2	13.9	0.602E-02	0.275E-03	• -	10
39000	252.4	6.2	1.9	0.375E	03		25	14.1	0.5176-02	0.268E-03	٠~	11
70000	255.2	6.1	1.9	0.325E	03		75	13.4	0.444E-02	0.245E-03	_	14
41000	258.1	7.1	2.0	0.284E	60		22	13.4	0.384E-02	0.225E-03	_	15
4 2000	261.1	8.6	2.0	0.250E	0.0		25	13.6	0.333E-02	0.202E-03	~	16
4 3000	263.2	6	1.7	0.219E	n 0		2 5	13.8	0.290E-02	0.177E-03	~	16
7 4000	264.1	4 0	- C	0.192E	n c		2 5	13.8	0.254E-02	0.138E-03	- 1 .	80 .
00004	1007	9 0		10 4 L - O	ີ ດ		3 5	14.4	0.1945-02	0.1096.03	٠,	77
2000	266.00	•	• 7	0.1305	9 6		3 5	7 - 7	20-1201-02	0.10901.0	٠,	3,4
00064	266.5	14.6	1.5	0.116E	9 6		: 5	13.8	0.152F-02	0.104F-03	15.7	74
00064	267.1	11.2	11.3	0.102E	20		15	13.6	0.133E-02	0.843E=04	15	54
50000	267.1	8•1	-1.3	0.905E	02		15	13.4	0.117E-02	0.781E-04	7	77
51000	266.7	0.9	-1.4	0.79BE	02		5	13.2	0.104E-02	0.770E-04	-	54
52000	265.7	6.3	-1.8	0.703E	02	0.598E	5	13.0	0.922E-03	0.760E-04	15•1	54
53000	264.0	ا م ع	2.0	0.619E	200		.	12.6	0.817E-03	0.710E-04	-	24
54003	262.2	œ .	0.2-	0.044	2 5	1694.0	7 6	12.3	0 . / Z4E-03	0.653E-04	-	24
0000	7000	e c	0 0	0.4.90	3 8		7 6	12.0	0.641E=03	0.5935-04	14.3	* (
15000	255.4			0.369E	200	3285	3 5	11.3	0.5045	0.483F=04	14.1	57
5000	251.9	10.2		0.323F	20	7725	: -		0.4475-03	0.427F=04	14.5	7 7
20006	248.3	9.6		0.282E	020		10	10.4	0.397E-03	0.369E-04	14.7	77
00009	244.6	9.6	-4.3	0.246E	0		10	7.6	0.351E-03	320E	14.9	54
61000	240.5	9.6	-5.2	0.214E	02		5	8 • 8	0.310E-03	76E	15.0	54
6.2000	236.7	4.6	-5.6	0.186E	05		ត :	7.9	0.274E-03	0.242E-04	14.6	54
90069	233.1	4 0	0 0	0.161E	2 6	0.136E	1 2	0, 0	0.241E-03	2 4	13•6	54
0000	225.0	0 0	0 u	0.1206	2 6		3 5	7	0.4446	9 7	9.71	\$ ¢
66000	222.6			0.103F	6		10	7 4	, C	1465	10.5	2 4
6 7000	219.4	7.0	-5.1	0.895E	010		20	0 • †	0.142E-03	134	8.6	23
68000	215.7	7.4	-5.1	0.76BE	010	0.64BE	8	3.1	24E	0.117E-04	8.9	23
69000	212.0	7.6	-5.1	0.656E	٥ ،		2	2.2	2 E	100	7.9	23
70000	208.4	8.4	-5.1	0.559E	01	1.1	2	1.4	36E	855	7.0	23
71000	205.6	7.6	L**1	0.476E	010		8	ر د د	37E	.742E-0	5.6	53
72000	203.9	70.7		1 to	5 6		3 2		, T	.623E-0	o. 1	23
7,000	203 • 3	10.6	7.7	0.3435			2 2	9 0	0.5885-04	0.2065-02	1•7	23
7 4000	503		•	37.70	3 3	3 7 7	3 6	• •	0 .	**************************************	0	, c
74000	202.2	10.4	• -	0.2105	3 5	1385	3 8	7 • • • • • • • • • • • • • • • • • • •	4 5	0.3545105	15.1	620
7,000	207.02	13.3	0	0.179E	; ;	1 11	3 8	1 4	10F	308F-0	13.7	77
78000	200 4	14.9		0.150E	;5	25.5	28	0	5.2E		1 4	20
79000	196.9	13.2	6.7	0.127E	:6	12	2 8		0.226E-04	0.173E-05	-3.5	16
	;		ŀ		j			1	:	,	· •	,

$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
11 10 10 10 10 10 10 10 10 10	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
0.148E 05 0.115E 05 0.116E 05 0.1109E 05 0.109E 05 0.645E 06 0.525E 06 0.300E 06 0.300E 07 0.300E 07 0.200E 07 0.201E 07	0.154E-07 0.134E-07 0.999E-08 0.999E-08 0.999E-08 0.099E-08 0.099E-08 0.099E-08
0.193E-04 0.165E-04 0.116E-04 0.996E-05 0.996E-05 0.697E-05 0.503E-05 0.503E-05 0.197E-05 0.170E-05 0.170E-05 0.170E-05 0.170E-05 0.170E-05 0.170E-05 0.170E-05 0.170E-05 0.170E-05 0.170E-05 0.170E-05 0.170E-05 0.170E-06	0.539E-07 0.539E-07 0.397E-07 0.312E-07 0.212E-07 0.239E-07 0.239E-07
######################################	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0.100E 0.9906E 0.694E 0.694E 0.611E 0.518E 0.518E 0.261E 0.261E 0.6162	0.1746-02 0.1606-02 0.1386-02 0.1306-02 0.1316-02 0.116-02 0.116-02 0.106-02
	90000000000000000000000000000000000000
	201020202020202020202020202020202020202
1989 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
8 8 10000 8 8 10000 8 8 10000 8 8 10000 9 10000 9 10000 9 10000 9 10000 9 10000 9 10000 100000	111000 112000 113000 114000 115000 116000 118000 120000

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE, 1962
SEASONAL MEAN PROFILE

WALLOPS SUMMER

NC OBS		e	7	12	11	16	13	16	15	16	11	12	=	6	
ERROR	ST DEV	0.3	0.	1:1	1.1	6.0	9.0	9.0	0.8	6.0	1.4	2.3	3.8	6.5	
TEMP	MEAN	0.7	0.8	6.0	1:0	1.0	0.9	0.8	1•1	1.1	1.6	5.6	4.4	8.9	
NO OBS		~	4	4	6	ď	4	'n	4	9	•	60	4	4	
SOUTH ERROR M/SEC	ST DEV	0.0	0.2	0.2	0.3	0.2	0.3	0.1	7.0	4.0	0.7	1.4	0.4	10.5	
SOUTH MX	MEAN	2.0	1.4	1.8	2.2	2.1	1.9	2.0	2.3	5.9	3.6	5.0	9.9	50.9	
ERROR	T DEV	0.0	0.2	0.2	4.0	0:1	0.2	0.5	0.1	9.0	6.0	0.7	2.5	5.1	
WEST ERROR M/SEC	MEANS	1.0	8	1:1	1.4	1.2	1.0	1.4	1.4	2.3	2.7	5.9	5.3	13.7	
NO OBS		6	10	16	17	23	18	22	50	21	22	17	15	11	
DIRECTION	MEAN	83.4	89.7	78.0	97.4	87.2	82.7	96.5	99.4	88.3	96.1	347.3	341.0	314.6	
SPEED M/SEC	MEAN	15.8	27.7	34.0	43.6	0.04	49.1	50.9	51.2	34.8	13.7	3.3	39.1	41.8	
SOUTH COMPONENT M/SEC	ST DEV	2.3	12.1	14.0	17.2	11.8	14.0	18.9	19.6	32.1	33.4	52.7	63.0	100.9	
SOUTH	MEAN	-1.7	-0-1	-7.0	5.6	-1.9	-6.2		4.0-	5.6	1.4	-3.2	-37.0	-29.3	
COMPONENT M/SEC	ST DEV	1.4	7.1	12.8	21.5	10.5	11.5	14.8	21.0	23.2	38.6	45.1	63.4	105.6	
	MEAN	-15.7	-27.7	-33.3	-43.2	-40.0	-48.7	-50.5	-51.2	-34.3	-13.6	0.7	12.7	29.7	
ALTITUDE M MSL		30000	35000	40000	45000	20000	55000	00009	9 5 0 0 0	20000	75000	80000	85003	00006	

SEASONAL MEAN PROFILE WALLOPS SPRING/FALE

MEAN STOCK Part MEAN STOCK MEAN	ALTITUDE	**	EMPERATURE**	URE**	* * * *	*PRESSURE*	****	***	******DENOITY*****	****	20
226 2.5	J 8 8		ST DEV	PCT	MEAN	ST DEV	ă	MEAN	ST DEV	t	i S
226.6 4.5 0.0 0.118E 0. 0.521E 02 -1.2 0.198E 02 0.521E 02 -1.8 0.188E-01 0.675E-02 226.1 3.1 2.3 0.908E 02 0.524E 02 1.8 0.134E-01 0.957E-02 226.1 3.1 2.3 0.692E 02 2.4 0.154E-01 0.957E-02 0.474E-02 226.1 5.0 2.5 0.692E 02 2.4 0.154E-03 0.957E-02 0.974E-03 226.1 6.0 3.1 0.659E 02 0.271E 02 2.4 0.154E-03 0.925E-02 0.974E-03 0.952E-02 0.975E-03	29000	228.3	0	1.2	•144E	0.000E		0.220E-01			-
230.7 3.7 1.4 0.9056 0.2 1.6 0.158E-01 0.657E-02 2.6 0.158E-01 0.657E-03 2.6 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.	30000	226.6	4.5	0.0	.118E	0.621E	•	0.181E-01			7
239.15 2.1 2.2 0.7060 0.3 0.3912 0.2 0.15 0.15 0.2 0.15 0.2	31000	230.7	F .	1.4	•104E	0.599E		0.158E-01			<i>e</i> 0 (
25.50 2.50	32000	235.8	- C	2.2	. 786F	0.3916		0.1346-01			*1 tr
24.2.5 5.6 2.5 0.01216 0.02716 0.01516 0.02716 0.01516 0.02716 0.01516 0.02716 0.01516 0.02716	000046	238.7	2.5	2.1	6 B O E	0.324E		0.992E=02			, 5
266.0 6.3 2.8 0.441E 03 0.237E 03 2.9 0.452E-02 0.497E-02 0.494E 03 0.237E 03 0.454E 03 0.237E 03 0.454E 03 0.234E 03 0.454E 03 0.234E 03 0.454E 03 0.234E 03 0.454E 03 0.244E 03 0.454E 03 0.2	35000	242.5	2.0	2.5	.593E	0.257E		0.852E-02			13
255.5 7.0 3.1 0.446E 03 0.234E 02 3.5 0.0542E-02 0.342E-02 2.545E-02 2.55.5 7.0 3.1 0.346E 03 0.234E 02 3.5 0.545E-02 0.346E-02 0.346E-0	36000	246.0	6.3	2 • 8	•512E	.0.271E		0.726E-02			19
255.2 8 6.7 3.2 0.390E 03 0.106E 02 3.5 0.465E-02 0.29XE-03 255.2 6.8 3.2 0.39XE-03 0.105E 02 4.7 0.465E-02 0.15EE-03 255.2 6.8 3.2 0.20XE 03 0.105E 02 4.7 0.465E-02 0.15EE-03 255.2 6.8 3.2 0.20XE 03 0.105E 02 4.7 0.465E-02 0.15EE-03 255.2 6.8 3.2 0.20XE 03 0.146E 02 4.4 0.255.2 6.0 1.5 EE-03 0.15EE-03 0.146E 02 4.5 0.25EE-02 0.15EE-03 255.2 7.4 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	37000	249.7	•	3.1	•446E	0.233E		0.623E-02			20
258.75 6.0 35.1 0.0301E 03 0.158E 02 4.7 0.0405F-02 0.105E-03 0.158E 02 4.5 0.205E-02 0.105E-03 0.105E 02 0.105E 03 0.158E 02 4.5 0.205E-02 0.105E-03 0.105E 03 0.	38000	252.8	•	m :	.390E	0.204E		0.537E-02			20
265.7 7.7 1.3 0.175E 03 0.137E 02 4.5 0.20E-02 0.13EE-03 0.15EE-03 0.13EE-03 0.13EE-03 0.13EE-03 0.13EE-03 0.13EE-03 0.13EE-03 0.13EE 03 0.13EE 02 4.5 0.20EE-02 0.13EE-03 0.13E	00066	2555	•	• •	241E	1405		0.4651.02			22
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265.4 7.8 -0.5 0.155E 03 0.118E 02 4.3 0.170E-02 0.118E-03 266.1 8.1 -1.5 0.120E 03 0.1018 02 4.3 0.170E-02 0.118E-03 266.1 8.1 -1.5 0.120E 03 0.1018 01 3.9 0.130E-03 0.120E-03 0.120E 03	44000	265.0	7.7		177E	0.132E		0.232E-02			34
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266.3 8.7 -2.6 0.6518 0.0 0.5645 0.1 2.5 0.652720.3 0.6138 0.4 266.3 0.5 266	51000	266.0	٠	-1.7	•724E	0.690E		0.947E-03		•	0 7
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256.2 8.7 -2.7 0.380E 02.409E 01 0.457E-03 0.505E-04 251.4.3 8.1 -2.8 0.234E 01 0.7 0.464E-03 0.466E-04 251.4.3 7.1 -3.3 0.255E 02 0.226E 01 0.7 0.404E-03 0.446E-04 249.0 7.1 -3.4 0.255E 02 0.221E 01 -0.6 0.347E-03 0.347E-04 243.6 5.1 -4.0 0.169E 02 0.221E 01 -1.1 0.245E-03 0.347E-04 241.6 4.5 -3.9 0.169E 02 0.171E 01 -1.1 0.245E-03 0.347E-04 241.6 4.5 -3.9 0.169E 02 0.171E 01 -1.1 0.245E-03 0.271E-04 0.27	55000	258.0	9.2	-2.8	.433E	0.457E		0.585E-03			0,4
254.3 8.1 -2.8	26000	256.2	8.7	-2.7	.380E	0.409E	-	0.517E-03			0 9
249.0 7.4 -3.3 0.225E 0.2 0.224E 0.1 -0.1 0.245E-0.3 0.347E-0.4 0.225E 0.1 -0.1 0.225E-0.3 0.347E-0.4 0.225E 0.1 -0.4 0.225E 0.1 -0.4 0.225E-0.3 0.347E-0.4 0.225E 0.1 -0.196E 0.1 -1.1 0.2245E-0.3 0.347E-0.4 0.196E 0.1 -1.2 0.225E-0.3 0.225E-0.4 0.225E-0.3 0.126E-0.3 0.225E-0.4 0.225E-0.3 0.126E-0.3 0.225E-0.4 0.225E-0.3 0.225E-0.4 0.225E-0.3 0.225E-0.4 0.225E-0.5 0.22	57000	254.3	 60 r	-2-8	.333E	0.366E	00	0.457E-03			9 0
246.4 6.0 -3.6 0.223E 02 0.252E 01 -0.6 0.315E-03 0.347E-04 0.246.6 6.0 -3.6 0.223E 01 -1.1 0.224E-03 0.347E-04 0.246.6 6.1 -4.0 0.194E 02 0.171E 01 -1.1 0.225E-03 0.347E-04 0.245E-03 0.245E-04 0.226E-04 0.245E-03 0.245E-04 0.245E-03 0.245E-04 0.245E-03 0.245E-04 0.245E-04 0.245E-03 0.245E-04 0.245E-04 0.245E-03 0.245E-04 0.245E-04 0.245E-03 0.245E-04 0.245E-04 0.245E-04 0.245E-03 0.245E-04 0.245E-05 0.440E-05 0.245E-04 0.245E-05 0.440E-05 0.	0000	240.0	7.4	13.0	2542E	0.0845	'	0.2575103			4 4
243.6 5.1 -4.0 0.194E 02 0.221E 01 -1.1 0.278E-03 0.304E-04 2318.8 5.1 -4.0 0.194E 02 0.196E 01 -1.8 0.258E-03 0.271E-04 2338.8 5.0 -1.9 0.116E 02 0.110E 01 -2.2 0.189E-03 0.271E-04 2338.8 5.0 -1.9 0.116E 02 0.110E 01 -2.2 0.189E-03 0.271E-04 2330.8 5.0 -1.9 0.181E 02 0.110E 01 -2.2 0.189E-03 0.191E-04 2230.8 5.0 -1.9 0.894E 01 0.184E 01 -2.9 0.166E-03 0.191E-04 2230.8 5.0 -1.9 0.894E 01 0.184E 01 -2.9 0.166E-03 0.191E-04 2230.8 7.5 0.1 0.894E 01 0.835E 00 -3.1 0.101E-03 0.191E-04 2230.8 7.5 0.1 0.894E 01 0.894E 00 -3.1 0.101E-04 0.127E-04 0.127E-05 0.147E 01 0.247E 01 0.245E 01 0.246E 01 0.226E 01 0.246E 01 0.226E 01	00004	7446	• •		223F	0.252E		0.3156.03			1 4
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238.8 5.0 -3.3 0.148E 02 0.171E 01 -1.8 0.215E-03 0.236E-04 233.3 4.7 -2.4 0.134E 02 0.150E 01 -2.2 0.186E-03 0.211E-04 233.3 4.7 -2.4 0.110E 0.204E 01 -2.6 0.146E-03 0.171E-04 230.8 5.0 -1.9 0.044E 01 0.114E 01 -2.6 0.146E-03 0.171E-04 226.0 6 0.74E 01 0.146E 01 0.156E-04 0.156E-04 226.0 6 0.74E 01 0.74E 00 01 0.156E-04 0.156E-04 221.2 8.6 0.6 0.74E 0 0.16E 0 0.156E-04 0.126E-04	62000	241.0	4.5	-3.9	.169E	0.196E		0.245E-03			3.5
235.1 4.6 -2.9 0.12RF 02 0.150E 01 -2.2 0.186E-03 0.211E-04 235.3 4.7 -2.4 0.111E 02 0.130E 01 -2.5 0.166E-03 0.191E-04 230.8 5.0 -1.9 0.984E 01 0.988E 00 -3.1 0.106E-03 0.193E-04 228.4 5.8 -1.2 0.884E 01 0.888E 00 -3.1 0.106E-03 0.158E-04 228.6 6.6 -0.6 0.716E 01 0.888E 00 -3.7 0.110E-03 0.158E-04 228.8 7.5 0.1 0.652E 01 0.885E 00 -3.8 0.962E-04 0.126E-04 221.2 8.6 0.6 0.6 0.716E 01 0.852E 00 -3.9 0.962E-04 0.128E-04 221.2 8.6 0.6 0.6 0.75E 01 0.646E 00 -3.9 0.628E-04 0.128E-04 0.128E-04 0.252E 01 0.646E 00 -3.9 0.628E-04 0.128E-04 0.252E 01 0.269E 02 0.266E-05 0.269E-04 0.266E-05 0.269E-04 0.269E-05 0.269E-04 0.269E-05 0.269E-04 0.269E-05 0.269E-04 0.269E-05 0.269E-04 0.269E-05 0.269E-04 0.269E-05 0.269E-	43 000	238.8	5.0	-3. 3	•148E	0.171E		0.215E-03			0,4
233.3 4.7 -2.4 0.111E 02 0.130E 01 -2.6 0.165E-03 0.191E-04 2230.8 5.0 -1.9 0.984E 01 0.988E 01 -2.9 0.165E-03 0.175E-03 0.175E-04 223.8 7.5 0.1 0.1 0.175E 00 -3.1 0.127E-03 0.175E-04 223.8 7.5 0.1 0.1 0.175E 00 -3.8 0.962E-04 0.128E-04 221.2 8.6 0.6 0.529E 01 0.614E 00 -4.0 0.836E-04 0.128E-04 0.128E-04 0.126E-04 0.126E-05 0.126E-04 0.126E-04 0.126E-05 0.126E-04 0.126E-05 0.126E-04 0.126E-05 0.126E-04 0.126E-05 0.126E-04 0.126E-05 0.126E-04 0.126E-04 0.126E-05 0.126E-04 0.126E-05 0.126E-04 0.126E-05 0.126E-04 0.126E-05	94000	236.1	4.6	-2.9	•128E	0.150E		0.189E-03			0,4
226.0 6.6 -0.6 0.834E 01 0.886E 00 -3.1 0.127E-03 0.155E-04 0.226.0 6.6 -0.6 0.617E 01 0.886E 00 -3.7 0.110E-03 0.155E-04 0.5121.2 8.6 0.6 0.657E 01 0.864E 00 -3.8 0.965E-04 0.105E-04 0.105E-04 0.521.2 8.6 0.6 0.654E 01 0.523E 00 -3.8 0.965E-04 0.929E-04 0.105E-04 0.105E-05 0.105E-04 0.105E-05 0.105E-04 0.105E-04 0.105E-05 0.105E-04 0.105E-04 0.105E-04 0.105E-05 0.105E-04 0.105E-04 0.105E-05 0.105E-04 0.105E-04 0.105E-04 0.105E-05 0.105E-04 0.105E-05 0.105E-04 0.105E-04 0.105E-05 0.105E-05 0.105E-04 0.105E-05 0.105E-05 0.105E-04 0.105E-05 0	65000	233.3	7 4	-2.4	•111E	0.130E		0.166E=03			3 0
226.0 6.6 -0.6 0.716E 01 0.836E 00 -3.7 0.110E-03 0.138E-04 223.8 7.5 0.1 0.617E 01 0.715E 00 -3.8 0.962E-04 0.122E-04 2213.8 7.5 0.1 0.617E 01 0.715E 00 -3.8 0.962E-04 0.122E-04 2218.9 9.8 1.4 0.454E 01 0.523E 00 -3.9 0.725E-04 0.122E-04 2218.9 9.8 1.4 0.454E 01 0.523E 00 -3.9 0.725E-04 0.928E-05 218.7 11.3 2.2 0.336E 01 0.446E 00 -3.4 0.526E-04 0.797E-05 210.5 12.2 3.1 0.242E 01 0.327E 00 -3.4 0.542E-04 0.598E-05 207.4 11.8 3.6 0.242E 01 0.226E 00 -2.6 0.408E-04 0.598E-05 207.4 11.8 3.6 0.242E 01 0.226E 00 -2.1 0.356E-04 0.472E-05 207.4 11.8 0.0147E 01 0.188E 00 -2.1 0.356E-04 0.354E-05 198.7 7.7 0.125E 01 0.185E 00 0.9 0.256E-04 0.256E-05 198.7 7.7 0.125E 01 0.999E-01 2.3 0.187E-04 0.187E-05 0.127E-05 0.	67000	228.4	• •	-1.2	.834E	0.988E		0.127E-03			1 4
223.8 7.5 0.1 0.617F 01 0.715F 00 -3.8 0.96ZE-04 0.12ZE-04 2218.9 8.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0	68000	226.0	•	9.0-	.716E	0.836E		0.110E-03			39
218.9 9.8 1.4 0.4529 01 0.645 00 -3.9 0.7255-04 0.9226-05 218.9 9.8 1.4 0.456 01 0.466 00 -3.7 0.628E-04 0.9226-05 218.9 12.2 2.8 0.338 01 0.446E 00 -3.7 0.628E-04 0.797E-05 213.9 12.2 2.8 0.338 01 0.346E 00 -3.4 0.542E-04 0.592E-05 213.9 12.2 2.8 0.337E 01 0.327E 00 -3.4 0.542E-04 0.592E-05 207.4 11.8 3.6 0.242E 01 0.226E 00 -2.6 0.408E-04 0.592E-05 207.4 11.8 3.6 0.242E 01 0.226E 00 -2.6 0.408E-04 0.592E-05 207.4 11.8 3.6 0.205E 01 0.226E 00 -2.1 0.352E-04 0.408E-05 199.8 13.1 6.0 0.174E 01 0.155E 00 -0.7 0.256E-04 0.354E-05 199.8 13.1 6.0 0.125E 01 0.155E 00 0.0 0.9 0.221E-04 0.286E-05 199.0 17.5 10.1 0.896E-01 0.996-01 2.3 0.187E-04 0.197E-05 0	69000	223 • 8	•	0.1	•617E	0.715E		0.962E-04			39
216.7 11.3 2.2 0.33E 01 0.546E 00 -3.7 0.628E-04 0.797E-05 213.9 12.2 2.8 0.33E 01 0.31E 00 -3.4 0.628E-04 0.797E-05 213.9 12.2 2.8 0.33E 01 0.31E 00 -3.4 0.628E-04 0.638E-05 207.4 11.8 3.6 0.269E 01 0.269E 00 -2.6 0.408E-04 0.598E-05 207.4 11.8 3.6 0.205E 01 0.269E 00 -2.6 0.408E-04 0.526E-05 199.8 13.1 6.0 0.174E 01 0.156E 00 -0.7 0.256E-04 0.357E-04 0.357E-05 199.8 13.1 6.0 0.125E 01 0.125E 01 0.075E-01 0.357E-04 0.358E-05 199.8 13.1 6.0 0.125E 01 0.125E 01 0.238E-01 0.238E-05 199.0 17.5 10.1 0.894E-01 4.2 0.138E-04 0.154E-05 0.156E-05 199.0 17.5 10.1 0.894E-01 4.2 0.138E-04 0.154E-05 0.154E-05 0.155E-05 0.156E-05 0	70000	221.2	9 ° 0	9•0	• 529E	0.614E		0.836E-04			00 (
213.9 12.2 2.8 0.333E 01 0.381E 00 -3.4 0.544E-04 0.6638E-05 20.4 12.2 2.8 0.284E 01 0.327E 00 -3.0 0.474E-04 0.598E-05 20.4 11.8 3.6 0.269E 01 0.226E 00 -2.6 0.408E-04 0.558E-05 20.4 11.8 3.6 0.205E 01 0.226E 00 -2.1 0.352E-04 0.471E-05 20.4 13.2 5.0 0.174E 01 0.185E 00 -2.1 0.352E-04 0.471E-05 199.8 13.1 6.0 0.125E 01 0.125E 00 0.0 0.9 0.221E-04 0.394E-05 199.8 13.1 6.0 0.125E 01 0.125E 01 0.256E-05 0.221E-04 0.286E-05 199.8 13.5 9.8 0.106E 01 0.996E-01 4.2 0.158E-04 0.158E-05 199.0 17.5 10.1 0.895E 00 0.694E-01 4.2 0.138E-04 0.154E-05 195.9 14.7 8.4 0.631E 00 0.517E-01 5.9 0.112E-04 0.123E-05	72000	216.7	, (4	3.89F	0.446E		0.6285-04			0 00
210.5 12.2 3.1 0.284E 01 0.337E 00 -3.0 0.472E-04 0.598E-05 20.4.6 11.8 3.6 0.2642E 01 0.266E 00 -2.6 0.4.08E-04 0.508E-05 20.4.6 12.2 4.3 0.208E 01 0.226E 00 -2.1 0.352E-04 0.410E-05 20.2.0 13.2 5.0 0.174E 01 0.188E 00 -1.5 0.302E-04 0.410E-05 199.8 13.1 6.0 0.147E 01 0.155E 00 -0.7 0.258E-04 0.410E-05 199.4 13.5 7.7 0.125E 01 0.150E 00 0.9 0.2 18E-04 0.354E-05 199.0 17.5 10.1 0.899E 00 0.854E-01 2.3 0.187E-04 0.189E-05 196.7 15.5 8.8 0.749E 00 0.619E-01 4.5 0.135E-04 0.154E-05 0.154E-05 195.9 14.7 8.4 0.631E 00 0.517E-01 5.9 0.112E-04 0.123E-05	73000	213.9	12.2	2.8	•333E	0.381E		0.544E-04			38
207.4 11.8 3.6 0.242E 01 0.269E 00 -2.6 0.404E-04 0.526E-05 204.66 12.2 4.3 0.205E 01 0.265E 00 -2.1 0.352E-04 0.471E-05 202.0 13.2 5.0 0.147E 01 0.188E 00 -1.5 0.302E-04 0.447E-05 199.8 13.1 6.0 0.147E 01 0.155E 00 -0.7 0.256E-04 0.346E-05 198.4 13.5 7.7 0.125E 01 0.120E 00 0.9 0.256E-04 0.354E-05 198.4 13.5 9.8 0.106E 01 0.999E-01 2.3 0.187E-04 0.187E-05 199.0 17.5 10.1 0.899E-01 4.2 0.158E-04 0.189E-05 196.7 15.5 8.8 0.749E 00 0.619E-01 4.5 0.132E-04 0.123E-05 195.9 14.7 8.4 0.631E 00 0.517E-01 5.9 0.112E-04 0.123E-05	74000	210.5	12.2	3.1	•284E	0.327E		0.472E-04			38
202.0 13.2 5.0 0.147E 01 0.155E 00 -1.5 0.302E-04 0.447E[-05 199.8 13.1 6.0 0.147E 01 0.155E 00 -0.7 0.256E-04 0.4416E[-05 198.7 12.7 7.7 0.125E 01 0.120E 00 0.9 0.9 0.256E-04 0.354E[-05 198.4 13.5 9.8 0.106E 01 0.999E-01 2.3 0.187E[-04 0.288E[-05 199.0 17.5 10.1 0.899E[-01 4.2 0.158E[-04 0.189E[-05 196.7 15.5 8.8 0.749E[-01 4.5 0.158E[-04 0.158E[-05 195.9]]]] 0.631E 00 0.617E[-01 5.9 0.112E[-04 0.123E[-05 0.123E[-05 0.123E]]]	75000	207.4	11.9	9.0	.242E	0.269E		0.408E-04			96
199.8 13.1 6.0 0.147E 01 0.155E 00 -0.7 0.256E-04 0.354E-05 199.8 13.1 6.0 0.125E 01 0.120E 00 0.9 0.221E-04 0.236E-05 199.4 13.5 9.8 0.106E 01 0.999E-01 2.3 0.187E-04 0.219E-05 199.0 17.5 10.1 0.899E 00 0.884E-01 4.2 0.158E-04 0.198E-05 196.7 15.5 8.8 0.749E 00 0.619E-01 4.5 0.135E-04 0.154E-05 195.9 14.7 8.4 0.631E 00 0.517E-01 5.9 0.112E-04 0.123E-05	72000	204-0	19.3	4 դ	174F	0.1885		0.3025-04			9 6
9000 198.7 12.7 7.7 0.125E 01 0.120E 03 0.9 0.221E-04 0.288E-05 0000 198.7 12.7 7.7 0.125E 01 0.120E 03 0.9 0.221E-04 0.288E-05 0000 199.4 13.5 9.8 0.106E 01 0.089E-01 4.2 0.136E-04 0.189E-05 0000 196.7 15.5 8.8 0.749E 00 0.019E-01 4.5 0.138E-04 0.154E-05 0.106E-05 0.106E-05 0.112E-04 0.125E-05	7,8000	100	13.1		14.75	0.155		0.2585-04			9 60
0000 199.4 13.5 9.8 0.106E 01 0.999E-01 2.3 0.187E-04 0.219E-05 1000 199.0 17.5 10.1 0.899E 00 0.854E-01 4.2 0.158E-04 0.189E-05 2000 196.7 15.5 8.8 0.749E 00 0.619E-01 4.5 0.133E-04 0.154E-05 3000 195.9 14.7 8.4 0.631E 00 0.517E-01 5.9 0.112E-04 0.123E-05	20000	198.7	12.7	7.7	.125E	0.120E		0.221E-04			9 6
1000 199.0 17.5 10.1 0.899E 00 0.854E-01 4.2 0.158E-04 0.189E-05 -4. 2000 196.7 15.5 8.8 0.749E 00 0.619F-01 4.5 0.133E-04 0.154E-05 -3. 3000 195.9 14.7 8.4 0.631E 00 0.517E-01 5.9 0.112E-04 0.123E-05 -1.	80000	198.4	13.5	6.0	.106E	0.999E-	7	0.187E-04	0.219E-0	-6.3	
2000 196.7 15.5 8.8 0.749E 00 0.619E-01 4.5 0.133E-04 0.154E-05 3000 195.9 14.7 8.4 0.631E 00 0.517E-01 5.9 0.112E-04 0.123E-05 .	91000	199.0	17.5	10.1	9668•	0.854E-	4	0.158E-04	0.189E-0	7.4-	34
3000 195.9 14.7 8.4 0.631E 00 0.51/E-01 5.9 0.112E-04 0.123E-05 .	82000	196.7	15.5	8 • 8	3647.	0.619E	*	0.1335-04	0.154E-0	13.3	32
	83000	195.9	14.7	4.8	.631E	0.517E	ın.	0.112E-04	0.123E-0	-1.7	35

SEASONAL MEAN PROFILE WALLOPS SPRING/FALL

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE, 1962

NO OBS		7	10	16	58	37	30	36	32	33	35	35	35	38	20
ERROR SREES	ST DEV	0.0	0.2	1.3	1.7	2.3	2.2	1 • 6	1.9	2.7	2.5	2.1	3.8	5.0	12.0
TEMP	MEAN	1.0	9.0	1.0	1.3	1.8	1.9	1.6	1.8	2.3	1.9	1.7	2.9	4.8	8.8
NO OBS		0	m	5	5	o	2	90	7	60	10	7	6 0	o	-
SOUTH ERROR M/SEC	ST DEV	0.0	0.2	0.3	0.5	0.2	0.3	1.0	43.2	71.6	81.5	1.4	5.6	2.2	76.1
SOUTH	MEAN	0.0	6.0	1.1	1.6	2.0	2.2	2.8	50.4	0.44	43.1	4.0	7.1	7.6	56.6
WEST ERROR M/SEC	T DEV	0.0	0	0.2	0.3	0.2	0.2	0.5	14.1	73.1	49.8	6.0	1.6	2.0	76.8
wEST ₹	MEAN			0.7											
NO OBS		-	12	18	38	45	40	9 7	43	45	40	42	42	44	22
DIRECTION DEGREES	MEAN	93.0	286.2	292.4	276.2	272.47	270.8	261.2	267.6	251.9	265.8	245.6	263.6	350.6	356.5
SPEED M/SEC	MEAN	18.9	4.7	15.7	24.1	28.4	28.2	23.8	19.0	19•1	21.1	2•0	15.7	10.5	5.3
SOUTH COMPONENT M/SEC	ST DEV	0.0	3.3	6.3	8.6	11.4	12.7	21.4	16.4	19.2	20.4	30.5	50.3	63.5	78.5
SOUTH	MEAN	1.0	-1.3	0.9-	-2.6	-1.3	7.0-	3.6	0.7	5.9	1.5	0.9	1.7	-10.4	15.3
COMPONENT M/SEC	ST DEV	0.0	10.7	17.7	23.8	31.3	31.6	33.0	36.6	38.4	36.B	42.1	34.9	45.5	56.0
WEST CO	MEAN	-18.9	4.5	14.5	24.0	28.3	28.2	23.5	19.0	18.2	21.0	1.8	15.6	1.7	0
ALTITUDE M MSL		25000	30000	35000	40000	4 5 0 0 0	20000	55000	00009	65000	70000	75000	90000	85000	00006

Table A.3(a).

SEASONAL MEAN PROFILE

Fig. 10 Fig.										
STORY POT DIEST NEAR NEA	ALTITUDE **	TEMPERAT	URE**		*PRESSURE***	*	* *	*DENSITY**	****	S
10.0 1.0	MEAN	STE	PCT D1	MEAN	NT/SO M ST DEV	5	MEAN	ST 0		085
4.0 7.8 8 0.1122 C 0. 0.1026 C 2. 19.7 0.106F-01 0.6456-03 110.4 0. 10.8 1.0 0.1022 C 0. 0.1026 C 0. 19.7 0.106F-01 0.1026-03 110.4 0. 19.8 0.1026 C 0. 0.1026 C 0	6000 203.		œ l	õ	0.350E 02	-17.5	3606.	0.106E-02	0	2
1.0 1.0			8	52E	0.169E	-18.7	.261E	0.806E-03	-10	~
1.0 1.0	206			2 d	0.1295	1.941	• 218t	0.6456-03	-12	,
2.5	203		. 4	7 17	0.5176	121.0	1546	0.205F-03	1 4	1 1
2.5	212.		9	9 E	0.424E	-22.5	1316	0.1896-03	-17	t 1
2.2 -6.7 0.55EE 03 0.126FE 02 -20.8 0.1409E-02 0.4499E-02 0.4499E-03 -1151.0 0.55EE 03 0.328FE 02 -20.8 0.1409E-02 0.4499E-03 -1151.0 0.55EE 03 0.328FE 03 0.328FE 02 -20.8 0.51EF-02 0.4499E-03 -1151.0 0.528FE 03 0.328FE	213.		9-	32E	0.223E	-23.2	• 111E	0.153E-03	87	. 1
3.6 -8.1 0.516F 03 0.208F 02 -22.0 0.538F 02 0.455F 03 -155.1 9.7 -8.6 0.208F 03 0.308F 02 -22.5 0.558F 02 0.455F 03 -12.0 10.7 -8.6 0.208F 03 0.308F 02 -22.5 0.548F 02 0.455F 03 -12.0 10.7 -8.6 0.208F 03 0.208F 02 -22.5 0.548F 02 0.238F 03 -12.0 10.8 0.208F 03 0.208F 02 -22.5 0.548F 02 0.238F 03 -12.0 10.9 0.208F 03 0.208F 02 -22.5 0.548F 02 0.238F 03 -12.0 10.0 0.208F 03 0.208F 02 -22.5 0.548F 02 0.238F 03 -12.0 10.0 0.208F 03 0.208F 02 -22.5 0.548F 03 0.238F 03 -12.0 10.0 0.208F 03 0.208F 03 -22.5 0.238F 03 0.238F 03 -12.0 10.0 0.208F 03 0.208F 03 -22.5 0.238F 03 0.238F 03 -12.0 10.0 0.208F 03 0.208F 03 -22.5 0.238F 03 0.238F 03 -12.0 10.0 0.208F 03 0.208F 03 -22.5 0.238F 03 0.238F 03 -22.0 10.0 0.208F 03 0.238F 03 -22.5 0.238F 03 0.238F 03 -22.0 10.0 0.208F 03 0.238F 03 -22.5 0.238F 03 0.238F 03 -22.0 10.0 0.208F 03 0.238F 03 -22.5 0.238F 03 0.238F 03 -22.0 10.0 0.208F 03 0.238F 03 -22.5 0.238F 03 0.238F 03 -22.0 10.0 0.208F 03 0.238F 03 -22.5 0.238F 03 0.238F 03 -22.0 10.0 0.208F 03 0.238F 03 -22.5 0.238F 03 0.238F 03 -22.0 10.0 0.208F 03 0.238F 03 0.238F 03 0.238F 03 0.238F 03 -22.0 10.0 0.208F 03 0.238F 03 0.238F 03 0.238F 03 0.238F 03 0.238F 03 -22.0 10.0 0.208F 03 0.238F 03 0.23	215		-6-	3.2E	0.199E	-24.1	*941E	0.101E-03	138	4
7.2 -7.9 0.6454E 03 0.334E 02 -20.48 0.777E02 0.455E-03 -14.0 0.77 -8.4 0.239E 03 0.234E 02 -21.5 0.555E-02 0.334E-03 -14.0 0.77 -8.4 0.239E 03 0.237E 02 -23.5 0.355E-02 0.334E-03 -14.0 0.239E 03 0.200E 02 -23.5 0.359E-02 0.234E-03 -17.5 0.1006 -8.4 0.231E 03 0.200E 02 -24.0 0.235E-02 0.234E-03 -17.5 0.1006 -9.3 0.200E 02 -24.0 0.235E-02 0.234E-03 -17.5 0.1006 03 0.200E 02 -24.0 0.235E-02 0.236E-03 -17.5 0.1006 03 0.200E 02 -24.0 0.235E-02 0.236E-03 -17.5 0.1006 03 0.200E 02 -24.0 0.235E-02 0.236E-03 -17.5 0.1006 03 0.200E 02 -25.0 0.216E-02 0.236E-03 -17.5 0.1006 03 0.200E 02 -25.0 0.216E-02 0.100E-03 -17.5 0.1006 03 0.100E 02 -25.0 0.110E-02 0.100E-03 -18.5 0.1006 03 0.100E 02 -25.0 0.110E-02 0.100E-03 -20.5 0.1006 03 0.100E 02 -25.0 0.110E-02 0.100E-03 -20.5 0.1006 03 0.100E 02 0.100E 02 -20.6 0.1006 03 0.100E 02 0.100E 02 -20.6 0.1006 03 0.100E 02 0.100E 02 0.100E-03 -20.0 0.1006 03 0.100E 02 0.100E 02 0.100E-03 -20.0 0.1006 03 0.100E 02 0.000E 03 0.100E-03 -20.0 0.1006 03 0.100E 02 0.000E 03 0.100E-03 -20.0 0.1006 03 0.100E 02 0.000E 03 0.000E-04 -20.0 0.1006 03 0.000E 03 0.000E-03 -20.0 0.1006 03 0.000E 03 0.000E-03 -20.0 0.1006 03 0.000E	214.		-8	1 9 E	0.268E	-22.0	•338E	0.489E-03	-15	90
9.9	217.		-	345	0.318E	8-02-	•727E	0.462E-03	17	13
1.0. 1.0.	218		00 c	356	0.304E	-20.¢	•631E	0.465E-03	77	17
10.0.7 -8.6. 0.2.51E 0.0.20EE 0.2.25.5 0.386E-0.2 0.2.28E-0.3 11.1.5 11.8	223		0 q	77.0	0.230E	127.5	1000	0.329E-03	1 .	
10.0 -8.3 0.216E 03 0.18BE 02 -2444 0.235F=02 0.238E-03 -17.5 11.9 -8.0 0.106E 03 0.19BE 02 -24.2 0.246F=02 0.238E-03 -17.5 11.9 -8.0 0.106E 03 0.19E 02 -24.2 0.246F=02 0.238E-03 -17.5 11.3 -7.4 0.109E 03 0.136E 02 -25.6 0.18BE-02 0.186E-03 -19.5 14.7 -7.5 0.125E 02 0.136E 02 -25.6 0.18BE-02 0.18FE-02 -19.5 14.7 -7.5 0.125E 02 0.126E 02 -27.3 0.136F=02 0.18FE-03 -19.5 14.7 -7.5 0.125E 02 0.126E 02 -27.3 0.136F=02 0.18FE-03 -19.5 14.7 -7.5 0.125E 02 0.126E 02 -27.3 0.136F=02 0.18FE-03 -22.2 15.5 -7.6 0.126E 02 0.126E 02 -28.8 0.116F=02 0.126E 03 -22.2 15.5 -7.6 0.126E 02 0.136E 01 -28.7 0.18FE-03 0.126E-04 -22.2 15.5 -7.6 0.126E 02 0.178E 01 -28.7 0.18FE-03 0.126E-04 -22.2 15.5 -7.6 0.126E 02 0.178E 01 -28.7 0.126F=03 0.126E-04 -22.2 15.5 -7.6 0.126E 02 0.178E 01 -33.6 0.176E-03 0.126E-04 -22.2 15.5 -7.5 0.126E 02 0.178E 01 -33.6 0.176E-03 0.126E-04 -22.2 15.5 -7.5 0.126E 02 0.126E 01 -33.6 0.126E-03 0.126E-04 -22.2 15.5 -7.5 0.126E 02 0.126E 01 -33.6 0.126E-03 0.126E-04 -22.2 15.5 -7.5 0.126E 02 0.126E 01 -33.6 0.126E-03 0.126E-04 -22.2 15.5 -7.5 0.126E 02 0.126E 01 -33.6 0.126E-03 0.126E-04 -22.2 15.5 -7.5 0.126E 02 0.126E 0.1 -33.6 0.126E-03 0.126E-04 -32.6 15.5 -7.5 0.126E 02 0.126E 0.1 -34.5 0.126E-03 0.126E-04 -32.6 15.5 -7.5 0.126E 02 0.126E 0.1 -34.5 0.126E-03 0.126E-04 -32.6 15.5 -7.5 0.126E 02 0.126E 0.1 -34.5 0.126E-03 0.126E-04 -32.6 15.5 -7.5 0.126E 0.1 -34.5 0.126E-03 0.126E-04	226.0		800) E	0.206E	-23.5	•386E	0.283E-03	19	161
11.3	229		8	391	0.183E	-24.4	•329E	0.238E-03	-17	20
11.6	232 •		-7	306	0.205E	-24.0	•285E	0.243E-03	-17	22
1.24	235		œ I	96E	0.193E	-24.2	• 245E	0.229E-03	-17.	56
1.3. -7.4 0.109E 0.3 0.136E 0.2 -25.6 0.136E 0.2 -25.6 0.136E 0.2 -21.4 0.136E 0.3 0.136E 0.2 -25.6 0.136E 0.2 -21.4 0.136E 0.3 0.136E 0			1	1 to	C.168t	25.0	•211E	0.200E-03	8 7	80 0
1.5. 1.5.	2410		1	יו היי	0-1345	-26.6	1555	0.1686103	7 7	8 6
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13.6	250			± 9E	0.388E	-33.6	•348E	0.538E-04	-30	58
12.6	249			. E	0.342E	*34.1	-305E	0.476E-04	-30	53
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13.0	24047			u u.	0.22PF	, c	200F	0.3485-04		200
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12.9	240			7 E	0.147E	-36.4	•139E	0.242E-04	100	50
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0.159E-05 0.132E-05 0.120E-05 0.101E-05	0.744E-06 0.701E-06 0.571E-06 0.498E-06 0.347E-06	0.298E-06 0.176E-06 0.147E-06 0.142E-06 0.124E-06	0.662E-07 0.643E-07 0.486E-07 0.460E-07	0.472E-07 0.451E-07 0.231E-07 0.140E-07 0.103E-07 0.785E-08	0.152E.07 0.625E.00 0.625E.00 0.237EE.00 0.288E.00 0.238E.00 0.224E.00 0.224E.00
0.110E-04 0.947E-05 0.812E-05 0.705E-05	0.523E105 0.328E105 0.328E105 0.228E105	0.128E-05 0.192E-05 0.165E-05 0.121E-05 0.121E-05	0.888E-00 0.753E-00 0.5540E-00 0.5540E-00 0.5540E-00	0.374E-06 0.310E-06 0.254E-06 0.2256-06 0.193E-06 0.131E-06	0.946E-07 0.668E-07 0.668E-07 0.554E-07 0.3459E-07 0.326E-07 0.226E-07 0.226E-07
111111111111111111111111111111111111111	0 1 1 1 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0		4 W W W O C		111111111111111111111111111111111111111
0.7926-01 0.6836-01 0.5896-01 0.5026-01 0.4276-01	0.355E-01 0.299E-01 0.256E-01 0.182E-01	0.125E-01 0.116E-01 0.874E-02 0.681E-02 0.461E-02	0.345E=02 0.316E=02 0.270E=02 0.224E=02 0.195E=02	0.153E 0.111E 0.496E 0.996E 0.367E 0.367E 0.322E 0.259E	0.184E-03 0.187E-03 0.375E-03 0.361E-03 0.361E-03 0.362E-03 0.362E-03 0.352E-03
0.682E 00 0.584E 00 0.500E 00 0.43CE 00 0.367E 00		0.138E 00 0.117E 00 0.106E 00 0.85E-01 0.701E-01	0.510E-01 0.430E-01 0.363E-01 0.307E-01	0.219E-01 0.187E-01 0.136E-01 0.136E-01 0.996E-02 0.656E-02	0.642E-02 0.490E-02 0.432E-02 0.344E-02 0.346E-02 0.346E-02 0.286E-02 0.286E-02 0.286E-02
1100 1100 1100 1100 1100 1100 1100 110	1100 1100 1100 1100 1100 1100	10 4 10 10 10 10 10 10 10 10 10 10 10 10 10	11111 00440 00440 00440 00440	1	0.04 0.04 0.05 0.05 0.05 0.05 0.05 0.05
20.5 18.7 20.5 17.5	1122 1152 1153 1154 1154 1154 1154 1154 1154 1154	19.0 10.0 13.2	8 4 6 6 7 1 1 2 4 4 6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	11245 11245 1134 1134 1134 1134 1134 1134 1134 11	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
216.2 216.4 216.4 213.9	209.7 207.6 209.2 208.0 212.2	213-1 212-9 211-3 207-1 196-0	200.2 199.1 197.8 195.6	205.7 212.6 209.8 210.6 210.4 2215.9 233.5	242.6 242.6 242.6 242.7 294.7 315.7 343.6 343.6 344.6 344.6 344.6 344.6
8 1000 8 2000 8 4 000 8 5 0 0 0	887000 887000 890000	00000000000000000000000000000000000000	97000 98000 99000 100000 101000	103000 103000 105000 105000 105000 108000	1110000 1110000 1113000 1114000 1116000 1118000 1119000

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE. 1962

SEASONAL MEAN PROFILE CHURCHILL WINTER

NC OBS TEMP ERROR DEGREES MEAN ST DEV on o SOUTH ERROR
M/SEC
MEAN ST DEV MASEC MASEC MASEC MASEC MASEC MASEC 1.5 DEV 1.5 DE NO OBS DIRECTION DEGREES (MEAN 2866.7 2253.0 2708.8 2708.8 2553.9 2553.9 2563.9 2563.9 2563.9 2563.9 3328.9 3328.9 3328.9 3328.9 SOUTH COMPONENT M/SEC MEAN ST DEV WEST COMPONENT M/SEC MEAN ST DEV 8887117008747777788887117708978 ALTITUDE M MSL 300000 35000 45000 50000 50000 50000 70000 70000 70000 70000 70000 70000 70000 70000 70000 70000 70000 70000 70000

Table A.3(b).

SEASONAL MEAN PROFILE

NO OBS

* * *	EMPERATURE DEG K ST DEV PC	URE**	* * * * * * * * * * * * * * * * * * *	**PRESSURE** NT/SQ M ST DEV	**** PCT DIF	** ** ** ** ** **	ENSITY** G/CU M	****
<u> </u>	2	2	Š	32.00	5	u e	200	-
30.	ċ	•	.275E	0.000E	7.	.416	0.000E 00	•
30.	ċ	•	237E	0.000E	80	.358		•
30.	ċ	٠	204E	0.000E	œ ·	308		•
29	o o	5°0	176E	0.000E	.	. 26		•
•	.	•	1276					•
•	• c	1 7	1136	2000	. 0	171		• •
. 0	• c	• 7	0 7 7 E	0.00 C		1		
	• d		3446	0.00		7.7.		•
4 (6	ó	200-	729F	0.000	0	108		
200	'n		657E	0.210E	14.	944		
9	4	•	569E	0.178E	14.	.806		•
65	3•	•	497E	0.163E	14.	• 693		•
53.	'n	٠	434E	0.148E	15.	. 598		•
52	7.	•	379E	0.107E		517		•
58.	ģ	•	332E	0.954E	. 15	44.		,
9	٠. د	n c	1467	0.869E				•
		•	2007	7265				•
9 5		•	3000	1004		, 26		•
•	'n	•	1000	150000	0 0			•
, v	ů :	•	1565	0.00	0 0	777		• •
, ,		•	1275	7004.0	0	7		
20	1 4	, t • 0	1215	0.449E	19.	15		18
72.	4	•	107E	0.398E	19.	.137		•
272.2	4	0.5	0.951E 0	02 0.360E 01	19	_	0.396E-04	18.5
71.	4	0.2	940E	0.328E	19.	101		18.9
0.	4	0.0	742E	0.301E	16	. 955		٠
69	4	0	655E	0.274E	67	40		•
9 1	•	٠	2 / OE	3167.0				0 0
9	•	0 C	1000	0.20 VE	67	0 4		• •
2 4	• 4		395F	0.187F	10	52		
262.4	7	1.0	348E	0.170E	19.	.462		
5	•	•	306E	0.153E	19.	410		18.7
56	•	0.2	.268E	0.138E	19.	• 365		•
52	7	-0•3	.235E	U.123E	19.	•324		٠
8	.	80 F	-206E	0.109E	19	• 288		•
Ĵ.	• ,) ·	1 / 95	0.995	6			•
4 6	٥	0 0	1000	0.001	. 0			•
0 4	•		100	0.710E	10			
1 0	0 4	7 · O	1025	0.424F	18	12.		
, ,	1 4	-0-	3 9 4 F	0.552E	8	135	0.7795-05	
20	(6)	-1.1	761E	0.485E	18	120		
15	m		.652E	0.421E	18.	. 105		•
• 60	ë	-2.7	.557E	0.363E	17.	.925		
• 40	;	•	3474E	0.315E	17.	308.		•
• 66	4	•	.402E	0.272E	16.	702		•
•	'n	•	339E	0.236E	15.	.607		•
189.1	91	ري د د د	-284E	0.205E	14.	5.24	0.354E-05	21.0
ė,	• ,		138E	0.1.0E				•
ė,	.	1 .	1 / L	C • 1 3 3 E	•	000		•
			34.25	10010		000		

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2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	112.1	111111111111111111111111111111111111111	11111 600000 600000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0.195E-05 0.170E-05 0.146E-05 0.120E-05 0.100E-05	0.855E-06 0.697E-06 0.625E-06 0.547E-06 0.571E-06	0.233E-06 0.136E-06 0.103E-06 0.834E-07 0.000E	0000E 0000E 0000E 0000E	00000000000000000000000000000000000000
0.227E-04 0.188E-04 0.155E-04 0.129E-04		0.231E-05 0.137E-05 0.137E-05 0.109E-05	0.629E-06 0.507E-06 0.422E-06 0.352E-06 0.298E-06	0.135E-06 0.132E-06 0.132E-06 0.132E-06 0.956E-07 0.811E-07
0.04 0.0 0.00 0.0 0.00 0.00 0.00 0.00 0.	15.0 17.3 115.8	1 2 2 2 2 2 2 3 3 2 4 4 4 4 4 4 4 4 4 4 4	11111 00000 00000000000000000000000000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0.964E-01 0.817E-01 0.693E-01 0.588E-01 0.502E-01	0.431E-01 0.369E-01 0.317E-01 0.218E-01 0.158E-01	0.757E-02 0.760E-02 0.528E-02 0.443E-02	0000E 0000E 0000E 0000E 0000E	0000E 0000E 0000E 0000E 0000E 0000E 000E
0.110E 01 0.910E 00 0.746E 00 0.610E 00	0.403E 00 0.325E 00 0.264E 00 0.206E 00 0.130E 00	0.8666 0.8666 0.8666 0.8686 0.8636 0.8636 0.8636	0.345E-01 0.291E-01 0.248E-01 0.211E-01 0.180E-01	0.1376-01 0.1376-01 0.9186-01 0.8326-02 0.7166-02 0.5356-02 0.5356-02 0.54646-02
16.9	112.7	111100	87-1900 87-1900 11	242997779 242997779
8 8 8 8 8 8 8 8 8 8 8 8 4 8 8 8	9 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	122.1	000000	
169.9 169.9 167.6 164.7	1557 1553 1553 1553 1553 1553 1553 1553	166.9 166.9 172.9 180.9	1990 2099 21086 21086 21086 31	213.7.2 2114.7 2114.7 2225.5 2225.6 2239.8 2339.9
8 1000 8 1000 8 2000 8 3000 8 4000	85000 86000 87000 88000	91000 92000 93000 94000	96000 97000 98000 99000 100000	10,200 10,300 10,500 10,500 10,500 10,500 10,500

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE. 1962

SEASONAL MEAN PROFILE

	NO OBS		7	'n	7.	7	13	16	15	7,	11	13	17	13	10
	RROR	T DEV	0.0	1.4	1.3	1.3	0	1.4	1.5	7.7	1.5	2.0	2.0	1.5	2.0
	TEMP ERROR DEGREES	MEAN	1.1	1.5	2.3	1.9	5.7	2•1	2.0	1.4	1.8	1.9	1.5	1.7	5.4
	NO OBS		0	0	0	0	0	0	0	0	0	0	0	0	0
	SOUTH ERROK M/SEC	ST DEV	0.0	0.0	0.0	0.0	0	0	0	o •	0	0.0	0	0	0.0
	SOUTH M/S	MEAN :	0.0	0	o• •	0	0.0	0	0.0	0	0	0.0	၀ ၁	°.	0.0
	ERKOK SEC	T DEV	0.0	ပ ၁	0	0.0	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	WEST ERROR M/SEC	MEAN S	0.0	0.0	0.0	0	0.0	0	0.0	0.0	0	0.0	0.0	0	0.0
SCAMER	NO OBS		2	5	14	14	13	91	12	7.	17	13	17	61	10
כאטאכאזרר אנ	DIRECTION DEGREES	MEAN	109.4	0.06	87.7	76.5	67.6	78.3	88.5	7.96	86.3	72.1	49.2	250.3	279.8
ŧ	SPEED M/SEC	MEAN	11.9	17.6	15.5	17.3	25.3	33.3	24.4	41.5	57.1	62.7	23.0	2240	52.4
	SOUTH COMPONENT M/SEC	ST DEV	3.3	7.9	7.7	7.3	11.3	14.9	28•6	20•1	17.3	62.1	46.1	46.0	101.7
	SOUTH	MEAN	3.9	0	9.0-	0.4-	9.6-	-6.7	9.0-	4.9	-3.6	-19.2	-15.0	7.4	-8.9
	COMPONENT M/SEC	ST DEV	6•0	13.0	12.9	8•3	10.0	15.6	15.2	19.0	26.3	6.44	52.8	61.5	6.09
		MEAN	-11.2	-17.6	-15.5	-16.8	-23.4	-32.6	-24.4	-41.3	-57.0	-59.7	-17.4	20.7	51.6
	ALTITUDE M MSL		30000	35000	40000	45000	20000	55000	90000	65000	70000	75000	80000	85000	00006

Table A.3(c).

SEASONAL MEAN PROFILE CHURCHILL SPRNG/FALL

3	•	(°	or or	6	11	1	17	11	12	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13		o e		7 -	7 6		13	13	13	13	13	13	13	13	13	13	13		13	13	7.	71	12	71
PCT DIF		1	0.3	-1.2	-2.2	•	-3.9	6.4-	0.4-	-5.1	S	4.6-	1	5	5	9	-6-	-	60	ç	-10.2	97	-11.4	-11.9	-12.6	-13.1	-13.4	-13.5	-13.7	-14.2	0.61	0.01	170.0	5 a l	2001	-19.7	-20.2	-20.7	-21.0	-21.1	-21.0	-20.5	-19.7	-18.8	-17.8	-17.1	•	-12.9	•	•		1.5.		0
*DENSITY*** KG/CU M ST DEV		0.1005-03	• 135E	.181E	.201E	221E	.228E	.226E	.205E	• 186E	.158E	•141E	0.130E-03	.121E	0.114E-03	0.109E-03	0.104E-03	0.992E-04	0.931E-04	0.869E-04	0.805E-04	0.741E-04	677	.616E	• 554	964.	•435	380	.336	903		162.	200	0.1755-04	0.1535-04	13.6	0.118E-04	104	• 918	808	• 714	• 623	544	• 463	0.384E-05	323	272	• 228		165	0.140E-05	11.	0.949E-06	90-356.0
* * * * * * * * * * * * * * * * * * *	- (0.9675-02	0.723F-02	0.615E-02	0.524E-02	0.448E-02	0.383E-02	0.328E-02	0.287E-02	0.246E-02	14E	0.185E-02	5 1 E	Ξ.	23E	0.108E-02	0.955E-03	0.837E=03	0.733E-03	0.643E-03	0.566E-03	0.499E-03	0.440E-03	0.388E-03	0.341E-03	0.300E-03	0.264E-03	0.233E-03	0.206E-03	0.182E-03	0 1 1 0 E = 0.3	0 - 140E - 03	0 1 2 2 E 1 0 3	0.1065-02	0.8075-04	0.7075-04	0.609E-04	0.527E-04	0.457E-04	0.395E-04	0.342E-04	0.296E-04	0.257E-04	0.223E-04	0.193E-04	0.165E-04	4 TE	20E	310	57E	0.751E-05	9 :	344E	1
**** PCT DIF	,		7.7.		-5.7	-6.3	8.9-	-7.4	9.9-	-7.9	-9.5	-8-7	-9.1	7.61	-10.3	-10.8	11.4	6.11.	-12.5	-13.0	-13.5	-14.0	-14.4	-14.8	-15.2	-15.5	-15.9	-16.3	-16.7	-17.0	n 1 - 1 - 1	/•/T	A	0 0 0	104	-17.7	-17.4	-16.9	-16.2	-15.5	-14.4	-13.4	-12.2	-10.9	7.6-	-7.7	0.9-	7.7	-2.9	4.1.	2•3	9.0	4 t	0
PRESSURE* N1/SC M ST DEV PC	0	0.2835 02	285E	.266E	•231E	.218E	.205E	3761.	.198E	87E	.173E	.159E	147E	•135E	.124E	13E	1036					.608E	.541E	.480E	.425E	.3756 0	335E	0.293E 01	.259E	.228E		10 1971 0		0.1345 01	1006	2004	751E	.646E	0.553£ 00	.471E	.398E	.334E	.279E	.231E	.192E	.159E	.132E	• 109E	•	0.738E-01	0.507E-01	. 394ti	0.306E-01	
* * * * * * * * * * * * * * * * * * *		0.5425 03																																																	0.422E 00		0.299E 00)
JRE** PCT DIF	,	-2.5		-3.6	-3.6	-3.3	-2.9	-2.5	c;	-2.9	-3.4	-3.7	0.4-	7.4-	-5.0	-5.1	-5.1	6.4-	7.4-	-4.2	-3.9	-3.6	13.4	-3.2	-3.0	-2.7	-2.9	~ 3•3	-3.6	4.6-	8.7	1,21	7.0	0 K		2.6	3.5	6.7	6.1	7.3	8•6	7. 6	10.0	10.4	10.8	11.9	11.3	10.4	10.1	9.3	9•6	۰ د د	, ,	•
EMPERATURE* DEG K ST DEV PCT	•	11.0	17.5	11.6	11.3	12.6	14.5	16.7	15.6		13.9		13.0	12.5	•	11.		6	8	7.1	6.5	7.2	8.6	9.8	7.6	9.1	8.3	9 • •	7.6	7.0	ος (Ο (n c) ·	1 0		7.7	8	7.5	7.0	•	7.3	7.1	8.5	10.3	11.5	11.9	11.7	11.8	12.5	13.6	15.0	۲۰,۲ د د د د د د د د د د د د د د د د د د د	0.0	• 0 1
**TE MEAN		731.0	229.4	233.3	235.8	239.2	242.9	246.7	246.5	250.8	252.4	254.3	256.0	256.7	256.9	256.8	256.6	257.2	257.8	257.9	257.1	255.8	254.4	253.1	251.8	250.5	248.2	245.2	241.9	238.5	2.962	7.0467	4.757	730.5	226.9	225.1	223.5	222.3	220.7	219.1	217.5	214.8	211.5	208.1	204.5	202.3	201.2	199.6	199.0	_	œ.	196.1	7.00	•
ALTITUDE M "SL		34000	36000	37000	38000	39000	4 0000	41000	4 2000	43000	00044	45000	7 6000	4 7000	00087	49000	50000	51000	52000	53000	54000	55000	56000	57000	58000	28000	00009	61000	62000	63000	64000	0000	99000	000,4	00000	2000	71000	72000	73000	74000	75000	76000	77000	78000	79000	80000	91000	8 2000	43000	R 4 0 0 0	85000	86000	000/8	

	m	z.	ıς.	2		6	2
	-	6.5	6	6	80	9	9
0.5935-06	0.483E-06	0.354E-06	0.220E-06	0.974E-07	0.479E-07	0.659E-07	0.104E-06
0.3875-05	0.321E-05	0.276E-05	0.234E-05	0.192E-05	0.158E-05	0.129E-05	0.107E-05
6.7	6.7	9.5	8.6	7.2	8•3	3.4	-2.4
0.190E-01	0.129E-01	0.834E-02	0.784E-02	0.834E-02	0.982E-02	0.870F-02	0.8396-02
0.210E CO	0.175E 00	0.150E 00	0.124E 00	0.102E 00	0.873E-01	0.7035-01	0.560E-01
6. 2	6.8	7.7	. 0.1	-1.4	0.0	-3.4	-8.6
18,8	22.6	54.9	21.4	19.2	19.5	17.2	9.6
191.9	193.0	191.7	186.8	186.8	192.4	188.6	181.3
0006	0000	91000	12000	3000	0005	2000	0009

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE, 1962

SEASONAL MEAN PROFILE

CHURCHILL SPRNG/FALL

NO OBS	m 01	11	14	14	14 19	16 21	3
TEMP ERROR DEGREES MEAN ST DEV	0.1	1.3	1.6	1.6	1.3	2.9	15.7
TEMP DEG MEAN	1.0	1.6	2.0	1.9	2.5	4.0	9.6
NO OBS	~ ~	n o	so so	۰ ۰	6 60	7 01	10
ERKOR SEC ST DEV	0.0	1.4	n n	2.7	1.7	11.2	14.6
SOUTH B	0.6	4.6	6.0	7.0	11:1	16.2	34.6
WEST ERROR M/SEC MEAN ST DEV	0.0	2.1	9 ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °	2.6	1 .4	11.3 8.8	10.5
WEST MEAN				7.1			
NO OBS	33	13	16	16 15	17	18	17
DIRECTION DEGREES MEAN	5.5	286.5	288.6	271.7	259.9	255.7	252.7
SPEED M/SEC MEAN	10.5	18.2	32•1 31•9	25.8	29.4	11.5	33.9
SOUTH COMPONENT M/SEC MEAN ST DEV	10.3	20.8	15.0	17.1	28.2	60.2	116.3
SOUTH M MEAN	-10.5	-5.1	-10.2	1.6	5.1	22.1	10.0
COMPONENT M/SEC N ST DEV	3.4	18.7	30.4	33.7	32.3	4 1 • 6 4 5 • 5	0.44
WEST CO	-1.0	17.5	30.4	25.8	28.9	11.1	32.4
ALTITUDE M MSL	30000	40000	50000	60000	70000	80000	00066

Table A.4(a

SEASONAL MEAN PROFILE BARROW WINTER

TITUDE	**	TEMPERATURE*	JRE**	****	*PRESSURE***	* * *	****	*DENSITY**	****	8
1 MSL		DEG K			M DS/IN			KG/CU M		085
	MEAN	ST DEV	PCT DIF	MEAN	ST DEV	PCT DIF	MEAN	ST DEV	PCT DIF	
3000	241.8	9.0	4.7	•736E	0.261E	ë	•106E	C.348E-03	.8	2
14000	230.3	14.4	-1.4	•599E	0.469E	Ġ.	• 905E	0.292E-03	-8.3	ı,
5000	228.1	15.3		. 504E	0.434E	•	1697	0.282E-03) (, ,
0000	7.000	0 .		7/010	1000000		000	0.3016103	7.6	
000	220.4	- 4	1.4	3000	0.347F		7.07.	0.247F=03	- 1	9 -
0000	229.7	16.4	7.	283F	0.325E		429E	0.253E-03	٠,	9 -
0000	230.1	17.3	0.81	.245E	0.305E	-14.6	369E	0.245E-03	-7.4	19
1000	232.7	19.1	0.8-	.214E	0.287E	•	.319E	0.230E-03	-7.6	17
2000	234.1	17.5	-8.5	•188E	0.269E	•	.279€	0.252E-03	-6.7	19
00061	235.2	16.7	0.6-	•163E	0.247E	•	•240E	0.243E-03	-7.3	19
0007	236.3	15.8	-6.5	.141E	0.225E	16.	•207E	0.2346-03	-7.9	18
2000	237.2		-10.2	•123E	0.205E	-17.4	•179E	0.222E-03	1.8-	61
0009	237.7		-10.9	•106E	0.186E	-18.6	•155E	0.206E-03	-9.1	61
,7000	238.6		-11.5	.928E	0.168E	-19.9	• 134E	0.190E-03	8.6	6.
9000	238.9		-11.7	0.806E 02	0.151E	-21•1	•117E	0.1755-03	-11.0	5 6
0006	239.2		9•11-	• / 0 1 E	0.133E	6.77	11010	00101010	12.5	7
0000	239.1		9111	1000	17710	120.7	1000	0.1406-03		A 0
0001	239.1		9771	. 4 6 J F	10010	0.40	4 4 4 4 4	0.121F-03	15.5	10
0002	7.066		11.	100	0.001	-27.0	7 C C C C	0.110F-03		
0004	739.3		-10.5	348F	0.747E	-28.1	506E	0.103E-03	-19.7	18
5000	239.4		8.01	3035	0.652E	-29.0	3275	0.967E-04	-21.1	19
0009	239.8	12.0	0.6.	.263E	0.564E	-30.0	.384E	0.899E-04	-22.6	18
7000	240.6	12.9	0.8	.228E	0.483E	-30.9	.333E	0.799E-04	-24.3	19
8000	241.3	12.1	-7.0	.198E	0.413E	-31.7	•289E	0.684E-04	-25.9	19
0006	241.1	11.9	7.9-	.172E	0.353E	-32.5	•251E	0.588E-04	-27.2	19
0000	539.4	12.4	-6.3	.148E	0.301E	+33+8	•218E	0.517E-04	-28.7	18
1000	237.8	13.4	-6.2	•128E	0.255E	194.5	• 190E	0.448E-04	-29.4	8
2000	236.3	15.0	00 C	•111E	0.216E	2.00	1001	0.386E-04	130.4	D 0
0006	734.9	7 C	· ·	1,00°		1000	1245	0.2775-04	132.0	0 a
000	231.0	11.2	1 (7265	0.131F	34.46	1006	0-2375-04	36.3	9 6
0000	220.0	0.0		626F	0.111	36.9	. 455F	0.198E-04	-35-0	9 9
7000	228.2	11.3	-1.3	540F	0.940E	-37.2	830E-04	0.168E-04	135.8	18
8000	225.9	11.1	9.0	.466E	0.793E	-37.3	.723E-04	0.143E-04	-36.5	18
0006	222.7	11.3	-0. 3	.401E	0.6655	-37.4	.631E-04	0.124E-04	-36.8	18
0000	219.6	12.1	0.0-	.344E	0.554E	-37.5	•551E-04	0.110E-04	-37.0	18
1000	217.0	13.2	ر د د	•295E	0.459E	-37.6	•478E-04	0.973E-05	-37.3	18
2000	215.0	14.4	1.4	•252E	0.375E	-37.6	•414E-04	0.8485-05	-37.8	8.
3000	213.5		9 0	. 2 1 5 E		10/01	0.3566104	0.186100	138	9 6
000	211.5	14.4		157F	0.192F	136.0	7.00	0.475F-05	, ,	9 6
0009,	211.4	15.4	7.7	. 134E	0.153E	-36.3	•223E	0.388E-05	-40.5	18
7000	213.8	16.7	11.2	.114E	0.121E	-35.4	.188E	0.321E-05	-41.2	18
9000	217.4	18.9	15.4	979E	0.955E-	-34.1	.158E	0.266E-05	~ 1	18
00064	221.3	55.6	19.9	.839E	0.7546	-32.5	•133E	0.220E-05	-42.9	18
30000	221.8	22.0	22.7	.714E	0.558E-0	-31.1	•113E	0.178E-05	-43.0	17
1000	219.6	21.0	21.5	•613E	0.446E-	-28.8	• 984E	0.139E-05	ċ	1 /
12000	218.7	20•B	21.0	•525€	0.364E-	-26.7	•846E	0.109E-05		1.
3006	218.7	22.5	21.0	•450E	0.304E	-24.4	• 726E	0.948E-06	•	17
0000	221.6	21.9	22.6	•386E	0.262E-	-22.0	•613E	0.731E-06	Ġ.	\
0 0	224.1	22.5	24.0	•332E	0.224E	•	• 521E	0.0216-00	194.4	
96000	726.	22 6	24.2	0.245E 00	0.1746	110.0	0.4496103	0.4505-06	1 20 4 0	17
1 /000	F = + 2 /	6.23	7 • 6	+ 2 4 0 F	0.111	• 0 1	200	•	0 • 2 7	•

111111227111111111111111111111111111111	
0.345E106 0.289E106 0.216E106 0.136E106 0.136E106 0.102E106 0.102E106 0.000E	2
0.333E-05 0.254f-05 0.254f-05 0.230F-05 0.176E-05 0.116E-05 0.317E-05 0.659F-06	STANDARD ATMOSPHERE, 1962
0 4 0 4 0 4 0 4 8 0 4 0 4 0 4 8 0 4 0 4	ANDAKD
0.145E-01 0.107E-01 0.927E-02 0.773E-02 0.694E-02 0.660E-02 0.000E 00	USING U.S. ST
0.213E 00 0.185E 00 0.136E 00 0.136E 00 0.116E 00 0.842E-01 0.6842E-01 0.664E-01	CALCULATED US
00 00 00 00 00 00 00 00 00 00 00 00 00	WERE
188.5 200.0 172.0 173.0 100.0 0.0	DIFFERENCES
224.1 220.5 214.7 201.0 201.9 201.9 206.5 206.5 238.5 279.0	PERCENT DI
889000 990000 91000 92000 94000 95000 95000	

11110000011

SEASONAL MEAN PROFILE

BARROW WINTER

0 8 S	œ	13	20	56	22	52	23	50	5,4	54	28	31	21	÷
ERROR SREES ST DEV	0.1	4.0	6.0	1.0	1,3	1.3	1 • e	1.8	2.0	2.8	5.1	7.1	11.4	8.3
TEMP DEG	9.0	7.0	7.9	5.6	3,3	3.7	4.3	5.3	6.0	6.5	11.0	13.9	18.2	17.3
NO OBS	'n	7	7	7.7	6	10	o.	٥	7	01	14	13	œ	-
SOUTH EKROR M/SEC MEAN ST DEV	6.0	5.4	7.0	5.4	2.9	1•3	3.5	£.6	7.0	0.8	12.2	15.9	33.8	0.0
SOUTH MEAN	2.6	3.5	4.4	6.8	7.4	6.9	8.8	11.9	14.9	16.0	30.1	35.8	52.3	41.4
ERROK /SEC ST DEV	6.0	2.3	٠٠٥	2.2	2.8	1.4	3.2	3.6	7.0	7.7	12.1	15.8	33.4	0.0
WEST MEAN	2.6	3.4	4.3	9.9	7.2	6.3	9.4	11.3	14.2	15.5	30.5	34.8	52.0	50.8
085	6	14	21	28	23	27	23	50	24	54	28	31	21	4
DIRECTION DEGREES MEAN	306.8	320.7	323.6	327.8	337.5	347.3	345.1	333.4	1.8	240.4	226.1	281.6	160.6	305.8
SPEED M/SEC MEAN	48.2	53.1	58.4	60.2	51.1	46.4	25.3	37.4	29.9	10.4	20.6	17.8	42.5	102.1
TH COMPONENT M/SEC AN ST DEV	18.4	19.4	22.2	36.3	40.7	39.7	39•3	42.1	51.2	37.6	46.0	9.49	124.0	143.8
SOUTH O	-28.9	-41.1	-47.0	-50.9	-47.2	-45.3	-24.4	-33.5	-29.9	5.1	14.2	-3.6	40.1	-59.7
COMPONENT M/SEC ST DEV	19.7	22.5	22.5	28.8	54.9	37.6	25.4	21.7	24.6	46.4	65.1	81.7	75.1	94.5
WEST CO	38.5	33.6	34.6	32.0	19.5	10.1	4.9	16.7	6.0-	9.1	14.8	17.5	-14.1	85.8
LTITUDE M MSL	30000	35000	40000	45000	50000	55000	00009	65000	70000	75000	80000	85000	00006	95000

SEASONAL MEAN PROFILE BARROW SUMMER

NC OBS	200	v ~	7	(3)	7 0	1 7	7	~	7	'n.	۰ ب	ه م	3 - C	•	•	9	9	^	•	9.	3 .	20	01	01	01	2	0	9	3 6	3 2	2	10	2	9 0	9 0	21	2	01	9	9	.	P 0	~ ~	. 0-	0.	•	•	œ
**** PCT DIF	60 c	3.5	3.6	4.2																																	27.3									37.1	37.4	35.1
**************************************	0.593E-03	166E	.134E	0.1465-03	0.9735-04	0.204E-03	0.142E-03	0.1556-03	0.115E-03	0.242E-03	0.176E-03	0.1346103	0-1085-03	0.109E-03	0.106E-03	0.961E-04	0.852E-04	0.696E-04	0.793E-04	0.748E-04	0.041E-04	0.510E-04	0.455E-04	0.426E-04	0.3796-04	0.328E-04	0.294E-04	0.262E-04	0.237E-04	0.207E-04	0.199E-04	0.180E-04	0.161E-04	0-1435-04	0.111E-04	U-100E-04	C.938E-05	U.815E-05	0.739E-05	0.679E-05	0.6376.05	0.01777.00 0.0177.00 0.0170.00	0.457E-05	0.410E-05	0.370E-05	E-0	0.294E-05	0.198E-05
** ** ** ** ** **	0.4135-01	303E	260E	0.223E-01	0.1935-01	0.144E-01	0.126E-01	0.109E-01	0.945E-02	0.784E-02	0.677E-02	0.5055102	0 - 4 3 6 F - 0 2	0.377E-02	0.328E-02	0.286E-02	0.250E-02	0.221E-02	0.197E-02	0.173E-02	0.193E=02	0.120F-02	0.106E-02	0.946E-03	0.840E-03	0.748E-03	0.666E-03	0.592E-03	0.5285-03	0.4216-03	0.375E-03	0.334E-03	0.298E-03	0.295F=03	0.209F-03	0.185E-03	0.165E-03	0.146E-03	0.128E-03	1136-03	000000000000000000000000000000000000000	7725-04	575E-04	588E-04	509E-04	0.440E-04	77E	<u>.</u>
**** PCT DIF	604			8•2	y = 1	10.6	11.1	11.3	11.3	10.6	12.2	13.4	10	14.8	15.5	16.2	17.0	18.1	19.9	19.4	200	20.9	21.4	21.9	22.5	23.0	23.7	24.3	25.0	26.4	27.0	27.5	28.0	28.5	29.6	30.2	30.9	31.4	31.9	32.4	20.00) C	95.00 0.00 0.00	32.6	31.9	31.1	•	26 ; 3
******PRESSUKE****** NT/SG R AN ST DEV PCT	0.200E 02					0.110E 02																									0.159E 01												0.293E 00					•105E
* * * * * * * * * * * * * * * * * * *	0.271E 04	-201E	.174E	50E	3 T	1 W	52E	39E	14 O	2 E	1 (1	7 7	77.	1 LLJ	34E	24E	38E												0.414E 02			.251E	.220E	9.3F	148F	129E	.112E	.978E	347E	31E	6 2 9 E	1000	390E	330E	.277E	232E	93E	0.157E 01
URE** PCT DIF	3.1 1.4 1.4) M	3.9	œ i	n 4	3.4	1.6	0.5	2.0-	2.3	3.5	- a	2 4	0	5.3	5.5	5.5	5.0	0•4	0,0	8 0	0 6 6	3.1	3.2	3.4	3.7	0.4	m (n -	4 0C	3.4	2 • 9	2.6	2 ° 8	0) O	2 • 8	2•6	2.4	1. 89		7.0	100	-2.3	-3.2	-4.3	-5.3	-6.5
TEMPERATURE DEG K AN ST DEV PCT	1 5 • 5	00	0 • 8	0	2.0	9	0.2	0.7	0.2	6.1	5.5	1 t	3.5	2.7	3.7	5.1	9.	7.3	6.9	4.0				3.5	3.4	3.3	3.6	3,66		2 • 1	2.3	2.2	2.4	7.7	. "	3.2	3.8	4.7	5.7	2.0	2.0	20 u	4 4 0 4	m	m	7	w	3.1
* * TE	228.6	231.4	233.3	234.2	236.4	236.6	534.9	235.1	235.9	244.9	250.0	6.66.	261.62	266.0	269.6	272.8	276.0	277.4	277.1	278.0	218.3	278.7	279.1	279.4	278.9	277.6	276.2	275.0	2/3•1	267.5	264.5	261.2	257.7	254.62	246.6	242.5	237.9	233.4	228.9	223.7	21/16	207.0	201.3	195.5	189.7	183.9	178.3	172.4
ALTITUDE M MSL	25000	27000	28000	29000	30006	32000	33000	34000	35000	36000	37000	00088	00000	41000	4 2 0 0 0	43000	00044	45000	00094	47000	0000	50000	51000	52000	53000	24000	55000	56000	00074	2000	90000	61000	62000	63000	65000	96000	9 1000	68300	00069	70000	00077	00000	74000	75000	76000	17000	78000	79000

20	20	80	80	30	80	80	6)	90	100	7	•	• •0	m	. 7	~1	~ 4	
35.0	36.1	39.9	39.8	37.8	33.7	27.3	20.5	14.0	8.2	2.0	-2.5	-8.2	-17.4	-21.1	-26.8	-27.3	
0.170E-05	0.153E-05	0.141E-05	0.130E-05	0.117E-05	0.941E-06	0.707E-06	0.526E-06	0.409E-06	0.327E-06	0.337E-06	0.281E-06	0.232E-06	0.211E-06	0.162E-06	0.911E-07	0.000E 00	21
C.270E-04	0.229E-04	0.193E-04	0.16CE-04	0.131E-04	0.106E-04	0.842E-05	0.6635-05	0.522E-05	0.412E-05	0.323E-05	0.253E-05	0.195E-05	0.145E-05	0.115E-05	0.885E-06	0.732E-66	STANDARD ATMOSPHERE, 1962
24.4	22.3	18.5	14.8	10.0	4 • 8	-0-3	-5.5	7.6-	-13.9	-18.1	-21.9	-25.0	-31.3	-36.7	-39.0	-53.1	NDARD A
0.8738-01	0.7466-01	0.608E-01	U.486E-01	0.378E-01	0.287E-01	0.219E-01	0.168E-01	0.134E-01	0.107E-01	0.9006-02	0.766E-02	0.670E-02	0.430E-02	U.532t-02	0.650E-02	0.300c.0	NG U.S. STA
0.129E 01	0.1356 01	0.852E 00	0.684E 00	0.545F 00	0.43ZE 00	0.341E 00	0.27CE 00	0.214E 00	0.170E 00	0.134E 00	0.1C6E 00	0.857E-01	0.658E-01	0.51CE-01	0.414E-01	0.269E-01	DIFFERENCES WERE CALCULATED USING U.S.
-7.8	-11.4	-14.9	-17.8	-20.0	-21.4	-21.6	-21.2	-20.6	-20.3	-19.3	-19.1	-17.2	-14.5	-16.8	-14.3	-35.5	ES WERE
3.4	3.3	3.5	5.0	5.9	6.3	6.2	7.9	6.9	7.5	10.4	13.4	18.3	29.8	38.6	45 • B	0	FERENC
166.4	159.9	153.7	148.4	144.4	141.9	141.6	142+3	143.3	143.9	145.7	148.3	154.3	161.9	160.0	167.4	127.9	PERCENT DIF
80000	8 1000	8 2000	83000	84000	85000	86000	87000	88000	89000	00006	91000	92000	93000	00076	95000	00096	-

SEASONAL MEAN PRUFILE

BARROW SUMMER

0.40	1		٠.	_				. ~	- 20				. ~	. 73
NO OBS		•	-	-	-	,	7	•			-	7		7
ERROR	ST DE	0.1	4	9.0	6.0	8.0	8.0	8.0	0	6	9.0	1.04	3	0
TEMP	MEAN	0.2	9.0	6.0	1.5	1	1.5	1.2	1.4	1.4	8	2.6	7.7	5.3
ONO		9	0	0	0	၁	a	0	0	a	0	0	0	၁
SOUTH ERROR M/SEC	ST DEV	0	0	0	0	0.0	0.0	0.0	0	0	0.0	0	0.0	0.0
SOUTH M/	MEAN	0	0.0	0.0	0.0	0.0	0.0	0	0	0.0	0	0.0	•	0.0
WEST ERKOR M/SEC	T DEV	0	0.0	0.0	0.0	0.0	0	0	0	0.0	0	0	0.0	0
WEST A	MEAN S	0.0	0.0	0.0	0	0	0.0	0	0	0	0.0	0.0	ာ	0.0
NO OBS		4	'n	1	11	6	7.0	^	æ	σ	10	10		7
DIRECTION DEGREES	MEAN	113.2	91.5	78.8	67.3	94.1	9.62	79.2	8.8	73.8	9999	132.3	103.5	8.06
SPEED M/SEC	MEAN	6.7	6.8	13.1	15.7	16.4	25.5	22.5	34 • B	40.5	50.7	23.1	18.0	27.8
SOUTH COMPONENT M/SEC	ST DEV	2.6	3.2	4.3	7.1	5.6	14.3	60 60	12.7	54.6	34.0	45.7	47.7	6•9
SOUTH 8	MEAN	5.6	0.1	-2.5	0.9-	-1.6	-4.5	-4.2	-0.7	-11.2	-20.9	15.5	4.2	4.0
COMPONENT M/SEC	ST DEV	5.3	8•3	5.2	4.9	7.6	7.1	10.0	8.7	21.3	34.6	47.7	88.9	16.5
¥ES7 ∑X		-6.2	8.9-	-12.8	-14.5	-16.3	-25.1	-22.2	-34.8	-38.9	-46.2	-17.0	-17.5	-27.8
ALTITUDE M MSL		35000	40000	45000	50000	55000	6 0000	65000	70000	75000	80000	85000	00006	95000

Table A.4(c).

SEASONAL MEAN PROFILE BARROW SPRING/FALL

ALTITUDE M %SI	*	TEMPERATURE**	URE**	* *	*	**************************************	* * *	****	*******DENS117***********************************	***	80 083
1	MEAN	ST DEV	PCT DIF	MEAN		ST DEV	PCT DIF	MEAN	ST DEV	PCT DIF	
34000	225.3		-3.5		03	184E	-10.4	.919	90E	-7.0	e
35000	233.5	_	-1.2		03	453E	-7.8	0.789E-02	32E	9.9-	11
36000	235.7	8.6	11.4	0.468E	69	0.475E 02	6*5*	0.692E-02	0.580E-03	9.4-	71
37000	239.5	٠.	0		e (5.3	0.595E-02	מיני זיר	**************************************	` '
88000	241.2	-	7.0		600	3806	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.5136-02	0.404E=03	7 6	- 1
0000	24.0	- ٦	17.0		n e		ο α • • •	0.3836=02	0.3236=03		1-
	4.4.4	-	1.5.1		9 6		0 - 7	0.33550	0.2045-03		
000	240.7	٠-	12.0		ף סכ		7.9	0.3316102	0.2666-03		1
0000	250.5	٠.	0.6		ם כ		- a	0.2495-02	0.242F=03		
	252.4	•-	4.0) r			0.216F-02	0.221F=03		1.
0004	254.1	• ~	1 6		9 6		-7-5	0.188F-02	0.196E-03		17
0004	756.5	• -	8.0		36		-7-0	0.1635-02	0.174E-03		17
7000	258.6	٠.	-4.1		03.0		18.3	0.142E-02	0.162E-03		17
8000	260.3		-3.8		05		18.7	0.124E-02	0.152E-03		17
0006	260.8	_	-3.6		20		-9.1	0.109E-02	0.138E-03	9	17
0000	250.7	_	-3.6		02	1.1	7.6-	0.959E-03	0.126E-03		17
1000	260.0	_	-3.9		02		8.6-	0.846E-03	0.116E-03		17
2000	258.9	_	-4.3		20		-10.2	0.747E-03	0.107E-03		17
3000	257.8	٠,	14.3		25		-10.6	0.6595-03	0.100E-03		11
4000	256.8	٠,	0.4		05	.853E	-11.0	0.581E-03	0.924E-04	o · / -	1,
0000	20007	•	13.5		٠ ر د د	1010	111		0.7965-04		
2000	256.7		0.7		200		· ·	0.3946-03	0.737E-04	•	
0008	256.1				20	553E	-12.0	0.347E-03	0.676E-04		17
0006	253.4		-1.6		20		-12.2	0.307E-03	0.602E-04	-11-1	17
0000	250.1		-2.1		02		-12.3	0.272E-03	0.533E-04		17
1000	246.2		-2.9		05		-12.5	0.242E-03	0.479E-04	-10.3	17
2000	243.7		-2.8		200	.346E	-11.6	0.216E-03	0.438E-04		16
2000	29.40		2.0		2 6		7 .	0.191E=03	0.3536-04	1.011	9 4
	733.3		7.6		, ,		-12-2	0 1485-03	0.317F-04	401-	16
0000	230.9		11.8		70		-12.6	0.130E-03	0.285E-04	-11.3	91
2000	228.8	7.6	-1.0		010	0.184E 01	-12.7	0.113E-03	0.257E-04	-12.0	16
8000	226.0		-0.3				-12.7	0.995E-04	0.232E-04	-12.6	16
0006	224.7	an ·	S .				-12.6	0.867E-04	0.206E-04	-13.2	91
0000	223.1						12.4	0.752E-04	0.182E-04	6.61	16
000	210.3	-	2.0				1771	7 5	0.1425-04	1	9.
0000	714.9	• ~) M				-11.3	9	0.126E-04	17	9.
4000	212.3	-	0.4				-10.8	3	0.113E-04	-14.1	16
2000	210.5	_	5•1		0.1	.584E		7	0.101E-04	7	16
0005	509.4	_	6.7		0,1	565		2	0.911E-05	7	16
7000	207.8	-	0.8		70	•413E		0.275E-04		7	91
8000	205.3	٦,	o (~ ;	943	6.	<u> </u>		57.	9 ;
0006	201.	12.3				1 K	1 °	0.204E-04	0.507E-05	-11.9	9 4
000	104.7	• -	7.7		2 6	1856	13.60	0.1516-04		9	94.
2000	193.1	• ~	. 60		000	•	-2.6	28		9	16
3000	190.2	٠,			00	.121E	-1.0	0.110E-04		4-	15
84000	189.8	15.2	5.0		0	970	4.0	202		-3.	15
2000	192.2	18.1			00	0.777E-01	6.0-	0.753E-05	38E-0	-5.3	14
0009	8	2	9•6		00	3	-1.6	60	61E-0		13
7000	199.9	N	10.6		00	0.464E-01	1.5	20E-	إبنا	-5.3	12
8 8000	199.5	26.5	10.4	43E	00	0.3656-01	2.5	0.4385-05	0.110E-05	-4.2	12

-2.6 0.6 3.8 12.6 20.5 0.843E-06 0.675E-06 0.531E-06 0.398E-06 0.350E-06 0.310E-05 0.319E-05 0.269E-05 0.240E-05 0.212E-05 0.192E-05 PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE, 1962 10.22 10.22 10.23 0.287E-01 0.231E-01 0.186E-01 0.159E-01 0.132E-01 0.205E 00 0.173E 00 0.145E 00 0.122E 00 0.104E 00 0.889E-01 24.0 26.4 26.3 13.5 2.5 197.4 194.5 191.9 173.4 161.6 89000 90000 91000 92000 93000

9 2 2 2 2 2 2 3

SEASONAL MEAN PROFILE BARROW SPRING/FALL

0 8 S	11	21	25	22	21	22	52	27	20
ERROR GREES ST DEV	0.5	0.4	3.6	2.0	1.0	4.8	6.5	18.2	23.9
TEMP E	7.00	2.3	6	 	3.2	6.8	8.4	15.4	16.7
088	t t	99	σ.	0 0	ው ແ	0	œ	10	6 0
SOUTH ERROR M/SEC MEAN ST DEV	9.0	1.8	4.	40	2.3	13.4	29.6	83.4	131.1
	3.4	3.1	7.2	7•1 9•3	10.4	25.7	47.2	86.9	116.2
WEST ERROR M/SEC MEAN ST DEV	0.0	2.1	2.3	1.5	7.7	12.0	24.0	9.69	127.9
WEST MEAN	3.4								
NO OBS	11	23	27	5¢ 5¢	22	54	56	27	20
DIRECTION DEGREES MEAN	259.6	271.8	274.6	121.3	36.0	295.7	88.5	235.7	82.1
SPEED M/SEC MEAN	21.7	13.9	19.0	1.9	3.7	3	13.5	25.8	3•3
SOUTH COMPONENT M/SEC MEAN ST DEV	9.7	13•1 15•0	14.3	24.7	20.9	40.6	51.3	114.7	102.7
SOUTH MEAN	9.9	4.00	1.5	0	-3.0	-1.4	2.1	14.5	7.0-
WEST COMPONENT M/SEC MEAN ST DEV	21.8	23.0	27.0	31.1	28.9	29.5	0.04	6*69	71.7
WEST CL	21.3	13.9	18.9	-1.6	-2.2	3.0	-13.3	21+3	-3•3
ALTITUDE M MSL	35000	40000 45000	50000	00000	65000 70000	75000	80000	85000	00006

Appendix B

The annual mean temperature, pressure, and density profiles for Natal-Ascension and seasonal mean profiles for Wallops Island, Churchill, and Barrow, along with the corresponding wind parameters and error analyses for temperature and wind, are tabulated in the following tables [comparisons are made with values from "U.S. Standard Atmosphere Supplements, 1966" (Reference 3)]:

· Table	Station	Data	Page
B.1	Natal-Ascension	Annual	58
B.2(a)		Winter	60
B.2(b)	Wallops Island	Summer	62
B.2(c)		Spring/Fall	64
B.3(a)		Winter	66
B.3(b)	Churchill	Summer	68
B.3(c)	,	Spring/Fall	70
B.4(a)		Winter	72
B.4(b)	Barrow	Summer	74
B.4(c)		Spring/Fall	76

Table B.1.

ANNUAL MEAN PROFILE

NATAL

LTITUDE	*	TEMPERATURE**	URE**	****	*PRESSURE**	* * * *	****	*DENSITY***	***	ON C
M MSL	MEAN	DEG K	PCT DIF	MEAN	ST DEV PC	PCT DIF	MEAN	ST DEV PCT	PCT DIF	\$80
					1					
25000	218.1	5.0	11.4	0.247E 04	0.524E 02	-3.6	0.395E-01	0.606E-03	-2.2	m r
26000	223.6	•	•	• 212E	1264°C		10-331E-01	0.460	η,	•
2000	230.8	•	•	1635	10000	•	0.2275101	0.3346-03	0 1	9 (1
0000	226.1	7 .		1275	0.426		0.2025	0.410F+03		1 (*
0000	737.0			1001	0.2446		0.1745-01	0.225F-03	7	. «
31000	236.6	. 4		1035	0.244E		0.1516-01	0.127E-03	9 9	
32000	239.4			.875E	0.337E		0.127E-01	0.558E-03	15.3	'n
33000	241.1	5.2		.762E	0.282E		0.110E-01	0.423E-03	9.4-	'n
34000	242.2	6.4		•666E	0.225E		0.959E-02	0.344E-03	-3.8	^
35000	244.0	5.1	0•3		0.320E	•	0.821E-02	0.428E-03	7.5-	6
36000	244.7	7.7	•	.509E	0.205E	•	0.726E-02	0.300E-03	-2.2	23
37000	247.2	4•1	-0.1	9446E	0.168E	•	0.628E-02	0.236E-03	-2.0	30
38000	250.1	3.9	0.1	390E •	0.148E	•	0.543E-02	0.202E-03	-2.1	31
39000	252.9	3.9	7.0	•341E	0.131E	•	0.470E-02	0.181E-03	-2.3	32
4 0000	255.6	4.7	9•0		0.116E	-2.0	0.406E-02	0.162E~03	-2.7	33
41000	258.5	4.6	6.0	•261E	0.103E	•	0.352E-02	0.142E-03	-2.8	33
4 2 0 0 0	261.1	4.6	1.0	3622•	0.920E	•	0.306E-02	0.132E-03	-2.9	34
43000	263.1	4.7	1•0	.202E	0.786E	-1.7	0.267E-02	0.113E-03	-2.6	34
00044	265.0	5.1	8°.	.177E	0.721E	•	0.233E-02	0.103E-03	-2.5	34
4 5 0 0 0	566.9	5.7	0.8	•156E	0.616E	-1.6	0.204E-02	0.925E-04	-2.3	34
00094	268.2	5.8	0.5	•138E	0.550E	•	0.179E-02	0.781E-04	-2.0	34
4 7 0 0 0	269.2	5.8	0	•122E	0.483E	-1.4	0.157E-02	0.672E-04	-1.4	34
4 8 0 0 0	269.4	5.6	-0.2	.107E	0.424E	•	0.139E-02	0.564E-04	-1.3	34
00064	269.5	5.3	.0 .0	3676	0.396E	•	0.122E-02	0.504E-04	-1.3	4 (
20000	268.4	2.6	9.0	838E	0.348E	•	0.108E-02	0.448E-04	0.1	833
51000	267.5	6•1	6.0	- 740E	0.316E	œ ·	0.963E-03	0.398E-04	B .	60.0
52000	266.1	6.3	-1-	•652E	0.281E	•	0.8536-03	0.353E-04	0	
53000	79.49		o. 0	14 / V	0.245E	•	0.7365-03	0.5056-04		90
54000	262.4	.	٠. ا	1000	0.222E	•	50-11-03 0-07-11-03	0.2745.04	6 · 1 · 1	9.0
55000	260.4	n .		1444	144E		0.3746-03	2000000	† • •	9 6
1000	256.7	7		1 4	70.1.0		0.2656103	0.2145-04		
0000	252.0			100	0 1 3 4 F		0.4075-03	0.1835-04	7-1-	
0000	250.6	9 4		26.35	0.1.0F		0.3665-03	0.1615-04	7.	1 6
0000	24.7			2305	0.106		0.324F=03	0.156F+04	17	
61000	243.3	9.9	-2.5	00E	0.933E	9.69	0.287E-03	0.143E-04	-1.3	9 69
62000	239.7	•	-2.6	.174E	0.846E		0.2546-03	0.129E-04	-1.6	33
93000	235.9	9.9	-2.8	52E	0.761E	•	24E	0.112E-04	-1.7	33
64000	232.7	٠	-2.7	•131E	0.662E		376	0.941E-05	-2.4	33
65000	229.5	6.9	-2.6	•113E	0.591E	•	7 2 E	0.803E-05	-2.9	93
66000	226.0	٠	-2.8	-982E	0.534E	•	E I	0.711E-05	- A	E 6
9000	7.72.44		9 6 6	1777	10.44.0	10	7 2	0.6816-05	0.	35
0000	29672	•	9 7 1	102/	0.4400	•		0.5765.05	1 4 7 1	3.5
1000			6 6 6 6	1220 E 23E	10.00	•	, ,	0.00	1	3 6
71000	7000		-2.7	0.454F 01	0.315E	. 60	0.756E-04	0.526E-05	5.6	32
72000	207.0		-2.4	.387E	0.280E		32E	0.490E-05	4.9-	31
73000	204.5		-1.9	.329E	0.243E	-9.1	51E	0.448E-05	-7.2	31
74000	202 . 4	•	-1.3	.279E	0.209E	•	32E-	0.413E-05	-7.9	31
75000	201.1	9.8	-0.2	•236E	0.178E	9•6-	10E-	0.353E-05	-9.1	31
26000	199.8	10.1	0.7	00E	0.152E	•	30E-	0.286E-05	-10.0	31
77000	198.6	10.2	1.8	•169E	0.134E	4.6-	37E-	0.223E-05	-11.0	31
78000	197.9	11.3	3•3	0.143E 01		-9.2	52E-	0.185E-05	-12.1	30
19000	198.2	10.5	5•3	• 1 20E	0.107E 0	-8.6	2		-13.2	OR

00000000000000000000000000000000000000	200
1111111 4 4 4 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	69.6 0.0 96.3
0.139E 0.134E 0.1024E 0.0761E 0.076	0.243E-07 0.301E-07 0.000E 00
0.178E-04 0.1578E-04 0.9097E-05 0	
1 1 1 1 1 1	82.0 0.0 150.8
0.963E-01 0.847E-01 0.847E-01 0.5674E-01 0.567E-01 0.7493E-01 0.313E-01 0.313E-01 0.226E-01 0.226E-01 0.226E-01 0.226E-01 0.226E-01 0.226E-01 0.226E-01 0.226E-01 0.226E-01 0.226E-01 0.226E-01 0.226E-01 0.226E-01 0.226E-01	0.819E-02 0.769E-02 0.000E 00
0.102E 01 0.732E 00 0.619E 00 0.525E 00 0.377E 00 0.278E 00 0.159E 00 0.159E 00 0.166E 00 0.166E 00 0.116E 00	
7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	9.0 0.0 9.0 9.0 9.0
**************************************	75 75 70 70 70 70
2 1 4 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	226.5 230.3 291.1
3 3 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	104000 105000 106000

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE SUPPLEMENTS. 1966 15 N ANNUAL STANDARD ATMOSPHERE ABOVE 90 KM IS AVAILABLE FOR EVEN KILCMETER LEVELS ONLY

ANNUAL MEAN PROFILE NATAL

NO OBS		m	56	28	4 1	33	42	38	32	38	31	36	20	37	-
ERROR GREES	T DEV	0.2	6.0	1.0	2.3	1.4	1.9	2.1	2.2	2.1	2.2	5.9	3.8	6.1	0.0
TEMP E	MEAN	0.5	0.7	1:1	2.2	2•1	2.7	3.3	5.9	2.8	3,3	7.7	6.3	6.8	40.7
NO OBS		0	e	e	4	4	S	4	m	9	m	'n	7	9	0
SOUTH ERROR M/SEC	ST DEV	0.0	0.5	0.1	0.8	5.5	5.9	9.6	4.6	2.1	1.3	2.0	4.3	3.6	0.0
SOUTH M.	MEAN	0.0	1.8	2.5	4•1	7•3	5.6	14.0	12.5	9.6	10.4	12.7	23.4	31.7	0.0
ERROR SEC	T DEV	0.0	0.7	0.2	1.0	3.4	4.4	6.2	0.4	5.6	3.0	3.5	6.3	3.6	0.0
WEST ERROR M/SEC	MEANS	0.0	2.4	3.1	5.3	9.5	11.2	16.6	12.7	10.4	11.6	14.8	27.0	35.5	0.0
NO OBS		m	27	59	43	34	77	39	33	40	35	0	52	39	-
DIRECTION DEGREES	MEAN	88.8	65.3	251.6	238.7	256.2	278.4	270.2	285.5	278.6	84•1	86.0	18.0	63.1	18.6
SPEED M/SEC	ME NA	10.7	7.4	4.2	2.1	8 • 5	19.7	28.6	24.2	6.1	5.1	13.4	4.2	39.9	29.1
SOUTH COMPONENT M/SEC	ST DEV	2.1	89	5.7	10.7	12.5	18.3	16.1	20.0	16.2	30.5	35.0	55.5	71.3	0.0
SOUTH M	MEAN	-0.2	9.0	1.3	1.0	2.0	-2.9	10.	-6.5	6.0-	-0-5	6.0-	0.4-	-18.0	-27.5
COMPONENT M/SEC	3 1 DEV	9.1	15.8	22.9	30.2	25.4	20•3	20.7	16.2	27.3	34.7	30.3	45.4	79.1	0.0
WEST CO	MEAN	-10.7	4.7-	4•0	1.8	8 • 2	19.4	28.6	23•3	6.1	-5.1	-13.3	-1+3	-35.6	-9.3
ALTITUDE M MSL		30000	35000	40000	45000	20000	25000	00009	65000	10000	75000	80000	85000	00006	95000

Table B.2(a).

NO 08S

PCT DIF

					S	SEASONAL ME	AN PROFILE			
						WALLOPS	WINTER			
TUDE	**TEI MEAN	EMPERATURE DEG K ST DEV PC	URE**	* * **	*	PRESSURE** NI/SQ M ST DEV	****	* * * * * * * * * * * * * * *	*DENSITY** KG/CU M ST DEV	*****
0	÷	•	•	• 72	03	•939E 0	e.	07	• 326E	•
000	236.7	6.1	5.2	0.640E	0 0	0.274E 02	4 6	0.9425-02	0.420E-03	- 0
88				1 7	0	210E 0		6.68	.312E	
8	ě	•	•	.41	03	.180E 0	80	. 587	.2775	•
8	ċ	•	•	•36	03	.163E 0	8	• 508	.237E	•
0	٠,	•	•	.31	03	.143E 0	6	4.39	• 207E	•
0 0	ė	•	•	27	0 0	•135E 0	6 6	986	• 180E	
3 6		•		7 7	ם ס כ	1155 0	. 0		1225	• •
88				9 6	9 6	110E 0	10.	246	.128E	•
00				16	03	.103E 0	10	.215	.112E	
00	'n	6	•	41.	03	948E 0	01	187	•107E	•
0 0	٠,	•	•	: 15	0 0	.863E 0	0.	.163	• 102E	•
0 0		•	•	1.0	0 0	710F 0	0 -	1	4 7 5 5 E	•
9 6	• :	•	•	. 4	200	6110E 0		7.	7646F	·-
88	· ·			75	0 2	572E 0	::	100	721E	::
00			:	•66	02	.512E 0	10.	.887	•681E	2
00	ċ	•	-:	58	05	.457E 0	10.	• 784	.595E	2
88	å.	•	٠,	5.	05	409E 0	0.0	6693	• 526E	
9 6	• :	• 6		4.0	2 6	366E U	9 0	9 4	70777	
000	: :			34	02	290E 0	. 6	4.80	419E	1 ~
0				30	02	.256E 0	80	425	.386E	5
00	ŝ	ě	ė	•26	05	.224E 0	8	.375	.347E	5
88		•	ė,	53	05	.195E 0	· r	928	.308E	٦.
36				200	200	.169E O	• ;	707	244E	
8 8	•		• •		9 0	125F 0		222	217E	0
88	0				02	106E 0	Š	195	190E	9
00		•	÷	7	02	.913E 0	5.	170	.163E	9.1
00	٠.		ė.	66	0	.779E 0	4 (149	• 140E	•
0 0	ċ		e c	9	5 6	.667E 0		130	* 122E	7 0
3 6	• •	; ;	• •	• •	5 6	405F		100	9 0 0	- 6
88	: :		•	7.7	50	.428E 0		. 8 6 E	. 794E	
00		÷	•	4.7	0	.367E 0	:	.751	• 700E	•
0 0	.	÷ .	•	940	50	•311E 0	o q	40.	•656E	•
200	• •	• •	•	4.0	3 5	.228F 0		4 7 7 7	. 262E	- 0
200		·	: :	25	50	196E 0	7	707	386E	40
00	ó			57	:5	.175E 0	7	.346	.319E	-
8	÷		•	.18	01	.142E 0	-2.	• 296	• 260E	5
8 8	ů.	ġ.	•	-5	0	.129E 0	-2.	.257	• 208E	2
0 0		•	•	. :3	5 5	.107E 0	7	777	17/1	7
200	• •	• •		10	35	8745	0	166	.154E	
00	•	. "		8.	8	.814E-0	o	144	.155E	-
00	ċ	•	•	• 74	8	.701E-0	o	.123	•134E	2
CO	6.	ě.	•	69	8	.606E-0	o o	105	. 109E	-1 -
000	'n.	Š.	6.0	60.	38	.530E+0	9 -	916	7055	- د
000	. c		•		3 8	•>14E=0	-2-	6.56	. 638E	
200	•		-1.2	, 6	38	.420E-0	, e		9649e	u ~•
, !	•	;	 		,	:				

ALTITUDE M MSL

01 4 0 0 0 1 0 1 4 4 4 4 0 0 0 0 0 0 0 0
0.677E.06 0.666E.06 0.407E.06 0.750E.07 0.112E.07 0.000E
0.484E-05 0.401E-05 0.273E-05 0.273E-05 0.179E-05 0.179E-05 0.179E-05 0.179E-05
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0.377E-01 0.319E-01 0.263E-01 0.842E-03 0.1046E-02 0.124E-02 0.000E 00
0.275E 00 0.127E 00 0.152E 00 0.128E 00 0.127E 00 0.000E 01 0.738E-01
1000 1000 1000 1000 1000
8477 2000 2000 2000 2000
1998.0 1998.3 2004.1 1944.4 1948.4 1188.0 1182.4 177.3
9 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9

- 9900000

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE SUPPLEMENTS, 1966 45 N JANUARY STANDARD ATMOSPHERE ABOVE 90 KM IS AVAILABLE FOR EVEN KILOMETER LEVELS ONLY

SEASONAL MEAN PROFILE WALLOPS WINTER

OBS	10 9 2 5 7 5 7 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7	
TEMP ERROR Degrees Mean St Dev		0
TEMP DEG MEAN	4 C B C C C C C C C C C C C C C C C C C	19.2
NO OBS	100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-
SOUTH ERROR M/SEC MEAN ST DEV	00000000000000000000000000000000000000	0
SOUTH MEAN	1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	200.3
WEST ERROR M/SEC MEAN ST DEV	000000000000000000000000000000000000000	0
WEST MEAN		
NO OBS	11899999999999999999999999999999999999	-
DIRECTION DEGREES MEAN	20000000000000000000000000000000000000	71.6
SPEED M/SEC MEAN	4 10 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	30.8
SOUTH COMPONENT M/SEC MEAN ST DEV	111. 114. 114. 1184. 1184. 1186. 118	0.0
SOUTH MEAN	4 W I W W W W W W W W W W W W W W W W W	9.6-
COMPONENT M/SEC	10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0
WEST C	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	-29.5
ALTITUDE M MSL	ww44ww9arraa	00056

Table B.2(b).

SEASONAL MEAN PROFILE WALLOPS SUMMER

NEAN STORY POT DIF NEAN STORY POT DIF NEAN STORY POT DIF NEAN STORY POT DIF NEAN STORY POT DIF NEAN STORY POT DIF NEAN STORY POT DIF NEAN STORY POT DIF NEAN STORY POT DIF NEAN STORY POT DIF	ALTITUDE M MS!	*	Σ	rure**	* * * *	d. *	****PRESSURE****	:	****	***DENSITY***	* * * * * * * * * * * * * * * * * * * *	0 0
225.3 9 10 10 10 10 10 10 10 10 10 10 10 10 10		MEAN	<u> </u>	PCT DI	MEAN	-	ST DEV	0	MEAN	ST DEV		200
223.9 1.4 1.10 0.0234E 04 0.0774E 02 0.018 0	2000	223.0	2.	6.0-	73E			٠	5	94E=0	-0.5	2
225.3 1.0 1.15 0.1204E 04 0.1244E 02 -0.06 0.1247E-01 0.1349EE-03 0.09 226.8 3.2 2.2 0.151E 04 0.1244E 02 -0.06 0.1249EE-03 0	0000	223.9	;	-1.0	34E			'	4	46E-0	8.0-	7
228.6 2.8 2.9 2.0 0.2395 01 0.3395 03 0.3385 03	000	223.9	1.	-1.5	34E			'	7	98E-0	6.0	m
286.8 3.2 22.0 0.0101E 04 0.044E 02 - 114. 0.199E-011 0.559E-033 0.14. 0.159E-011 0.559E-033 0.14. 0.159E-012 0.159E-013 0.14. 0.159E-013 0.	000	226.3	ċ	-1-3	75E			•	69	59E -0	e .	m
259.1 4.14 5.17 5.17 5.17 5.17 5.17 5.17 5.17 5.17	000	226.8	m c	0 - 0 - 0) I E			• '	5 6	0 1 1 0 1 0 0 1 0 0 1 0 0 1	•	m (
255.2 5.7 -	000	220	,	13.2	U L			'	70	100		
254.5 8.7 -2.4 0.04516 0.0 0.04526 0.2 0.1039-0.1 0.40776-0.3 1.18 0.04726 0.3 0.3 0.0456 0.3 0.3 0.0456 0.3 0.3 0.0456 0.3 0.3 0.3 0.0456 0.3		230.2		3.6	J (L			•	1 4	35610	- a	n 4
255.6 7.2 2.8 0.0466 0.0 0.0456 0.0 0.0109-010 0.04076-03 0.0446 0.0 0.0466 0	000	734.3	٠ ۵	-2.4	1995 26E			١	2,5	39E-0		• •
259. 778 -279 0.6466 0.0 0.3566 0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0		725.0	ď	2.8	. u			'	. 0	07F-0	9 00	•
245. 7.7	200	230.4		-2.3	1 14			'	, 6	435-0	4.	, ~
264.5 7.7 -1.4 0.4026E 03 0.315E 02 0.11 0.701E-02 0.0459E-02 0.0459E-03 0.1045 02 0.255. 252.4 6.2 -1.0 0.375E 03 0.256E 02 0.115E 02 0.125E 02 0.0458E-02 0.0458E-03 0.125E 02 0.255. 252.1 7.1 -0.7 0.256E 03 0.125E 02 -2.5 0.333E-02 0.0458E-03 0.125E 02 0.125E 02 0.125E 03 0.125E 02 0.125E 03 0.125E	000	243.0	_	1 1 1	57E			'	2,	46E-0	1.7	- 00
256.2 6.1 6.2 6.2 6.2 6.2 6.2 6.2 6.2 6.2 6.2 6.2	000	246.5	7	1100	36E				5	99E-0	1.4	0
255.7. 6.2 -11 0.354E 0.3.24E 0.3.1F 0.3.24E 0.3.34E 0.3.24E 0.3.34E 0.3.34E </td <td>000</td> <td>248.2</td> <td>α</td> <td>-1-7</td> <td>36Z</td> <td></td> <td></td> <td>'</td> <td></td> <td>0.275E-0</td> <td>9.0</td> <td>10</td>	000	248.2	α	-1-7	36Z			'		0.275E-0	9.0	10
255.2 6.1 -0.8 0.239£ 03 0.219£ 02 -2.1 0.44£ -0.2 0.224£ -0.3 -1.1 261.1 3.1 0.0 0.206 03 0.137£ 02 -2.2 0.224£ -0.3 -1.1 261.1 3.6 0.0 0.206 03 0.131£ 02 -2.2 0.224£ -0.3 -2.1 265.7 6.8 -1.2 0.131£ 02 -2.2 0.134£ 02 0.224£ -0.3 -1.1 266.8 11.9 -1.2 0.131£ 02 -2.2 0.134£ 02 0.134£ 02 -2.2 0.134£ 02	000	252.4	9	-1.0	75E			١		0.268E-0	-0.5	11
255.1 7.1 -0.7 0.244E 0.0.137E 0.2.25 0.335E-0.2 0.225E-0.3 -1.6 255.1 7.1 -0.5 0.259E 0.0	000	255.2	40	8.0	25.			٠		0.245E-0	1.3	14
26.1.1 6.6 0.5 0.1576 0.2 0	000	258.1		20.	1 H			١		0.225E-0		15
265.7 6.3 6.1116 6.2 7.3 6.296 6.1116 6.2 7.3 6.296 6.1116 6.2 7.3 6.296 6.1176 6.2 7.3 6.296 6.1176 6.2 7.3 6.296 6.0 7.3 6.0 7.3 6.0 7.3 6.0 7.3 6.0 7.3 6.0 7.3 6.0 7.3 6.0 7.3 6.0 7.3 6.0 7.3 6.0 7.3 6.0 7.3 6.0 7.3 6.0 7.3 6.0 7.3 6.0 7.3 7.3 6.0 7.3 7.3 6.0 7.3 7.3 6.0 7.3 7	000	26141	or.		0.0			•		0.202E-0	-2-1	1.4
266.8 11.9 -2.8 0.1192E 03 0.1192E 02 -3.8 0.234E-02 0.1194E-03 -11.3 0.1195E 03 0.1195E-03 0.1195E		263.2	0	9.0	1 6			,		0.177E-0	-2-1	9 -
265.7 6.8 -1.5 0.1176 03 0.119E 02 -2.8 0.223E-02 0.110FE-03 -1.12 266.8 11.9 -2.1 0.110E 03 0.102E 02 -3.3 0.112E-02 0.110FE-03 -1.12 266.8 11.9 -2.1 0.102E 03 0.994E 01 -4.0 0.113E-02 0.108E-03 -1.12 267.1 11.2 -3.1 0.102E 03 0.896E 01 -4.0 0.113E-02 0.108E-04 -1.14 267.1 11.2 -3.1 0.102E 03 0.896E 01 -4.0 0.113E-02 0.108E-04 -1.14 267.1 18.1 -3.1 0.102E 03 0.896E 01 -4.0 0.113E-02 0.770E-04 -1.14 267.1 18.1 -3.1 0.102E 03 0.896E 01 -4.0 0.113E-02 0.770E-04 -1.14 267.1 18.1 -3.1 0.102E 03 0.691E 01 -4.0 0.113E-02 0.770E-04 -1.14 267.1 6.0 -3.2 0.709E 02 0.651E 01 -5.2 0.770E-04 -2.0 268.2 7.8 -3.2 0.709E 02 0.651E 01 -5.2 0.770E-04 -2.0 268.3 9.0 0.730E 02 0.651E 01 -5.0 0.874E-03 0.750E-04 -1.14 269.2 7.8 -3.2 0.709E 02 0.750E 01 -5.0 0.874E-03 0.750E-04 -1.14 269.2 7.8 -3.2 0.709E 02 0.750E 01 -5.0 0.874E-03 0.750E-04 -1.14 269.2 7.8 -3.2 0.709E 02 0.750E 01 -5.0 0.874E-03 0.750E-04 -1.14 269.2 7.8 -3.2 0.709E 02 0.750E 01 -7.0 0.874E-03 0.750E-04 -1.14 27.0 0.709E 02 0.750E 01 -7.0 0.774E-03 0.750E-04 -1.14 27.0 0.709E 02 0.750E 01 -7.0 0.774E-03 0.750E-04 -1.14 27.0 0.709E 02 0.750E 01 -7.0 0.774E-03 0.750E-04 -1.14 27.0 0.709E 02 0.750E 01 -7.0 0.774E-03 0.750E-04 -1.14 27.0 0.709E 02 0.750E 01 -7.0 0.774E-03 0.750E-04 -1.14 27.0 0.709E 02 0.750E 01 -7.0 0.774E-03 0.750E-04 -1.14 27.0 0.709E 02 0.750E 01 -1.10 27.0 0.709E 03 0.776E-04 -1.14 27.0 0.709E 03 0.709E 03 0.709E-04 -1.14 27.0 0.709E 03 0.709E 03 0.709E-04 0.750E-04 -1.14 27.0 0.709E 03 0.709E 03 0.709E-03 0.709E-04 0.750E-04	000	264.1		-1.2	32E			•		0.138E-0	-2.0	18
266.9 8.7 -2.1 0.1926 0.304026<	000	265.7		7	302			١		0.1196-0	-1.3	21
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264.0 7.84 -3.5 0.0.059 0. 0.598 05.6 0. 0.917E-03 0.700E-04 -2.0 0.508.0 0. 0.508.0 0. 0.508.0 02.4 0. 0.508.0 0. 0.508.0 0. 0.508.0 02.4 0. 0.508.0 0. 0.508.0 0. 0.508.0 02.4 0. 0.508.0 0. 0.508.0 02.4 0. 0.508.0 0. 0.508.0 02.4 0. 0.508.0 0. 0.508.0 02.4 0. 0.508.0 0. 0.508.0 02.4 0. 0.508.0 0. 0.508.0 02.4 0. 0.508.0 0. 0.508.0 02.4 0. 0.508.0 0. 0.508.0 0. 0.508.0 02.4 0. 0.508.0 0. 0.508.0 0. 0.508.0 02.4 0. 0.508.0 0. 0.508.0 02.4 0. 0. 0.208.0 0. 0.208.0 0. 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0.208.0 0. 0. 0.208.0 0. 0. 0.208.0 0. 0.208.0 0. 0. 0.208.0 0. 0. 0.208.0 0. 0. 0.208.0 0. 0. 0.208.0 0. 0. 0.208.0 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	000	266.7		.3	98E			•			-2.0	24
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266.2	000	264.0			 			îì		40110110 6450104	* 0	4 6
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255.4 9.8 -3.3 0.325E 02 0.312E 01 -7.8 0.504E-03 0.427E-04 -4.5 251.9 10.2 -3.7 0.325E 02 0.328E 01 -8.8 0.4477E-03 0.427E-04 -4.5 241.8 9.6 -4.8 0.228E 02 0.238E 01 -9.4 0.351E-03 0.427E-04 -4.5 241.6 9.6 -4.8 0.228E 02 0.208E 01 -9.4 0.351E-03 0.427E-04 -4.5 241.6 9.6 -4.8 0.228E 02 0.208E 01 -10.2 0.316E-03 0.326E-04 -4.6 23.6 0.214E 02 0.218E 01 -10.2 0.316E-03 0.278E-04 -4.6 23.6 0.218E 02 0.136E 01 -11.8 0.2741E-03 0.216E-04 -4.6 22.5 1 0.138E 01 -11.8 0.2741E-03 0.216E-04 -5.1 2.2 2.2 2.2 7.6 -6.1 0.139E 02 0.118E 01 -12.6 0.2241E-03 0.136E-04 -5.1 2.2 2.2 2.2 7.6 -6.1 0.139E 02 0.118E 01 -13.3 0.185E-03 0.136E-04 -5.1 2.2 2.2 2.2 7.6 -6.1 0.139E 02 0.118E 01 -13.3 0.185E-03 0.136E-04 -5.1 2.2 2.2 2.2 7.6 -6.1 0.139E 02 0.118E 01 -13.3 0.185E-03 0.136E-04 -5.1 2.2 2.2 2.2 7.6 -6.1 0.139E 02 0.118E 01 -13.3 0.185E-03 0.136E-04 -5.1 2.2 2.2 2.2 7.6 -6.1 0.239E 02 0.118E 01 -13.3 0.185E-03 0.136E-04 -5.1 2.2 2.2 2.2 7.6 -6.1 0.239E 02 0.146E 03 0.136E-04 -5.1 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2	000	260.5			7 0			1		0.5346.04		, t
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202.2 12.7 5.5 0.210E 01 0.238E 00 -17.5 0.424E-04 0.376E-05 -20.1 2 202.2 12.7 5.5 0.210E 01 0.208E 00 -16.5 0.36EE-04 0.376E-05 -20.7 2 201.9 13.3 7.8 0.179E 01 0.170E 00 -14.8 0.36EE-04 0.388E-05 -20.8 200.4 14.9 9.6 0.150E 01 0.125E 00 -12.7 0.226E-04 0.173E-05 -20.8 194.9 13.2 10.3 0.157E 01 0.110E 00 -12.7 0.226E-04 0.173E-05 -20.8		202	-	7-1	1 1			- 1		0	8.8	2.6
202.2 12.7 5.5 0.210F 01 0.208F 00 -16.5 0.362F-04 0.354F-05 -20.7 2 2 201.9 13.3 7.8 0.179F 01 0.170F 00 -14.8 0.316F-04 0.308F-05 -20.8 2 200.4 14.9 9.6 0.150F 01 0.125F 00 -14.7 0.262F-04 0.224F-05 -21.9 2 194.9 13.2 10.3 0.157F 01 0.110F 00 -12.7 0.226F-04 0.173F-05 -20.8	000	202		3.6	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			-17		0.376E-0	å	23
201.9 13.3 7.8 0.179E 01 0.170E 00 -14.8 0.310E-04 0.308E-05 -20.8 200.4 14.9 9.6 0.150E 01 0.125E 00 -14.7 0.262E-04 0.224E-05 -21.9 200.4 13.2 10.3 0.127E 01 0.110E 00 -12.7 0.226E-04 0.173E-05 -20.8 1		202.2	• -		10			17		0.354E-0	-20.7	22
200.4 14.9 9.6 0.150E 01 0.125E 00 -14.7 0.262E-04 0.224E-05 -21.9 2	000	201.9	•	6.7	79E			-14		0.308E-0	200	21
106.4 13.2 10.3 0.127E 01 0.110E 00 -12.7 0.226E-04 0.173E-05 -20.8	000	2002	14	9.6	30E			177		0-224E-0	21.	20
	000	196.9	13	10.3	3.E			-12		0.173E-0	20.	: 2

19	7 7	9 7	17	17	16	7.	13	13	13	σ.	7	9	S	4	4	4	4	4	4	4	e	m	m	m	e	m	e	m	m	7	7	7	~1	7	ς,	7	7	7	7
-20.1	0.01	16.4	-13.8	-12.1	-9.7	9.9-	-2.5	-0-3	1.5	0	7.6	0.0	14.8	0.0	17.8	0.0	24.6	0.0	30.6	0.0	37.9	0.0	45.6	0.0	30.2	0.0	21.4	••	16.1	0.0	-6.1	0.0	-5.6	0.0	-1.8	0.0	3.4	0.0	0•0
0.148E-05		, w	'n	'n	2	0.891E-06			_			_									~	_				_		~	_	_	_	-	60	æ	80	80	00	80	0.5846-08
0.193E=04	1405104	0.118E-04	0.996E-05	0.829E-05	0.697E-05	0.589E-05	0.503E-05	0.420E-05	0.350E-05	0.297E-05	0.246E-05	0.197E-05	0.170E-05	0.137E-05	0.116E-05	0.986E-06	0.835E-06	0.703E-06	0.600E-06	0.513E-06	0.435E-06	0.365E-06	0.302E-06	0.244E-06	0.191E-06	0.155E-06	0.127E-06	0.106E-06	0.891E-07	0.639E-07	0.535E-07	0.458E-07	0.397E-07	0.348E-07	0.312E-07	0.280E-07	0.254E-07	0.232E-07	0.211E-07
-11-1	9,7	-5.4	-3.1	6.0-	6•0	4•1	7.8	8 • 6	11.8	0.0	20•7	0.0	28•6	0	29.5	0.0	33•3	0.0	35.8	0.0	28.0	0.0	22.7	0.0	17.7	0.0	15.3	0.0	14.6	0	12.0	0.0	16.3	0.0	21.0	0	24.7	0.0	0.0
0.100E 00	0.700F=01	0.694E-01	0.611E-01	0.518E-01	0.4436-01	0.382E-01	0.306E-01	0.261E-01	0.224E-01	0.169E-01	0.163E-01	0.142E-01	0.674E-02	0.406E-02	0.420E-02	0.430E-02	0.4336-02	0.434E-02	0.427E-02	0.424E-02	0.368E-02	0.350E-02	0.335E-02	0.308E-02	0.277E-02	0.2435-02	0.210E-02	0.186E-02	0.164E-02	0.174E-02	0.160E-02	0.148E-02	0.138E-02	0.130E-02	0.121E-02	0.114E-02	0.107E-02	0.100E-02	0.959E-03
0.107E 01	0.7555	0.631E 00	0.530E 00	0.443E 00	0.369E 00	0.312E 00	0.264E 00	0.219E 00	0.183E 00	0.159E 00	0.132E 00	0.108E 00	0.966E-01	0.793E-01	0.673E-01	0.571E-01	0.485E-01	0.412E-01	0.350E-01	0.296E-01	0.236E-01	0.198E-01	0.166E-01	0.140E-01	0.119E-01	0.103E-01	0.901E-02	0.793E-02	0.700E-02	0.599E-02	0.544E-02	0.497E-02	0.4565-02	0.421E-02	0.391E-02	0.362E-02	0.337E-02	0.314E-02	0.293E-02
11.2	12.7	12.9	12.5	13.3	12.5	12.6	11.2	10.6	10.4	0.0	11.0	0.0	12.9	0	11.1	0.0	8•9	0.0	6.5	0.0	-4.3	0.0	-11.4	0.0	-6.1	0.0	6.0	0.0	6•1	0.0	25.4	0.0	29.8	0.0	30.4	0.0	28.2	0.0	0.0
12.0		10.7	10.9	12.9	14.6	16.4	15.7	15.2	15.0	15.5	19.6	25.2	12.6	13.6	14.6	15.8	18.0	20.8	23.9	28.1	25.9	27.4	26.3	24.1	18.0	15.9	21.8	25.2	31.5	12.0	17.1	20.5	22.0	22.5	23.3	24.0	23.5	23.7	26.7
193.7	000	186.5	185.8	187.0	185.7	185.9	183.6	182.6	182.3	187.8	188.8	191.4	198.4	201.5	201.2	201.8	202 • 4	204.0	203.0	201.5	189.0	188.0	189.6	198•2	216.0	233.8	248 • 8	262.4	278.5	323.2	349.6	373.2	394.9	414.5	429.7	442.7	454.7	463.8	475.1
80000	0000	83000	84000	8 5000	86000	8 7 3 0 0	88000	89000	00006	91000	92000	93000	00046	95000	00096	97000	98000	00066	100000	101000	102000	103000	104000	105000	106000	107000	108000	109000	110000	111000	112000	113000	114000	115000	116000	117000	118000	119000	120000

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE SUPPLEMENTS. 1966 45 N JULY STANDARD ATMOSPHERE ABOVE 90 KM. IS AVAILABLE FOR EVEN KILOMETER LEVELS ONLY

SEASONAL MEAN PROFILE WALLOPS SUMMER

o B S	61	12	16	13	15	17	12	11	σ.
ERROR SREES ST DEV	000	1:1	6.0	9 9	900	1.4	2.3	3.8	6.5
TEMP E DEGR	0.0	0.0	0.0	9 8	1:1	1.6	2.6	4.4	8.9
NO OBS	- 4	4 6	· w	4 W	4 (•	m	4	4
ERROR SEC ST DEV	000	0 0	0.0	e ~	7 7	7.0	1.4	0.4	10.5
SOUTH B M/SE MEAN ST	2.0	1.8	2.1	2.0	2.3	3.6	5.0	9•9	20.9
ERROR SEC T DEV	000	0.0	0.1	7.0	0.1	6.0	0.7	2.5	5.1
WEST ERROR M/SEC MEAN ST DEV	1.0	1.1	1.2	0 4	1.4	2.7	5.9	5,3	13.7
NO OBS	10	16	53	7 7 7 7	20	22	17	15	Ξ
DIRECTION DEGREES MEAN	83°4 89°7	78.0	87.2	96.5	4.00	96.1	347.3	341.0	314.6
SPEED M/SEC MEAN	15.8	34.0	0	49.1 50.9	51.2	13.7	3,3	39.1	41.8
SOUTH COMPONENT M/SEC MEAN ST DEV	2.3	14.0	11.8	14.0	19•6	33.4	52.7	63.0	100.9
SOUTH MEAN	-1.7	5.6	-1.9	5.8	4.0.	4	-3.5	-37.0	-29.3
COMPONENT M/SEC ST DEV	1.4	12.8	10.5	11.5	21.0	38.6	45.1	63.4	105.6
WEST CC	-15.7	133.3	0.04-		-51.2	-13.6	0.7	12.7	29.7
ALTITUDE M MSL	35000	4 5000	00000	55000 60000	65000	75000	80000	85000	00006

Table B.2(c).

SEASONAL MEAN PROFILE WALLOPS SPRING/FALL

32	32	31	28	52	21	18	13	10	ď	m	7	7	7	7	7	~	7	7	€,	7	7	7	~	~	7	~;	~	~3	7	~	7	7	~	7	~	7	
-2.7	-1.9	-2.2	-3.4	-3.5	-1.9	-1.0	0.0	4.7	0.0	6.6	0.0	8•9	0.0	13.2	0.0	14.3	0.0	15.9	0.0	6•0	0.0	1.3	0.0	4.5	0.0	9•6	0.0	9.9-	0.0	-21.5	0.0	-23.3	0.0	-18.2	0.0	0.0	
0.100E-05	0.825E-06	0.684E-06	0.627E-06	0.529E-06	0.478E-06	0.467E-06	0.400E-06	0.377E-06	0.149E-06	0.102E-06	0.104E-06	0.493E-07	0.244E-07	0.606E-08	0.312E-07	0.3295-07	0.254E-07	0.681E-08	0.254E-09	0.178E-07	0.225E-07	0.194E-07	0.151E-07	0.982E-08	0.957E-08	0.801E-08	0.632E-08	0.665E-08	0.546E-08	0.469E-08	0.401E-08	0.352E-08	0.318E-08	0.301E-08	0.279E-08	0.274E-08	
0.957E-05	0.810E-05	0.678E-05	0.562E-05	0.472E-05	0.403E-05	0.3425-05	0.294E-05	0.2535-05	0.222E-05	0.185E-05	0.156E-05	0.128E-05	0.110E-05	0.946E-06	0.788E-06	0.679E-06	0.5895-06	0.491E-06	0.383E-06	0.302E-06	0.252E-06	0.218E-06	0.189E-06	0.163E-06	0.143E-06	0.125E-06	0.103E-06	0.7950-07	0.593E-07	0.465E-07	0.381E-07	0.3295-07	0.292E-07	0.262E-07	0.238E-07	0.219E-07	
Ċ			-1.2	4.0-	4.0	1.9					0.0	8.5	0.0	7.6							0.0	-1.5	0.0	-3.2	0.0	-6.1	0.0	-9.5	0.0	-7.6	0.0	-3.7	0.0	-0.2	0.0	0.0	
0.441E-01	0.380E-01	0.337E-01	0.286E-01	0.260E-01	0.240E-01	0.212E-01	0.205E-01	0.173E-01	0.579E-02	0.285E-02	0.184E-02	0.105E-02	0.699E-03	0.499E-03	0.6495-03	0.999E-03	0.124E-02	C.140E-02	0.140E-02	0.134E-02	0-114E-02	0.950E-03	0.800E-03	0.664E-03	0.590E-03	0.499E-03	0.429E-03	0.365E-03	0.315E-03					0.124E-03	0.950E-04	0.749E-04	
0.531E 00	0.447E 00		0.315E 00		0.226E 00			0.142E 00		0.101E 00	0.872E-01	0.736E-01	0.624E-01	0.526E-01	0.443E-01	0.373E-01	0.313E-01	0.261E-01	0.220E-01	0.187E-01	0.161E-01	0.139E-01	0.120E-01	0.103E-01	0.890E-02	0.763E-02	0.654E-02	0.566E-02	0.501E-02	0.452E-02	0.412E-02	0.379E-02	0.349E-02	0.322E-02	0.299E-02	0.277E-02	
2.0	1.4	1.8	2.8	3.7	3.2	4.2	0.0	2.9	0.0	-1.6	0.0	0.7	0.0	-3.2	0.0	-5.3	0.0	-10.0	0.0	1:1	0.0	1.4	0.0	-3.0	0.0	-8.9	0.0	3.0	0.0	25.7	0.0	35.0	0.0	32.1	0.0	0.0	
14.3	14.7	14.9	15.5	17.1	21.2	28.1	16.4	17.0	5.0	5.4	8.8	4.8	2.1	0.5	10.6	14.4	15.4	12.4	12.8	2.8	3.9	4.6	2.9	0.9	0	0.5	1.0	4.7	8.6	14.7	19.6	24.1	27.0	32.9	37.7	43.7	
194.5	193.3	194.1	195.9	197.7	196.7		. 197.5	196.9	194.0	191.7	195.0	199.3	196.7	193.6	196.3	191.9	185.9	185.3	199.8	215.5	222.9	223.1	220.8	219.9	216.1	212.6	219.6	248.4	295.2	339.5	378.1	403.1	419.1	431.9	441.0	7.574	1
84000	8 5000	86000	87000	88000	89000	00006	91000	92000	93000	94000	95000	00096	9 7 0 0 0	98000	00066	100000	101000	102000	103000	104000	105000	106000	107000	108000	109000	110000	111000	112000	113000	114000	115000	116000	117000	118000	119000	120000	

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE SUPPLEMENTS. 1966 MID LAT SPRING/FALL STANDARD ATMOSPHERE ABOVE 90 KM IS AVAILABLE FOR EVEN KILOMETER LEVELS ONLY

SEASONAL MEAN PROFILE WALLOPS SPRING/FALL

0 N O		7	91	16	58	37	30	38	32	33	32	32	35	38	50
ERROR GREES	ST DEV	0.0	0.2	1.3	1.7	2 • 3	2 • 2	1.6	1.9	2 • 7	2.5	2 • 1	3 • 8	0.0	12.0
TEMP B	MEAN			1.0											
NO OBS		0	e	'n	s	6	'n	a 0	7	60	2	7	œ	0	7
SOUTH ERROR M/SEC	ST DEV	0.0	0.5	0.3	0.5	0.2	0.3	1.0	43.2	71.6	81.5	7.7	5.6	2.2	76.1
SOUTH M/	MEAN	0.0	6.0	1:1	1.6	2.0	2.2	2.8	50.4	44.0	43.1	0.4	7.1	7.6	56.6
T ERROR M/SEC	ST DEV	0.0	0	0.5	0.3	0.2	0.5	0.5	14.1	73.1	49.8	6.0	1.6	2.0	76.8
wes1 ⊼	MEAN	0.0	0.5	0.1	0.8	1.2	1.5	1.6	7.3	44.2	24.5	2.8	4.7	6.1	55.2
NO OBS		7	12	18	38	45	0	4 6	43	745	40	45	745	77	22
DIRECTION DEGREES	MEAN	93.0	286.2	292.4	276.2	272.7	270.8	261.2	267.6	251.9	265.8	245.6	263.6	350.6	356.5
SPEED M/SEC	MEAN	18.9	4.7	15.7	24.1	28.4	28.2	23.8	19.0	19.1	21.1	2•0	15.7	10.5	5,3
SOUTH COMPONENT M/SEC	ST DEV	0.0	3•3	6.3	8•6	11.4	12.7	21.4	16.4	19.2	20.4	30.5	50•3	63.5	78.5
SOUTH	MEAN	1.0	-1.3	0.9-	-2.6	-1.3	1.0-	3.6	0.7	5.9	1.5	0	1.7	-10.4	-5.3
COMPONENT M/SEC	ST DEV	0.0	10.7	17.7	23.8	31.3	31.6	33.0	36.6	38.4	36.8	42.1	34.9	45.5	56.0
WEST CC	MEAN	-18.9	4.5	14.5	24.0	28.3	28.2	23.5	19.0	18•2	21.0	1•B	15.6	1.7	0.3
ALTITUDE M MSL		25000	30000	35000	40000	45000	20000	25000	00009	65000	70000	75000	80000	8 5000	00006

Table B.3(a).

SEASONAL MEAN PROFILE CHURCHILL WINTER

AL TITUDE	*		URE**	*	*	***************************************	*	****	* *	* * * *	Š C
J E	MEAN	ST DEV	PCT DIF	MEAN		ST DEV	PCT DIF	MEAN	ST DEV	PCT DIF	3
26000	203.3	w	-4.1	0.180E	70	0.350E 02	0.9-	0.309E-01	0.106E-02	-2.0	7
27000	203.7	4.		0.152E	3 6	0.169E 02	1.9-	0.261E-01	0.806E-03	12.4	m «
29000	209.1	ייי נ	2.2	0.110E	40	.829E	-7.6	0.183E-01	0.398E-03	0.4	t 4
30000		٠.	-2.1	0.937E	03	.517E	-8.0	0.1546-01	0.205E-03	0.9-	4
31000	212.4	2.0	-2.0	0.799E	60	0.424E 01	-8-3	0.131E-01	0.189E-03	4.9-	4
32000	213.8	2.5	1.8	0.682E	600	•223E	00 00 00 01	0 111E-01	0.1536-03	9 1	4 4
33000		2.5	11.6	0.5367	n e	249E	, 4 s s	0.941E102	0.480F=03	1 7 7 1	at or
34000	• •			0.4546	9 6	318F	2.6	0.7275-02	0.462E-03	-1.2	13
36000		6.6	-2.8	0.395E	03	304E	-2.0	0.631E-02	0.465E-03	99	17
3 7000	:	9.7	-2.6	0.339E	60	0.257E 02	-2.3	0.535E-02	0.384E-03	7.0	19
38000		10.2	-2.5	0.292E	03	.230E	-2.6	0.454E-02	0.329E-03	0.0-	19
39000	•	10.7	-2.3	0.251E	60	.206E	-3.0	0.386E-02	0.283E-03	9.0-	16
00004	•	0	-2•1	0.216E	60	•183E	e e	0.3295-02	0.238E-03	0.	20
4 1000	232.8	٦.	-1.7	0.190E	e c		00 F	0.285E-02	0.2436-03	90	22
4 2000	0 1	: :	o 1	199T • 0	9 6	17.00	7.1	0.2115-02	0.2695		9 6
000644	241.0	12.6	> * T	0.1446	9 6	1515	1 ·	0.1815-02	0.1845-03		2 8
4 4000	244.0	13.3		0.109E	9 6	136E	-1.7	0.156E-02	0.168E-03	4.0-	28
46000	246.99	14.3	0.1	0.953E	05	.121E	-1.8	0.134E-02	0.154E-03	9.0-	28
4 7000	249.0	14.7	-1-1	0.832E	02	.108E	-2.0	0.116E-02	0.139E-03	8.0-	28
4 8000	249.B	14.	-1.7	0.726E	02	.975E	-2.2	U.101E-02	0.123E-03	7.0-	28
4 9000	549.9	13.	-2.7	0.634E	02	1.1	-2.5	0.884E-03	0.109E-03	0.1	28
50000	250.1	12.	-3.5	0.554E	02	•781E	-2.9	0.772E-03	0.971E-04	0.5	28
51000	250.4	12.	-3.7	0.488	05	•717E	-2.7	0.679E=03	0.934E-04	0,0	50
52000	251+3	12.	13.4	0.427E	70		* ·	0.3426-0.5	0.84/E-04	7.0	6 0
53000	252.2	4 t	1 0	0.375F	3 6	170C	000	0.4526-03	0.6965-04	n «	600
1000	751.5	1 4		0.285	20	439E	10.0	0.396E-03	0.616E-04	1.00	53
56000	250.3	7	-2.6	0.249E	0.2		6.41	0.348E-03	0.538E-04	-2.1	29
57000	249.1	13.	-2.4	0.218E	02		-5+3	0.305E-03	0.476E-04	-2.7	53
58000	248.0	12.	-2.2	0.190E	02		-5.5	0.268E-03	0.426E-04	-3.2	53
29000	246.8	12.1	-2.0	0.166E	02		ŝ	35E-0	0.385E-04	-3.7	53
00009	545.4	15.	-2.1	0.145E	05		•	96	0.348E-04	9.6	29
61000	244.3	5	-2.4	0.126E	200	0.198E 01	n (0.181E-03	0.3146-04	100 P	520
62000	1.542		8 7 8	0.1100	3 5		N 1	200	0.2425=04	190	. 0
0000	227			חייים. ס	; ;	7 1	- 0	, ,	0 - 20 9F - 0 4	7 7	; ;
65000	235.4	12	-5.2	0.722E	; ;	0.109E 01	9.6	0.107E-03	0.180E-04	-3.2	53
9,000	234.0	=	-5.6	0.625E	010	.937E	7.6-	0.934E-04	0.154E-04	-3.6	29
6 7 0 0 0	233.4	Ė	-5.6	0.541E	01	.803E	-10.2	0.811E-04	0.134E-04	7.4-	58
68000	233.1	:	-5.5	0.469E	0.		-11.0	0.703E-04	0.118E-04	-5.3	58
00069	232.5	12.	-5.6	0.405E	0	•585E	-11.7	0.611E-04	0.103E-04	0.9	29
2000	232.5	12.	-5.2	0.351E	55	1004	-12.5	0.3 29E-04	0.400E-02	· ·	67
71000	232.3	٠,	, t	0.363E	3 5	0.421E 00	7.61-	0.3075-04	9 6		* °
73000	231.4	16.		• `	5 0	300F		3	96E-0	-10.9	53
7 000	229.9	17		0.196E	: 0		6.41-	6	P	:	5 2
75000	227.6	17.	-2.9	٦.	010		-15.4	19	9		58
76000	224.9	17.	-3.2	7	0		-15.9	27	E-0	5	58
7 7 0 0 0	223.6	17.	-2.9	7	0		*16.3	6	325E-0	-	58
7 8000	221.4	18	5.0	0.107E	50	0 126E 00	16.7	0.1/1E=04	0.2765-05	13.4	26
00067	214.2	٠,	0.6	• •	38	•	-17.7	9 6	87F=0	14.0	9 00
	3.013	•	•		;		•		!		}

4.017	18.7	-1.4	0.584F 00	0.683E-01	-18.2	0.947F=05	0.137E-05	1,6.4	- 10
	20.5	4.0-		0.589E-01	1.8.1	0.812E-05		-17.3	27
	17.5	9.0-	0.430E 00	0.502E-01	-18.2	0.705E-05		-17.2	56
	12.9	4.0-		0.427E-01	-18.4	0.606E-05	_	-17.6	56
_	12.4	-0.5		0.355E-01	-18.5	0.528-05	-	-17.6	56
	15.9	-0.5	0.267E 00	0.299E-01	-18.5	0.452E-05		-17.3	25
~	16.9	1.2	0.226E 00	0.256E-01	-19.0	0.380E-05		-19.3	23
0	20.5	1.7		0.182E-01	-18.4	0.328E-05	_	-18.9	21
7	24.3	6•4	0.163E 00	0.142E-01	-19.2	0.270E-05		-22.1	19
~	28.2	0.0	0.138E 0C	0.125E-01	0.0	0.228E-05		0.0	18
6	19.1	3.5	0.117E 00	0.116E-01	-19.5	0.192E-05		-21.8	17
211.3	4.5	0.0	0.100E 00	0.874E-02	0.0	C.165E-05		0.0	15
_	10.0	-1.0	0.855E-01	0.681E-02	-19.4	0.144E-05	_	-17.9	11
_	13.2	0.0	0.701E-01	0.461E-02	0.0	0.121E-05		0.0	3 0
0	15.8	-7.8	0.5946-01	0.386E-02	-23.3	0.106E-05	_	-15.4	σ,
ď	8.7	0.0	0.510E-01	0.345E-02	0.0	0.888E-06	0.662E-07	0.0	'n
-	6.2	-7.6	0.430E-01	0.316E-02	-24.7	0.753E-06		-17.1	4
6 0	6.4	0.0	0.363E-01	0.270E-02	0.0	0.640E-06	_	0.0	4
196.6	4.	6.6-	0.307E-01	0.224E-02	-27.3	0.546E-06	_	-17.3	4
4	12.3	0.0	0.2595-01	0.195E-02	0.0	0.464E-06	_	0.0	4
۲.	13.4	-7.5	0.219E-01	0.153E-02	-30.4	0.374E-06	_	-22.0	4
9.	17.9	0	0.187E-01	0.111E-02	0.0	0.310E-06	_	0	4
209.8	16.5	80 80	0.159E-01	0.179E-03	-32.7	0.267E-06	_	-23.0	4
•	14.8	•	0.136E-01	0.496E-03	0	0.226E-06	_	0.0	4
4.	12.6	-11.5	0.1165-01	0.396E-03	-35•6	0.193E-06	_	-24.2	4
6	13.7	0	0.996E-02	0.367E-03	0	0.161E-06		0.0	4
ω	11.5	-0.5	0.856E-02	0.322E-03	-38.3	0.134E-06		-28.7	4
ű	20.9	0.0	0.739E-02	0.259E-03	0.0	0.111E-06		0.0	4
ñ	39•3	-4•1	0.642E-02	0.184E-03	-40.3	0.946E-07	0.152E-07	-33.1	4
0	48.7	0.0	0.559E-02	0.187E-03	0.0	0.808E-07	0.136E-07	0.0	4
262.2	50.7	0.2	0.490E-02	0.256E-03	-41.8	0.668E-07	0.878E-08	-37.3	4
4	51.8	0.0	0.432E-02	0.317E-03	0.0	0.554E-07	0.625E-08	0.0	4
294.7	48.3	5.4	0.384E-02	0.361E-03	-42.5	0.4595-07	0.379E-08	-41.7	4
315.7	42.7	0.0	0.344E-02	0.373E-03	0.0	0.382E-07	0.289E-08	0.0	4
333.5	45.9	12.1	0.3105-02	0.362E-03	-42.3	0.3265-07	0.288E-08	-45.1	4
ñ	48.2	0.0	0.282E-02	0.360E-03	0.0	0.284E-07	0.2936-08	0.0	4
59.8	55.4	14.1	0.256E-02	0.353E-03	-41.6	0.250E-07	0.274E-08	-45.0	4
74.2	63.7	0.0	0.234E-02	0.352E-03	0.0	0.220E-07	0.263E-08	0.0	4
7.00	40.4	0.0	0.215F-02	0.3415-03	0.0	0.1955-07	0.24.75 D	0.0	4

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE SUPPLEMENTS. 1966 60 N JANUARY STANDARD ATMOSPHERE ABOVE 90 KM IS AVAILABLE FOR EVEN KILOMETER LEVELS ONLY

PROF 1LE	WINTER
MEAN	
SEASONAL	CHURCHILL

08 S	20	11	22	23	27	25	27	22	54	22	29	33	26	
ERROR REES ST DEV	0.1	0.3	0.7	1.3	1.3	1.4	1.9	1.9	2.0	2.1	4.4	6.7	11.2	
TEMP DEG MEAN	0.7	6.0	1.3	1.9	2.7	2.6	3.2	2.8	3.6	3.5	6.3	8.5	14.4	
NO OBS	s	~	11	11	16	13	16	11	12	11	16	19	20	r
SOUTH ERRUR M/SEC MEAN ST DEV	0.5	0.5	1.5	5.6	3.3	3.0	4•1	3.8	3.4	3.8	18.2	17.6	38.8	13.3
SOUTH MEAN	1.5	1.8	3.5	5.5	8.5	8.4	11.2	11.7	10.2	10.3	26.4	39.4	62.8	
WEST ERROR M/SEC MEAN ST DEV	4.0	0.5	1.6	2.8	3.3	3.1	4.2	3.7	3.5	3.9	17.2	18.4	38.9	
WEST MEAN 3	1.5	1.7	3.5	5.7	8.7	8.7	11.3	11.8	10.3	10.4	25.6	39.8	63.5	5. 50
088 088	٥	12	27	58	32	30	32	27	30	27	34	39	28	,
DIRECTION DEGREES MEAN	286.7	284.4	282.0	278.1	270.8	259.5	259.3	263.5	266.8	254.1	238•2	312.2	298.5	7 000
SPEED M/SEC MEAN	29.0	45.4	42.2	52.5	56.0	58.2	43.0	35.8	41.0	31.7	32.5	11.5	25.4	6 36
SOUTH COMPONENT M/SEC MEAN ST DEV	31.0	22.5	54.9	25.0	41.1	33.1	30.9	35.9	41.8	45.6	27.5	93.1	105.0	7.0.5
SOUTH MEAN	-8.3	-11.3	-8	7.4	-0.7	10.5	7.9	4•0	2 • 2	8.6	17.1	-7.7	-12.1	0.77*
COMPONENT M/SEC ST DEV	18.2	22.7	36.1	47.3	46.4	47.2	45.8	47.6	41.2	54.1	57.1	64.2	86.8	1,37.0
WEST O	27.7	43.9	41.3	51.9	56.0	57.2	42.3	35.6	6.04	30.5	27.7	8.5	22.3	9 70 4
ALTITUDE M MSL	30000	35000	00007	4 5000	50000	55000	6 0000	65000	70000	75000	80000	85000	60006	0000

Table B.3(b).

SEASONAL MEAN PROFILE CHURCHILL SUMMER

0. 358EE-01 0.000E 0 0. 358EF-01 0.000E 0 0. 358EF-01 0.000E 0 0. 230EF-01 0.000E 0 0. 230EF-01 0.000E 0 0. 198EF-01 0.000E 0 0. 198EF-02 0.109EF-02 0.109EF-03 0.129EF-03 0.129EF-0	00000000000000000000000000000000000000	0.2346 0.1346 0.1346 0.1346 0.1346 0.1346 0.03446 0.03446 0.03446 0.0346		00044884444444444444444444444444444444
11.1 (.358E-01 0.000E 00 1.1.4 (.358E-01 0.000E 00 0.200E 00 0.200		00000000000000000000000000000000000000	444444 <i>wwwwwwwwwwwwwwwwwwwwww</i>	00000000000000000000000000000000000000
11.5			, 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	00000000000000000000000000000000000000
11.6			444mmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmm	00000000000000000000000000000000000000
12.0			00000000000000000000000000000000000000	00000000000000000000000000000000000000
1.5 0.17 E = 0.1 0.000 E 0.000			20000000000000000000000000000000000000	00000000000000000000000000000000000000
13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9		00000000000000000000000000000000000000	,0000000000000000000000000000000000000	00000000000000000000000000000000000000
1.0 0.00 0		QQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQ	,0000000000000000000000000000000000000	00000000000000000000000000000000000000
1.3 0.80 6.50 6		00000000000000000000000000000000000000		00000000000000000000000000000000000000
1.5 0.806E-02 0.151E-03 0.699E-02 0.131E-03 0.699E-02 0.131E-03 0.699E-02 0.131E-03 0.699E-03		30000000000000000000000000000000000000		00000000000000000000000000000000000000
1.5 0.693E-02 0.151E-03 0.151E-03 0.151E-02 0.151E-03 0.151E-02 0.151E-03		000000000000000000000000000000000000000		00000000000000000000000000000000000000
1.6 0.598E-02 0.143E-03 1.4.1.9 0.598E-02 0.199E-03 1.2.3 0.447E-02 0.199E-03 1.2.3 0.447E-02 0.199E-03 1.2.2 0.256E-02 0.299E-04 1.2.3 0.296E-02 0.299E-04 1.2.3 0.299E-05 1.		00000000000000000000000000000000000000		00000000000000000000000000000000000000
1.9 0.517E-02 0.159E-03 1.2.3 0.474E-02 0.159E-03 1.2.3 0.474E-02 0.159E-03 1.2.2 0.291E-02 0.291E-02 0.292E-04 1.2.3 0.292E-04 0.292E-04 1.2.3 0.292E-04 0.292E-04 1.2.3 0.292E-05 1.2.3 0.29	2014 10 20 20 20 20 20 20 20 20 20 20 20 20 20			0.000000000000000000000000000000000000
12.3 12.3 12.4 12.5 12.6 12.7 12.7 12.7 12.7 12.7 12.8 12.8 12.9				0.000000000000000000000000000000000000
12.0 (2.39) EF 02 (2.40) EF 03 (2.40) EF 04 (2.40) (2.40) EF 05 (2.40)				00000000000000000000000000000000000000
12.0 12.2 12.2 12.2 12.2 12.2 12.2 13.3 13.2 13.2 13.2 13.2 13.3 13.2				0.25986 0.25986 0.25986 0.12066 0.13566 0.13566 0.13566 0.1376 0.1076 0.
12.0 0.341E-02 0.344E-04 0.25.2 0.246E-04 0.256E-02 0.256E-04 0.256E-02 0.256E-04 0.256E-05 0.25				0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
12.2 0.298E-02 0.893E-04 12.5 0.208E-02 0.793E-04 13.2 0.106E-02 0.793E-04 13.2 0.106E-02 0.793E-04 13.3 0.1076E-02 0.793E-04 13.4 0.1076E-02 0.795E-04 14.4 0.1076E-02 0.794E-04 14.4 0.796E-03 0.296E-04 14.4 0.796E-03 0.296E-04 14.4 0.796E-03 0.296E-04 15.4 0.796E-03 0.296E-04 15.4 0.796E-03 0.296E-04 15.5 0.796E-03 0.296E-04 17.5 0.796E-03 0.196E-04 17.6 0.796E-03 0.196E-05 17.6 0.796E-03 0.196E-05 17.6 0.796E-03 0.196E-05 17.6 0.796E-03 0.196E-05 17.6 0.796E-03 0.796E-05 18.8 0.796E-05 19.8 0.796E-0		C C C C C C C C C C C C C C C C C C C	00000000000000000000000000000000000000	0.227E 03 0 0.227E 03 0 0.156E 03 0 0.157E 03 0 0.157E 03 0 0.157E 03 0 0.457E 02 0 0.457E 02 0 0.557E
12.5 12.5 12.6 12.6 12.7 12.8 13.0 13.1 13.2 13.1 13.2 13.6 13.6 13.7 13.6 13.7 13.6 13.7 13.7 13.7 13.7 13.7 13.7 13.8 13.7 13.8	2000 2000 2000 2000 2000 2000 2000 200			0.1566603 0.1566603 0.1566603 0.131603 0.101603
12.7 13.2	20 20 20 20 20 20 20 20 20 20 20 20 20 2		00000000000000000000000000000000000000	0.1568 0.1368 0.1378 0.1018 0.1018 0.9918 0.9918 0.9918 0.9918 0.9918 0.9918 0.9918 0.9918 0.9918 0.9918 0.9918 0.9918
12.8 13.0 13.0 13.0 13.1 13.2	2012 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0))	001946 001018 00
13.2 0.176E-02 0.574E-04 13.2 0.176E-02 0.574E-04 13.2 0.176E-02 0.574E-04 13.2 0.176E-02 0.574E-04 13.2 0.176E-02 0.576E-04 13.2 0.176E-02 0.576E-04 14.1 0.856E-03 0.276E-04 14.1 0.856E-03 0.276E-04 14.1 0.866E-03 0.276E-04 14.1 0.866E-03 0.276E-04 14.1 0.866E-03 0.276E-04 14.1 0.866E-03 0.276E-04 15.2 0.176E-04 15.2 0.176E-04 15.2 0.176E-04 17.2 0.276E-03 0.176E-04 17.2 0.176E-03 0.176E-05 17.2 0.176E-05 0.176E	20 20 20 20 20 20 20 20 20 20 20 20 20 2	200200000 V44WWWWWWWW		0.156F 03 0.137F 03 0.107F 03 0.107F 03 0.851F 02 0.440F 02 0.450F 02 0.555F 02 0.555F 02
13.0 0.176E-02 0.577E-04 13.4 0.156E-02 0.577E-04 13.5 0.151E-02 0.596E-04 14.1 0.955E-02 0.396E-04 14.4 0.955E-03 0.296E-04 14.4 0.955E-03 0.296E-04 14.4 0.955E-03 0.296E-04 15.1 0.666E-03 0.296E-04 15.1 0.666E-03 0.296E-04 15.4 0.588E-03 0.296E-04 15.6 0.486E-03 0.296E-04 15.6 0.486E-03 0.175E-04 17.6 0.256E-03 0.175E-04 17.6 0.256E-03 0.175E-04 17.6 0.197E-03 0.197E-05 17.6 0.197E-03 0.197E-05 17.6 0.197E-03 0.197E-05 17.6 0.107E-03 0.425E-05 18.8 0.507E-04 0.435E-05 18.8 0.507E-04 0.386E-05 19.3 0.507E-04 0.386E-05		3 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	0.137E 03 0.107E 03 0.107E 03 0.04951E 03 0.0496 02 0.04
13.2 13.4 13.6 13.6 10.121E=02 0.454E=04 14.1 0.955E=03 0.750E=03 0.750E=03 0.750E=03 0.750E=04 15.1 0.664E=03 0.750E=04 15.4 0.750E=03 0.750E=04 15.4 0.750E=03 0.750E=04 15.4 0.750E=03 0.750E=04 17.0 0.750E=03 0.175E=04 17.0 0.750E=03 0.175E=05 17.0 0.750E=03 0.175E=05 17.0 0.750E=03 0.175E=05 17.0 0.750E=03 0.175E=05 17.0 0.175E=04 0.175E=05 17.0 0.175E=05 0.		2200000	8888888	0.121E 03 0.101E 03 0.107E 03 0.0.840E 02 0.0.442E 02 0.0.655E 02 0.0.005E 02 0.0.655E 02 0.0.005E 02 0.0.655E 02 0.0.005E 02
13.6 0.137E-02 0.495E-04 13.6 0.107E-02 0.495E-04 14.4 0.495E-03 0.296E-04 14.4 0.495E-03 0.296E-04 15.4 0.496E-03 0.229E-04 15.4 0.496E-03 0.229E-04 15.4 0.496E-03 0.229E-04 15.4 0.496E-03 0.229E-04 15.4 0.496E-03 0.239E-04 15.4 0.496E-03 0.239E-04 17.5 0.496E-03 0.134E-04 17.5 0.496E-03 0.134E-04 17.6 0.496E-03 0.134E-05 17.6 0.496E-03 0.134E-05 17.6 0.496E-03 0.495E-05 17.6 0.496E-03 0.495E-05 17.6 0.496E-03 0.495E-05 18.8 0.496E-05 18.8 0.496E-05 18.9 0.496E-05		202000	10000000000000000000000000000000000000	0.995 E 02 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
13.6 13.6 13.6 14.4 14.4 14.4 14.4 14.4 14.4 14.4 14.4 14.4 14.4 14.4 15.1 10.8847E-03 10.256E-04 15.4 10.864E-03 10.256E-04 15.4 10.864E-03 10.256E-04 15.4 10.864E-03 10.256E-04 10.4 10.664E-03 10.256E-04 10.4 10.664E-03 10.256E-04 10.4 10.664E-03 10.256E-04 10.607E-03 10.106E-04 10.607E-03 10.106E-04 10.256E-03 10.106E-04 10.256E-03 10.106E-04 10.256E-03 10.106E-04 10.256E-03 10.106E-04 10.256E-03 10.106E-05		000000	200000	0.4951E 02 0 0.4951E 02 0 0.492E 02 0 0.655E 02 0
13.6 (a) 107E-02 (b) 245E-04 (c) 107E-02 (c) 107E-04 (c) 107E-05 (00000	22222	0.840E 02 0 0.840E 02 0 0.655E 02 0
13.8 0.107E-02 0.345E-04 14.1 0.955E-03 0.234E-04 14.7 0.464E-03 0.235E-04 15.4 0.465E-03 0.225E-04 15.6 0.465E-03 0.225E-04 15.9 0.465E-03 0.225E-04 16.1 0.465E-03 0.225E-04 16.7 0.455E-03 0.137E-04 17.0 0.255E-03 0.137E-04 17.0 0.255E-03 0.136E-04 17.0 0.255E-03 0.136E-04 17.0 0.255E-03 0.136E-04 17.0 0.255E-03 0.136E-04 17.0 0.156E-03 0.136E-05 17.0 0.156E-03 0.136E-05 17.0 0.156E-03 0.136E-05 17.0 0.156E-03 0.136E-05 17.0 0.156E-03 0.136E-05 17.0 0.156E-03 0.455E-05 18.5 0.405E-04 0.435E-05 18.5 0.405E-04 0.435E-05 18.5 0.507E-04 0.435E-05 19.0 0.702E-04 0.435E-05 19.3 0.405E-05		4444	00000 00000	0.840E 02 0.3 0.742E 02 0.3 0.55E 02 0.2 0.578E 02 0.2
14.1 0.955E-03 0.294E-04 14.4 0.4847E-03 0.239E-04 14.4 0.4847E-03 0.239E-04 0.239E-05 0.139E-04 0.239E-05 0.139E-04 0.239E-05 0.139E-05	யயங்கர	4444	02 00 00 00 00 00 00 00 00 00 00 00 00 0	0.742E 02 0.3 0.655E 02 0.2 0.578E 02 0.2
14.7 0.847E-03 0.258E-04 -4.7 0.756E-03 0.235E-04 -5.4 0.588E-03 0.235E-04 -5.5 0.652E-03 0.235E-04 -6.5 0.462E-03 0.137E-04 -6.5 0.462E-03 0.137E-04 -6.5 0.356E-03 0.137E-04 -7.0 0.255E-03 0.137E-05 -7.0 0.156E-03 0.055E-05 -7.0 0.156E-03 0.055E-05 -7.0 0.156E-04 0.435E-05 -8.2 0.702E-04 0.435E-05 -8.3 0.502E-05 -9.3 0.502E	யங்கர்	444	0020	0.655E 02 0.2 0.578E 02 0.2
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	29E		0000	0.578E 02 0.2
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	29E	0 0) (0.5/8E 02 0
15.1 0.664E-03 0.225E-04 15.4 0.58E-03 0.225E-04 15.6 0.45E-03 0.222E-04 15.9 0.45E-03 0.219E-04 16.1 0.410E-03 0.115E-04 16.5 0.324E-03 0.115E-04 17.0 0.255E-03 0.115E-04 17.1 0.255E-03 0.115E-04 17.2 0.255E-03 0.115E-04 17.4 0.255E-03 0.114E-04 17.5 0.15E-03 0.346E-05 17.6 0.15E-03 0.42E-05 17.6 0.105E-03 0.42E-05 17.7 0.105E-03 0.42E-05 17.8 0.925E-04 0.455E-05 18.5 0.607E-04 0.455E-05 18.5 0.607E-04 0.386E-05 19.3 0.607E-04 0.386E-05	29E	0	٠	
15.4 0.588E-03 0.219E-04	1		0 20	0.509E 02 0
15.6 0.521E-03 0.12E-04 -6.1 0.410E-03 0.197E-04 -6.1 0.410E-03 0.197E-04 -6.5 0.35E-03 0.197E-04 -6.7 0.35E-03 0.197E-04 -7.0 0.25E-03 0.196E-04 -7.4 0.25E-03 0.196E-04 -7.5 0.196E-03 0.196E-04 -7.6 0.196E-03 0.196E-04 -7.6 0.196E-03 0.956E-05 -7.6 0.105E-03 0.975E-05 -7.6 0.105E-03 0.975E-05 -7.7 0.105E-03 0.975E-05 -7.8 0.925E-04 0.435E-05 -8.2 0.607E-04 0.435E-05 -8.3 0.607E-04 0.435E-05 -9.3 0.607E-04 0.386E-05 -9.3 0.607E-04 0.607E-05 -9.3 0.607E-05 0.607E-05 -	8 2	Š	0 7 0	0.449E 02 0
15.9 0.462E103 0.197E104 16.1 0.365E103 0.191E104 16.7 0.324E103 0.181E104 17.0 0.255E103 0.110E104 17.2 0.255E103 0.110E104 17.5 0.156E103 0.110E104 17.5 0.156E103 0.110E104 17.6 0.156E103 0.104E105 17.6 0.156E103 0.779E105 17.6 0.105E103 0.779E105 17.6 0.105E103 0.779E105 17.6 0.105E103 0.779E105 18.0 0.802E104 0.779E105	87E	0.1	02 0	0.395E 02 0
10.00	1 0			0 60 3076 0
10.1 (0.30 fg = 0.9) (0.30 fg	9 6	5 0	200	0.3485.02
16.5 0.35E-03 0.175E-04 17.0 0.25E-03 0.167E-04 17.2 0.25E-03 0.196E-04 17.4 0.25E-03 0.196E-04 17.5 0.196E-04 17.6 0.175E-03 0.935E-05 17.6 0.136E-03 0.935E-05 17.6 0.136E-03 0.935E-05 17.7 0.105E-03 0.642E-05 17.7 0.105E-03 0.642E-05 18.0 0.808E-04 0.435E-05 18.0 0.808E-04 0.435E-05 18.5 0.607E-04 0.435E-05 18.5 0.507E-04 0.435E-05 18.5 0.507E-04 0.435E-05 18.5 0.507E-04 0.435E-05 18.5 0.507E-04 0.435E-05	3E	•	2	0.306E 02 0
17.0 0.224E-03 0.167E-04 -7.2 0.225E-03 0.119E-04 -7.4 0.225E-03 0.119E-04 -7.5 0.195E-03 0.119E-04 -7.6 0.175E-03 0.893E-05 -7.6 0.156E-03 0.893E-05 -7.6 0.156E-03 0.893E-05 -7.6 0.120E-03 0.893E-05 -7.6 0.105E-03 0.873E-05 -7.7 0.105E-03 0.573E-05 -7.8 0.925E-04 0.573E-05 -8.2 0.805E-04 0.573E-05 -8.2 0.805E-04 0.573E-05 -8.2 0.805E-04 0.573E-05 -8.3 0.805E-04 0.8386E-05 -8.5 0.805E-04 0.8386E-05	38E	;	020	0.268E 02 0
17.0 0.288E-03 0.150E-04 17.2 0.255E-03 0.114E-04 17.4 0.255E-03 0.114E-04 17.5 0.195E-03 0.104E-04 17.6 0.175E-03 0.935E-05 17.6 0.175E-03 0.843E-05 17.7 0.120E-03 0.42E-05 17.7 0.120E-03 0.42E-05 17.7 0.120E-03 0.42E-05 18.2 0.80E-04 0.435E-05 18.2 0.80E-04 0.435E-05 18.5 0.80E-04 0.435E-05 18.5 0.80E-04 0.435E-05 18.5 0.80E-04 0.435E-05 18.5 0.80E-04 0.435E-05 18.5 0.80E-04 0.435E-05 18.5 0.80E-04 0.80EE-05 18.5 0.80E-04 0.80EE-05	23E	0	02 0.1	0.235E 02 0.1
7.2 0.255E-03 0.134E-04 7.4 0.225E-03 0.134E-04 7.5 0.195E-03 0.196E-04 7.6 0.195E-03 0.955E-05 7.6 0.136E-03 0.955E-05 7.7 0.156E-03 0.775E-05 7.7 0.156E-03 0.775E-05 7.7 0.105E-03 0.642E-05 7.7 0.105E-04 0.435E-05 8.2 0.702E-04 0.435E-05 18.5 0.524E-04 0.386E-05 9.3 0.524E-04 0.386E-05	360	0	02 01	0.206F 02 0.1
7.6 0.199E-03 0.119E-04 17.6 0.199E-03 0.119E-04 17.6 0.199E-03 0.104E-04 17.6 0.196E-03 0.104E-05 17.6 0.196E-03 0.104E-05 17.6 0.196E-03 0.779E-05 17.6 0.196E-03 0.779E-05 17.6 0.196E-03 0.776E-05 17.6 0.196E-05 0.196E-05 18.8 0.576E-05 18.8 0.576E-05 18.8 0.576E-05 19.3 0.451E-04 0.326E-05 19.3 0.451E-05 19.3 0.451E-04 0.326E-05 19.3 0.451E-05 19.3 0.	1 4			0 100 100 0
7.5 (0.199E-03 0.199E-05 17.5 (0.199E-03 0.129E-05 17.5 (0.199E-03 0.129E-05 17.5 (0.199E-04 0.129E-05 18.5 (0.199E-04 0.1399E-05 18.5 (0.199E-04 0.1399E-05 18.5 (0.199E-04 0.1399E-05 19.3 (0.199E-05 19.3 (0.199E-0		•		20 36 1710
17.5 0.199E-03 0.104E-04 17.6 0.154E-03 0.935E-05 17.6 0.154E-03 0.843E-05 17.6 0.156E-03 0.842E-05 17.7 0.105E-03 0.642E-05 17.8 0.925E-04 0.453E-05 18.2 0.807E-04 0.455E-05 18.5 0.607E-04 0.386E-05 18.5 0.607E-04 0.386E-05 18.5 0.451E-04 0.386E-05 18.5 0.451E-04 0.386E-05	376	٩	20	0.156E UZ U+8
7.6 (0.175E-03 0.995E-05 -7.6 (0.136E-03 0.724E-05 -7.6 (0.120E-03 0.724E-05 -7.7 (0.105E-03 0.642E-05 -7.8 (0.925E-04 0.495E-05 -8.0 (0.8026E-04 0.495E-05 -8.2 (0.607E-04 0.495E-05 -8.5 (0.607E-04 0.436E-05 -9.3 (0.524E-04 0.366E-05	39E	•	02 0.1	0.136E 02 0.7
7.6 0.154E-03 0.843E-05 17.6 0.136E-03 0.779E-05 17.6 0.136E-03 0.779E-05 17.7 0.105E-03 0.642E-05 17.7 0.925E-04 0.435E-05 18.5 0.576E-05 18.5 0.576E-05 18.8 0.524E-04 0.326E-05 19.3 0.451E-04 0.451E-05 19.3 0.451E-		۲.	02 0.7	02 0.7
-7.6 0.136E-03 0.779E-05	26E	۰	02 0.6	0.102E 02 0.6
-7.6 0.120E-03 0.724E-05 -7.7 0.105E-03 0.642E-05 -7.8 0.925E-04 0.642E-05 -8.0 0.808E-04 0.495E-05 -8.2 0.702E-04 0.435E-05 -8.5 0.607E-04 0.386E-05 -9.3 0.524E-04 0.326E-05		0.5	01 0.5	0.884E 01 0.5
17.7 0.105E-03 0.672E-05 17.8 0.925E-04 0.573E-05 18.0 0.802E-04 0.573E-05 18.5 0.607E-04 0.286E-05 18.5 0.607E-04 0.286E-05 19.3 0.51E-04 0.235E-05 19.3 0.51E-04 0.235E-05	LL C	1	0.10	4-0 10 FLAC
17.7 (0.410) (10 10 10 10 10 10 10 10 10 10 10 10 10 1
17.8 0.925E-04 0.573E-05 18.0 0.808E-04 0.495E-05 18.2 0.702E-04 0.435E-05 18.5 0.607E-04 0.386E-05 19.3 0.451E-04 0.334E-05 19.3 0.451E-04 0.334E-05	J	•		10 37 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
-8.0 0.808E-04 0.495E-05 -8.2 0.702E-04 0.455E-05 -8.5 0.607E-04 0.386E-05 -8.5 0.524E-04 0.354E-05 -9.3 0.451E-04 0.326E-05	63E	0	010	9 0.557E 01 0.3
-8.2 0.702E-04 0.435E-05 16. -8.5 0.507E-04 0.386E-05 16. -8.8 0.524E-04 0.326E-05 16.		0.3	01 0.3	0.474F 01 0.3
-8.5 0.607E-04 0.386E-05 -6.1 -8.8 0.524E-04 0.354E-05 -6.1 -9.3 0.451E-04 0.326E-05 -6.1	100	י י		10 10 10 10 10 10 10 10 10 10 10 10 10 1
-8.5 0.607E-04 0.386E-05 -6. -8.8 0.524E-04 0.354E-05 -6. -9.3 0.451E-04 0.326E-05 -6.	371		1	0 10 1204.0
-8.8 0.524E-04 0.354E-05 -6.	36E	0	010	0.339E 01 0.2
-9-3 0-451E-04 0-326E-05 -6-	4			29.45
-9.3 0.451E-04 0.326E-05 -6.	7	•	7	0.2845 01 0.5
	76E	•	010	0.238E 01 0.1
10.0 0.202F=05 15.	F		0.0	0.0
	, ,	•		0 10 1010
-10.5 0.328E-04 0.245E-05 -		•	70	0.163E 01 0.
3 0.274F-04 0.219F-05 -8	ū	5	01.0	1.0 10 34F 0 .
0 CO 167700 to 147700 COT	,		•	

12	12	12	12	12	12	12	11	01	æ	7	•	S	7	~1	-	7	-	-	~	~	-	-	-	-	7	-	-	-	٦,	-
-10.7	-12.3	-13.5	-11.7	-9.7	0.8-	-6.5	-5.8	-7.6	0.6-	-15.7	0.0	-17.5	0.0	-24.7	0.0	-34.6	0.0	-34.9	0.0	-32.7	0.0	-28.5	0.0	-23.3	0	-20.1	0.0	-18.9	0.0	-20•1
0.195E-05	0.170E-05	0.146E-05	0.120E-05	0.100E-05	0.855E-06	0.697E-06	0.625E-06	0.547E-06	0.571E-06	0.436E-06	0.2335-06	0.136E-06	0.103E-06	0.8346-07	0.000E 00	0.000E 00	00 3000°C	0.000E 00												
										0.292E-05																				
-11.1	-11.1	-10.7	-10.2	-10.1	-10.4	-11.1	-11.4	-14.8	-15.9	-18.7	0.0	-19.1	0.0	-25.5	0.0	-31.3	0.0	-29.3	0	-27.5	0.0	-25.9	0.0	-26.1	0.0	-27.5	0.0	-29.9	0.0	-32.8
0.9645-01	0.8176-01	0.693E-01	0.588E-01	0.502E-01	0.431E-01	0.369E-01	0.317E-01	0.218E-01	0.1586-01	0.886E-02	0.757E-02	0.700E-02	0.528E-02	0.443E-02	0.000E 00	0°000E	0.000E 00													
0.110E 01	0.910E 00	0.746E 00	0.610E 00	0.497E 00	0.403E 00	0.325E 00	0.264E 00	0.206E 00	0.166E 00	0.130E 00	0.106E 00	0.869E-01	0.660E-01	0.543E-01	0.4135-01	0.345E-01	0.291E-01	0.248E-01	0.211E-01	0.180E-01	0.153E-01	0.132E-01	0.113E-01	0.96eE-02	0.832E-02	0.716E-02	0.619E-02	0.535E-02	0.464E-02	0.403E-02
-0-3	1.5	3.5	1.8	-0.2	-2.4	8.4.	-5.9	-7.5	-6.7	-2.2	0.0	-1.6	0.0	-0.5	0.0	6.2	0.0	10.5	0.0	10.3	0.0	7•0	0.0	0.1	0.0	-5.1	0.0	0.6-	0.0	-11.1
8.5	9.1	9.5	9.3	9.5	9.8	0.6	7.0	9. 4	9.1	15.9	12.1	7.6	0.8	0.9	0.0	0	0.0	0	0	0.0	0	0	0	0	0	0	0	0	0	0.0
169.9	168.6	167.4	164.7	161.2	157.7	153.8	152.1	149.4	150.7	157.9	160.9	164.8	167.4	172.9	180.3	190.9	199.8	204.7	208.5	210.2	212,6	213.2	214.7	217.5	219.5	222.7	225.4	229 • 8	233.9	240.0
80000	91000 B	82000	83000	84000	85000	86000	87000	88000	00068	00006	91000	92000	93000	00076	00056	00096	97000	00086	00066	100000	101000	102000	103000	104000	105000	106000	107000	108000	109000	110000

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE SUPPLEMENTS, 1966 60 N JULY STANDARD ATMOSPHERE ABOVE 90 KM IS AVAILABLE FOR EVEN KILOMETER LEVELS ONLY

SEASONAL MEAN PROFILE CHURCHILL SUMMER

NO OBS	250	7 7 7	13 16	15	13	17	10
ERROR GREES ST DEV	0 4		 	1.0	2.0	2.0	2.0
TEMP E DEGE MEAN	1.1	7.63	2.1	2.0	 	1.6	2.4
o s s	00	00	00	00	00	00	0
SOUTH ERROR M/SEC MEAN ST DEV	00	00	00	00	000	000	0
SOUTH MEAN	00	00	000	00	00	000	0
ERKOR SEC ST DEV	00	00	00	00	000	00	0
WEST ERROR M/SEC MEAN ST DEV	000	00	00	00	000	000	0
NO OBS	2.2	7 7	13	12	17	17	10
DIRECTION DEGREES MEAN	109.4	7.59	67.6 78.3	98.5	86.3	49.2	279.8
SPEED M/SEC MEAN	11.9	17.3	25•3 33•3	24•4 41•6	57.1 62.7	23.0	52.4
SOUTH COMPONENT M/SEC MEAN ST DEV	8°6 6°8	7°7	11.3	28•6 20•1	17.3	46.0	101.7
SOUTH MEAN	60.0	90	-9.6 -6.7	4.0	-3.6	-15.0	6.8
COMPONENT M/SEC	0.9	12.9	10.0	15.2 19.0	26.3	52.9	6.09
WEST CO	-11.2	-15.5	-23.4	-24.4	-57.0	-17.4	51.6
ALTITUDE M MSL	35000	45000	50000 55000	60000	70000	85000	00006

Table B.3(c).

SEASONAL MEAN PROFILE CHURCHILL SPRNG/FALL

AL TITUDE	**TE	⋖	JRE**	* * * * *	****PRESSURE****	* * * *	****	******************	***	Q.
30 30 8	MEAN	ST DEV	PCT DIF	MEAN	ST DEV	PCT DIF	MEAN	ST DEV	PCT DIF	880
34000	228.0	0.0	-2.4	11.1	•000E	١	0.969E-02	0.000E 00		-
35000	231.0	11.1	-2.2	1.4	.283€	-2.1	0.847E-02	0.100E-03		
36000	229 • 4	12.5	14.1	0.476E 03	0.285E 02		C. /23E-02	0.135E-03	en c • • •	3 -0
000	235.8	7	4		.231F	•	0.5246-02	0.201F-03		"
39000	239.2	12.6	.3.3		.218E	16.3	0.448E-02	0.221E-03		::
4 0 0 0 0	242.9	14.5	-2.9		.205E	'	0.383E-02	0.228E-03		11
41000	246.7	16.7	-2.5	1.1	•194E	•	V.328E-02	0.226E-03		11
4 2 0 0 0	246.5	15.6	-2.6		.198E	•	0.287E-02	0.205E-03	•	12
4 3000	250.8	•	-2.9		• 187E	•	0.246E-02	0.186E-03		5
0004	252.4	•	4 1		•173E	•	0.214E=02	0.158E-03		<u>.</u>
45000	254 • 3	13.2	-3.	,	• 159E	•	0.185E=02	0.141E-03	1	
0000	256.7	12.60	0 1 1		0.14/E 02		0.1616-02	0.1215-03	0 4] E
0000	256.9	•			124F	1	0.1235-02	0.114F-03	١	13
4 9000	256.8		-5.1		.113E	-	0.108E-02	0.109E-03		1 2
20000	256.6		-5.1		.103E	7	0.956E-03	0.104E-03		13
51000	257.2	6.7	6.4-		.939E	7	0.837E-03	0.992E-04		13
52000	257.8	8.3	T-4-7		•848E		0.733E-03	0.931E-04	-8.4	13
53000	257.9	7.1	-4.2		•762E	7	0.643E-03	0.869E-04		13
24000	257.1	6.9	-3.9		•682E	7	0.566E-03	0.805E-04	-10.2	13
55000	255.8	7.2	-3.6		•608E	7	0.499E-03	0.741E-04		13
56000	254.4	9 0	4 C		•541E	7	0.4405	0.677E=04	*	61.
2000	253.1	e .	7 6 6		1000	7 1	0.5886-03	0.6165-04		7 .
2000	20167	*	7.0		3472	1	201246.0	401111111111111111111111111111111111111		7 -
0000	2000	•	12.0		30100	1 7	0.2445	0.4955.04	17	ת קר
6,000	24642		-3-3		293F	17	0.233F-03	0.380E-04	1	13
62000	241.9	4.6	3.6		.259E	'	0.206E-03	0.336E-04	-13.7	13
63000	238.5	4.6	4.6-		.228E	7	0.182E-03	0.303E-04	7	13
94000	236.2	8.9	-2.8		•201E	7	0.160E-03	0.275E-04	7	13
9 2000	234.2	8.5	-2.1	44.5	76E	-17.7	0.140E-03	0.251E-04		13
9000	232.4	•	-1.2		.154E	7	0.122E-03	0.227E-04		13
67000	230.5	•	4.0-		•134E	1	0.106E-03	0.201E-04		E .
68000	228.6	8.2	o .		•116E	7	0.929E-04	0.175E-04		
20000	6.977		† r		0.100E 01	7 7	0.4076104	0.1535-04		
1000	223.5	0 0	, t		. 75.F	17	0.6095-04	0.1346-04	9.0	3 5
72000	22243	7.5	9		949	· ~	0.527E-04	0.104E-04		3 2
73000	220.7	7.0	4.5		53E	7	0.457E-04	0.919E-05		13
14000	219.1	7.1	5.2		.471E	ī	0.395E-04	0.808E-05		13
7 5000	217.5	7.3	5.9		386	7	C.342E-04	0.714E-05	7	13
76000	214.8	7.1	6.1		4334	7	0.296E-04	0.623E-05	-19.2	
1,000	2000	້ໍ	•		7 .	7	0.2375104	0.0446-05	1	0 €
18000	1907	5 -	7.4				0.2235104	0.1000000000000000000000000000000000000	7	1 -
00067	202.3	11.0	0 - 4			1 1	4	0.3236-03	2 1	7 -
B 1000	201.2	11.7	5.5			101	3	0.270E-05	2.5	13
82000	199.6	11.8	4.	4.1	9	110	120	0.228E-05	-13	13
83000	199.0	12.5	4.4		.90	î	2	0.195E-05	-12	13
84000	197.6	13.6	3.6		73	•	367	0.165E-05	7	13
8 5000	198.1	15.0	3.9		50	٩	751	0.140E-05	6	75
86000	196.1		2.9	1	98	9-	540E-0	0.117E-05	Γ,	77
87000	194.3	18.5	6.7		0.306E-01	-6.2	40.	0.9496-06	• •	75
88000	173.0	•	n •		53	•	_	00-13200	ޕ9-	71

12	• 00	7	9	4	m	7
15.8	0	-3.4	0.0	-6.3	0.0	7.6-
0.5935-06	0.354E-06	0.220E-06	0.974E-07	0.479E-07	0.6595-07	0.104E-06
0.387E-05	0.276E-05	0.234E-0	0.192E-05	0.158E-05	0.129E-05	0.107E-05
-6.3	0	-6.8	0.0	6.71	0.0	-17.4
0.190E-01	0.834E-02	0.7845-02	0.834E-02	0.982E-02	0.870E-02	0.839E-02
0.210E 00	0.150E 00	0.124E 00	0.102E 00	0.873E-01	0.703E-01	0.560E-01
7.0	0	-2.3	0.0	-1.2	0.0	-8.2
18.8	24.9	21.4	19.2	19.5	17.2	9 • 6
191.9	191.7	186.8	186.8	192.4	188.6	181.3
00068	91000	9 2 0 0 0	93000	00076	9 5 0 0 0	00096

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE SUPPLEMENTS. 1966 MID LAT SPRING/FALL STANDARD ATMOSPHERE ABOVE 90 KM IS AVAILABLE FOR EVEN KILOMETER LEVELS ONLY

SEASONAL MEAN PROFILE

CHURCHILL SPRNG/FALL

OBS	61066694441194 121111111	· m
TEMP ERROR DEGREES MEAN ST DEV		11.7
TEMP DEG MEAN	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	14.7
NO OBS	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	7
SOUTH ERROR M/SEC MEAN ST DEV		66.1
SOUTH M/ MEAN	4 5 5 6 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	1111.2
WEST ERROR M/SEC MEAN ST DEV		72.7
WEST MEAN	90101011001000000000000000000000000000	115.9
NO OBS	7 + 8 8 4 5 6 0 6 9 9 0 9 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	6
DIRECTION DEGREES MEAN	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	254.5
SPEED M/SEC MEAN	2000 2000 2000 2000 2000 2000 2000 200	26.1
SOUTH COMPONENT M/SEC MEAN ST DEV	100.3 120.0 120.0 120.0 115.0 118.0 120.0	9.49
SOUTH MEAN	111111000000000000000000000000000000000	6.9
COMPONENT M/SEC ST DEV	4 5 7 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	0.69
WEST CO MI MEAN	0 4 2 2 4 2 4 2 4 5 4 5 4 5 4 5 6 6 6 6 6 6 6 6 6 6 6 6	25.2
ALTITUDE M MSL	00000000000000000000000000000000000000	00056

Table B.4(a).

SEASONAL MEAN PROFILE

BARROW WINTER

AL TITUDE	**TE	EMPERATURE**	IURE**	****	***PRESSURE***	* * * * * * * * * * * * * * * * * * * *	* * * * * *	****DENS_ITY***	****	NO NO
30.5	MEAN	ST DEV	PCT DIF	MEAN	ST DEV	PCT DIF	MEAN	ST DEV	PCT DIF	
33000	241.8			36E	0.261E		106	0.348E-03		2
34000	230.3	14.4	4.7	0.599E 03	0.469E 02	9,1	0.905E-02	0.292E-03	4 ·	.
35000	728.1			4 4	0.00		0 4	0.301F-03		. 5.
37000	229.7			80E	0.366E		5.5	0.278E-03		16
38000	229.6			28E	0.347E		497	0.267E-03		16
39000	229.7			83E	0.325E		53	0.253E-03		91
0000	230.1			τ 2	0.305E		365	0.245E-03	-	9!
41000	232.7			1. F	0.287E		319	0.230E-03	٠,	71
42000	234.1			11 L	0.269E		2 .	0.454E-03	٠,	A .
00067	235.2			4 u	0.225		4 6	0.2345-03		67
000	127.0			3 5 6	0.2055		2 6	0.2225-03		4 -
4 4 2 0 0 0	237.7			1 14 10	0.186E		. 6	0.206E-03		16
47000	238.6			28E	0.168E		34	0.190E-03		16
48000	238.9			390	0.151E		117	0.1756-03		19
00064	239.2			316	0.135E		2	0.161E-03		19
20000	239.1			360	0.121E		96	0.145E-03		19
21000	239.1			305	0.108E		9	0.132E-03		о (
52000	239.1			61E	0.964		266	0.121E-03		61
53000	239.4			9 6	0.637E		0 0	0.1025-03		•
54000	23.40			11 to	0.447		0 4	0.9675.04		10
5,5000	730.8			3 6	0.564E		384	0.899E-04		16
57000	240.6			28E	0.483E		333	0.799E-04		10
58000	241.3			98E	0.413E		289	0.684E-04		19
9 9 0 0 0	241.1			72E	0.353E		251	0.588E-04		19
00009	239.4			4 8 1 1	0.301		216	517E		18
61000	237.8			28E	0.255E		5	0.448E-04		3
62000	236.3			7 7 7	0.6155		0 1	300E		0 4
0000	7.54.5			U U	0.100		2 2	777F		
00044	231.9			7 20 5	0.131E		100	233E		9 7
9,000	229.9			2 6 E	0.111E		9.5	0.198E-04		18
67000	228.2			40E	0.940E	'	830	168E	-2.2	18
68000	225.9			999	0.793E	•	723	0.143E-04		18
00069	222.7			910	0.665E	•	69	0.124E-04		18
70000	219.6			# C	0.004	•		0.0725		9 9
12000	215.0			507	0.375	•	7	0.848E-05		9 6
73000	213.5			156	0.302E	•	35	0.718E-05		18
74000	212.4			84E	0.241E	•	305	0.586E-05		1.8
75000	211.5			5.7E	0.192E	•	261	0.475E-05	•	18
76000	211.4			344	0.1536	•	77	0.331F=05	• •	0 0
7,000	213.8			1 4 7	0.0555	•	9 6	0.2665-05		9 6
78000	20100			30F	0	•	3.0	0.220E-05	•	81
00000	221.8			14E	0.558E	٠	11	0.178E-05	'	17
8 1000	219.6			13E	0.446	•	984	0.139E-05	•	17
8,2000	218.7			25E	0.364	•	946	0.109E-05	•	17
8 3000	218.7			50E	0.304	•	726	0.948E-06	•	17
94000	221.6			86E	0.262	•	613	0.731E-06	٠	17
85000	224.1			326		٠.	0.5216-05	0.5315-06		17
86000	223.7			u u		•	1 0	0-440F-04		
9 /000	77			1 0 1			0	1		•

		-			
-29.3	-25.4	19.5	-17.6	-30.3	o •
0.345E-06 0.289E-06	0.254E-06 0.216E-06	0.236E-06	0.102E-06	0.000E 00	0.000E 00
0.333E-05 0.294E-05	0.259E-05 0.230E-05	0.198E-05	0.1446-05	0.877E-06	U.659E=06
-23.8	-21.5	4-02-	-20.6	-22.6	•
0.145E-01 0.107E-01	0.927E-02 0.847E-02	0.773E-02	0.671E-02	0.000E 00	0.000E 00
0.213E 00 0.185E 00	0.158E 00 0.136E 00	0.116E 00	0.842E-01	0.600E-01	10-3826-0
8.4 7.8	6.1	2.0	1.00	12.0	•
18.5	20.1	22.1	10.9	0	•
224.1	214.7	206.0	202.9	238.2	0.472
88000 89000	90000	93000	94000	96000	000

95500000

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE SUPPLEMENTS, 1966 60 N JANUARY STANDARD ATMOSPHERE ABOVE 90 KM IS AVAILABLE FOR EVEN KILOMETER LEVELS ONLY

SEASONAL MEAN PROFILE BARROW WINTER

NO OBS	9	20 26	22	25	53	70	54	28	31	21	4
ERROR SREES ST DEV	00	0.0	1.3	1.3	8.	2.9	8 8	5	7.1	11.4	8.3
TEMP E DEGH MEAN S	0.0	1.9 2.6	3.3	3.7		e 0	6.5	11.0	13.9	18.2	17.3
NO OBS	2 ~	7 11	σ,	2	σ.	• :	2	14	13	ø	~
SOUTH ERROR M/SEC MEAN ST DEV	2.4	2.4	5.9	e .		m 0	0.8	12.2	15.9	33.8	0.0
SOUTH MEAN	2.6 3.5	4 4 4 9	7.4	6.9	BO .	14.9	16.0	30.1	35.8	52.3	41.4
WEST ERKOR M/SEC MEAN ST DEV	2.3	2.2	2.8	7.	200	90	7.7	12.1	15.8	33.4	0.0
WEST MEAN	2.6	4 9 6 9	7.2	6.3	4 .	14.2	15.5	30.5	34.8	52.0	50.8
088	14	21 28	23	27		7 7	54	28	31	21	4
DIRECTION DEGREES MEAN	306.8	323.6 327.8	337.5	347.3	345.	333.4 1.8	240.4	226.1	281•6	160.6	305.8
SPEED M/SEC MEAN	48.2 53.1	58.4 60.2	51.1	46.4	65.3	29.9	10.4	20.6	17.8	42.5	102.1
SOUTH COMPONENT M/SEC MEAN ST DEV	18.4	22•2 36•3	40.7	39.7	7 · 7	51.2	37.6	46.0	9.49	124.0	143.8
SOUTH B	-28.9 -41.1	147.0	-47.2	-45.3	** 57°	-29.9	5.1	14.2	-3.6	40.1	-59.7
r COMPONENT M/SEC NN ST DEV	19.7	22.5 28.8	24.9	37.6	40.00	24.6	46.4	65.1	81.7	75.1	94.5
WEST CO	38.5 33.6	34.6	19.5	10.	0	6.0	9.1	14.8	17.5	-14.1	85.8
ALTITUDE M MSL	35000	4 5000	20000	55000	0000	70000	75000	80000	8 5000	00006	95000

Table B.4(b).

SEASONAL MEAN PROFILE BARROW SUMMER

		S E E	7 DEG K	,		20000000000000000000000000000000000000			M 10/08		OBS
	MEAN	ST DEV	PCT DIF	MEAN		ST DEV	PCT DIF	MEAN	11.7	PCT DIF	
25000	228 • 6	1.5	0.2	0.271E	70	.200E	'	•413	.593E-0	7	7
26000	229.9	0.3	0.1	0.234E	70	0.200E 02	2 -2.4	0.354E-01	364E	-2.5	7
27000	231.4	4.0	0.1	0.201E	70	•150E	•	• 303	.166E-0	2	21
28000	233.3	8	0.0	0.1745	7 0	• 150E	•	• 260	•134E-0	-2.7	N
29000	234.2	φ (o (0.150E	5 6	.150E		622.	240110	~ (7 (
30000	236.4	7.	• • • • • • • • • • • • • • • • • • •	0.151E	* 2	100	, ,	641	17 47 0	vς	4.0
31000	23/62		7.0	0.1135	3 6	3064		907.		7 7	4.0
32000	290,00	•		1000	9 0	0011				1	4 (
33000	234.9	9.0	9.7.	0.852E	500	3000	•	271		ο,	4 (
34000	235.1		-3.	0.739E	N (1000	•			٦,	7 (
35000	235.9	0.2	14.5	0.640E	60	. 700E	•	945		٠,	7
36000	544.9	9•1	-2.0	0.551E	9	.928E	•	487		7	Δ.
37000	250.0	5.5	-1.2	0.486E	03	•137E	1	677		2	•
38000	253.9	7.7	9.0	0.425E	03	•126E	•	583		- 5	•
39000	257.2	4.5	-0-1	0.372E	03	•115E	1	505		•	•
4 0000	261.5	3.2	-0.2	0.327E	03	.105E	•	•436		•	•
4 1000	266.0	2.1	0.0	0.288E	03	.960E	•	.377		1	9
42000	569.6	3.7	9•0	0.254E	03	.863E	•	• 328		2.4-	•
43000	272.8	2•1	9•0	0.224E	03	.797E	•	• 286		•	9
44000	276.0	9 • 4	1.2	0.198E	03	.726E	•	.250		•	9
4 5000	277.4	7.3	1.4	0.176E	03	•610E	٠	.221		1	7
46000	277.7	6.9	1.1	0.157E	03	.608E	'	197	0.793E-04	•	Φ.
4 7000	278.0	9. 4	8.0	0.138E	03	•621E	1	.173	0.748E-04	•	0.1
4 8000	278.3	5.9	0.5	0.122E	03	.557E	•	.153	0.641E-04	•	10
49000	278.4	e e	4.0	0.108E	60	.502E	•	136	0.559E-04	•	01
50000	278.7	7 .	٠. د	0.965E	200	45.7.	•	7	0.510E=04	•	7
51000	1.612	, ,	۵ •	0.4 4 4 5 7	3 6	144	•	2 2			2.5
00076	270	0 0	•	0.6735	7 0	70.00			0.3795-04		3.5
0000	277.6		9 0	1 4 0 4 0	4 0	200E	7	7 4 7	0 32 BF - 04		20
000	276.2	, 4		0.528F		.271F	7	444	0-294E-04		10
2000	275.0	9	1.1	0.468E	20	244E	•	592	0.262E-04		10
5,7000	273.1		1.1	0.414E	02	.221E	١	528	0.237E-04		10
58000	270.5	2.6	6.0	0.366E	02	.199E	•	471	0.222E-04		101
29000	267.5	2.1	0.5	0.323E	0	•178E		.421	20 7E		2
90009	264.5	2.3	0.7	0.285E	02	.159E	•	.375	_		0.1
61000	261.2	2.2	1.2	0.251E	02	•141E	•	•334	180E		ដ
62000	257.7	5 • 4	1.6	0.220E	02	•125E	î	• 298	191		10
63000	254.2	2.7	2•1	0.193E	05	•111E	•	• 265	~ .		2 :
94000	250.8	60	2.6	0.169E	20	*987E		6239	٠.		9.
65000	246.6	m (5.0	0.148E	200	•877E		. 209	-i :		2.
9000	244.0	7.0		367100) (11411			i à		7.
0000	7.000	9 1	V 0	0.0705	3 6	1000		777	. a		1.
000	220.0			0.8475	1 5	1 4 4		2 2	'n		9.5
70000	223.7	2		0.731F	50	476E		113	٠.		01
71000	217.6	5 2 2	2,6	0.629E	: 0	0.441E 0	300	1001	0.637E-05	1.2	•
72000	212.4	•	2.4	0.538E	010	.387E		.883	in		0.
73000	207.0	•	2.0	0.459E	01	.338E		•773	in		σ.
74000	201.3	•	1.5	0.390E	5	.293€		•675	3		•
75000	195+5	٠	6•0	0.330E	5	.253E		C.588E-04			O.
76000	189.7	3.4	7.0	0.277E	01	•217E		506			O
77000	183.9	•	-0.2	0.232E	5	.184E		•440E-			Φ,
78000	178.3	3.1	8.0-	0.193E	0	0.155E 00		-377E-	0.294E-05		о ъ
19000	172.4	•	-1.5	0.1576	5	1000		217	4000		a

ര ര	30	80	60	80	ဆ	60	30	00	7	9	•	m	7	7	-
5.8	7.4	8.6	10.6	9.6	6.7	3.1	-0.5	-3.1	-6.7	0.0	-12.0	0.0	-20.8	0.0	-23.9
0.170E-05 0.153E-05	0.1415-05	0.130E-05	0.117E-05	0.941E-06	0.707E-06	0.526E-06	0.409E-06	0.327E-06	0.337E-06	0.281E-06	0.232E-06	0.211E-06	0.162E-06	0.911E-07	0.000E 00
0.270E-04 0.229E-04	0.193E-04	0.160E-04	0.1316-04	0.106E-04	0.842E-05	0.663E-05	0.522E-05	0.412E-05	0.323E-05	0.253E-05	0.195E-05	0.145E-05	0.115E-05	0.8855-06	0.732E-06
3.3	2.0	9.0	-1.4	0.4-	-6.7	-6.3	-11.7	-14.0	-16.4	0.0	-20.1	c•0	-30.0	0.0	-46.4
0.873E-01 0.746E-01															
0.129E 01 0.105E 01	0.852E 00	0.684E 00	00.545E 00	0.432E 00	0.341E 00	0.270E 00.	0.214E 00	0.170E 00	0.134E 00	0.106E 00	0.857E-01	0.658E-01	0.510E-01	0.414E-01	0.2695-01
-2.4	6.4-	18.1	-10.6	-12.1	-12.3	-11.9	-11.3	-10.9	8.6-	0.0	-7.8	0.0	6.4	0.0	-28.7
3 ° ¢	3.5	5.0	5.9	6.3	6.2	9. 4	6.9	7.5	10.4	13.4	18.3	29.B	38.6	45.8	0.0
166.4	153.7	148.4	144.4	141.9	141.6	142.3	143.3	143.9	145.7	148.3	154.3	161.9	160.0	167.4	127.9
90000 81000	82000	83000	84000	P 5000	86000	97000	8 8 0 0 0	00066	00006	91000	00026	63000	00076	00056	00096

PERCENT DIFFERENCES WERE CALCULATED USING U.S. STANDARD ATMOSPHERE SUPPLEMENTS, 1966 60 N JULY STANDARD ATMOSPHERE ABOVE 90 KM. IS AVAILABLE FOR EVEN KILOMETER LEVELS ONLY

SEASONAL MEAN PROFILE

BARROW SUMMER

NO OBS	4 10	11	11	0.	10	~	æ	٥	01	10	7	~
ERROR SREES ST DEV	4.0	9.0	6.0	8.0	0.8	0.8	9.0	6.0	9.0	1.4	5.5	0.0
TEMP DEG	0.0	6.0	1.5	1.4	1.5	1.2	1.4	1.4	1.8	2.6	7.7	5.3
NO OBS	00	0	0	0	0	0	0	0	0	0	0	0
SOUTH ERROR M/SEC MEAN ST DEV	00	0.0	0	0.0	0	0	0.0	0	0.0	0	0	0
SOUTH MEAN	90	0.0	0	0.0	0	0	0	0.0	0	0.0	0,0	0
WEST ERROR M/SEC MEAN ST DEV	00	0.0	0	0	0	0.0	0.0	0.0	0	0.0	0	0.0
WEST M.	00					-	_				_	
NO 085	4 w	11	Ξ	o,	10	7	œ	0	10	10	7	7
DIRECTION DEGREES MEAN	113.2	78.8	67.3	84.1	79.6	79.2	88.8	73.8	9.59	132.3	103.5	8.06
SPEED M/SEC MEAN	6.4	13.1	15.7	16.4	25.5	22.5	34.8	40.5	50.7	23.1	18.0	27.8
SOUTH COMPONENT M/SEC MEAN ST DEV	2.6	4.3	7.1	5.6	14.3	8 • 8	12.7	24.6	34.0	45.7	47.7	6•9
SOUTH MEAN	2.6	-2.5	-6.0	-1.6	-4.5	-4.2	-0-7	-11.2	-20.9	15.5	4.2	4.0
WEST COMPONENT M/SEC MEAN ST DEV	5. 9.3 9.3	5.2	7.9	6.4	7.1	10.0	8.7	21.3	34.6	47.7	68.6	16.5
WEST C	-6.8	-12.8	-14.5	-16.3	-25.1	-22.2	-34.8	-38.9	-46.2	-17.0	-17.5	-27.8
ALTITUDE M MSL	35000	45000	50000	55000	60009	9 2000	70000	75000	80000	85000	00006	95000

SEASONAL MEAN PROFILE BARROW SPRING/FALL

MEAN 13.5 13.5 13.5 13.5 13.6 13.7 13.7 13.7 13.7 13.7 13.8	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	T	MEAN 0.919E-02 0.789E-02 0.692E-02 0.692E-02 0.593E-02 0.593E-02 0.283E-02 0.283E-02 0.283E-02 0.286E-02 0.286E-02 0.286E-02 0.286E-02 0.286E-02 0.286E-02 0.286E-02 0.286E-02 0.286E-03 0.286E-03 0.286E-03 0.396E-03 0.397E-03	00000000000000000000000000000000000000	POT 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	444	1	2002 2002	0.5926	1 * 1 1 1	- пппппппппппппппппппппппппппппппппппп
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	444 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		2002 2002	0.692E - 03 0.692E - 03 0.692E - 03 0.358E - 03 0.358E - 03 0.256E - 03 0.256E - 03 0.152E - 03 0.152E - 03 0.107E - 03 0.106E	1111	попопопопопопопопопопопопопопопопопопо
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	44 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0 0 4 4 8 0 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7. E E E E E E E E E E E E E E E E E E E	0.580E 0.398E 0.398E 0.208E 0.208E 0.208E 0.208E 0.208E 0.108E	11111	
0.000		11111111111111111111111111111111111111	74 F 8 E E E E E E E E E E E E E E E E E E	0.000000000000000000000000000000000000	11111	
0.200		1	2011 2011 2011 2011 2011 2011 2011 2011	0.3568FF 0.3	11111	
00.00 00 00 00 00 00 00 00 00 00 00 00 0		11111111111111111111111111111111111111	10000000000000000000000000000000000000	0.228E-03 0.228E-03 0.228E-03 0.221E-03 0.128E-03 0.158E-03 0.128E-03 0.128E-03 0.128E-03 0.128E-03 0.128E-03 0.128E-03 0.128E-03 0.128E-03 0.128E-03 0.128E-03 0.128E-03 0.128E-03 0.128E-03 0.128E-03 0.128E-03 0.128E-03	11111	,
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0.190E	0	-10.7	0E-04	0.911E-05		9 :
0.162E	0	-10.2	75E-04	0.805E-05		91
0.137E	0	8.6-	17E-04	0.699E-05		16
0.116E	0	-6.3	14E-04	0.595E-05		16
0.986E	0	-8.9	76E-04	0.507E-05		16
0.830E	•	-8.6	1E-04	0.433E-05		16
0.697E	•	-8.6	8E-04	0.367E-05		16
0.589E	0	-8.0	10E-04	0.295E-05		57
0.493E	0	-8.3	0E-05	0.233E-05		15
0.408E	0	-9.7	3E-05	0.188E-05	6.81	14
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SEASONAL MEAN PROFILE

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SOUTH MEAN	6000	13.5	-3.0 -2.9	-1.4 2.1 14.5 -0.4
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